

6 NYCRR PART 373 MODIFICATION REQUEST TO SITEWIDE PART 373 PERMIT PERMIT ID 9-2934-00022/00097

ADDITIONAL DOCUMENTS

CWM CHEMICAL SERVICES, LLC. MODEL CITY FACILITY

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Prepared By: CWM Chemical Services, LLC. 1550 Balmer Road

Model City New York, 14107

ADDITIONAL DOCUMENTS DEVELOPMENT OF RESIDUALS MANAGEMNET UNIT NO. 2

- RMU-2 Description, November 2013
- Facultative Pond Tank Assessment, November 2013
- Part 361 Siting Certificate Application, November 2013 (under separate cover)
- Part 617 Draft Environmental Impact Statement (DEIS), November 2013 (under separate cover)

"SECTION B" RMU-2 DESCRIPTION

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SECTION B

FACILITY DESCRIPTION

This section provides a brief overview of the existing treatment, storage, disposal and recovery (TSDR) facility located at CWM Chemical Services, LLC (CWM) Model City, New York. It also provides a general description of the proposed residuals management unit to be located at the existing facility that shall be referred to as Residuals Management Unit 2 (RMU-2). In addition, a general description of existing facilities to be relocated within the site is presented for those facilities affected by the proposed RMU-2 development. The NYSDEC has indicated that they will be treating the RMU-2 Permit Application as a major permit modification to the existing Sitewide 6 NYCRR Part 373 Permit #9-2934-00022/00097 (RMU-2 Modification Application). CWM submitted an updated RMU-2 Permit Application as a Sitewide Permit Modification Application on February 27, 2013 and a revised Permit Modification Application on August 28, 2013. The New York State Part 373 Permit Modification Application covers the proposed RMU-2 facility and those existing facilities to be relocated, as described herein, only. This section contains only descriptions of the proposed unit and the elements of the existing permitted facility that will interact with the operation of this unit.

B-1 GENERAL DESCRIPTION [6 NYCRR 373-1.5(a)(2)(i)]

B-1a <u>Description of Existing Facility</u>

The Model City Facility is located within the Erie-Niagara Region in the western section of New York State. The Model City Facility is situated on the boundary between the Towns of Lewiston and Porter in Niagara County. All hazardous waste management units are located within the Town of Porter. The regional location of the Model City Facility, the facility location relative to local areas immediately surrounding the facility and the facility site layout are shown on Figures B-1, B-2 and B-3, respectively. The existing active waste management units at the Model City Facility (United States Environmental Protection Agency [USEPA] ID No. NYD049836679) are fully permitted as part of the Model City TSDR Facility. It utilizes fully permitted, state-of-the-art technologies for the proper storage, treatment and disposal of a variety of liquid, solid and semisolid organic and inorganic hazardous waste and industrial non-hazardous waste. Storage, treatment and disposal capabilities include an aqueous waste treatment system that utilizes phase separation, waste-on-waste reactions, neutralization, solids precipitation and filtration, biological action and carbon filtration, ultimately resulting in the return of the treated effluent to the environment pursuant to the CWM's State Pollutant Discharge Elimination System (SPDES) Permit. Other operations include waste stabilization; secure landfilling of approved waste solids and semisolids, including polychlorinated biphenyls (PCBs); solvent and fuel blending processes and Resource Conservation and Recovery Act (RCRA) and Toxic Substances Control Act (TSCA) storage and disposal.

The Model City Facility began operations in 1971 as Chem-Trol Pollution Services, Inc (Chem-Trol). Activities included reclamation of waste oils, distillation of spent solvents, aqueous waste treatment and land disposal. In 1973, the stock of Chem-Trol was purchased by SCA Services, Inc. The Chem-Trol name was retained until late 1978, at which time, the corporate name changed to SCA Chemical Waste Services, Inc. In 1981, the name was changed SCA Chemical Services, Inc.

In October 1984, WM Acquiring Corp., owned jointly by Waste Management, Inc. (Waste Management), and Genstar, Inc., acquired SCA Services, Inc., of which, SCA Chemical Services, Inc. was a subsidiary. Through a corporate reorganization in October 1986, SCA Chemical Services, Inc. became a wholly owned subsidiary of CWM, itself majority-owned by Waste Management. In July 1988, the corporate name SCA Chemical Services, Inc. was changed to CWM Chemical Services, Inc. CWM Chemical Services, Inc. became a limited liability company in January 1998 and became CWM Chemical Services, LLC. CWM Chemical Services, LLC is the current owner and operator of the Model City Facility. Waste Management is based in Houston, Texas.

The effluent discharge pipeline for CWM originates at the Model City Facility, which is located in Niagara County near Model City, New York, and terminates at the Lower Niagara River near the Lower River Road entrance to Joseph B. Davis State Park in the Town of Lewiston (see Figures A-1 and A-3).

B-1b Description of Proposed Residuals Management Unit 2

CWM (the Applicant) proposes to construct and operate a residuals management unit for the permanent disposal of hazardous wastes (meeting the treatment standards in 40 Code of Federal Regulations [CFR] Part 268) and industrial non-hazardous wastes.

The proposed RMU-2 incorporates a double-lined fully permittable land burial facility design, in a geologically suitable location, to provide a safe approach to addressing part of the state's hazardous and industrial non-hazardous waste disposal capacity needs over the next 10 to 20 years. RMU-2 will accommodate approximately 4,030,700 cubic yards of waste and will be situated on approximately 43.5 acres of land in the location indicated on Figure B-3. The unit will be constructed in accordance with the requirements of 6 NYCRR 373-2.14. As provided in 6 NYCRR 360-1.1(b), non-hazardous industrial wastes disposed in RMU-2 will be managed in accordance with 6 NYCRR Part 373.

B-1c Existing Facilities in the RMU-2 Location

The proposed location for RMU-2 is within an existing developed portion of the Model City Facility currently occupied by the following structures, buildings and operational areas:

- 1. Drum Management Building;
- 2. Empty Trailer Parking Area;
- 3. Full Trailer Parking Area;
- 4. Emergency Response Garage;
- 5. Heavy Equipment and Facility Maintenance/Rolloff Repair Building;
- 6. McArthur and "M" Streets;
- 7. Various aboveground and belowground utilities and communications services;

- 8. Facultative (Fac) Pond 8;
- 9. Fac Pond 3;
- 10. Stabilization Facility Parking Area;
- 11. Secure landfill- (SLF-) 10 Leachate Building Unloading Ramp; and
- 12. SLF 1-11 Oil/Water Separator Building Unloading Ramp.

The following sections provide a brief description of each of the aforementioned facilities.

B-1c(1) <u>Drum Management Building</u>

The existing Drum Management Building, constructed in 1982, is located approximately 350 feet west of Residuals Management Unit 1 (RMU-1). The Drum Management Building, based on the types/volumes of wastes received by the site, is the focal point for most incoming drums and other small waste containers.

Following construction of the new Drum Management Building, the existing Drum Management Building will be closed in accordance with the closure requirements included in the Site-Wide Part 373 Permit. Closure activities to be implemented for the existing Drum Management Building include the following:

- An initial inventory of all wastes within the building will be performed to verify accuracy with current records, to confirm the integrity of all waste containers for removal and to identify, by visual observation, any potentially contamination areas.
- All wastes will then be removed from the building and either relocated to the new Drum Management Building, disposed on site or transported off site to an approved hazardous waste management facility.
- Following removal of all waste containers, the Drum Management Building will be decontaminated by sweeping or vacuuming the floors, followed by washing the floors. Any wastewater generated by the washing will be treated on site at the aqueous wastewater treatment (AWT) facility. Once the cleaning process has concluded, the building will be demolished. Following demolition of the building, the demolition debris will be properly disposed at an approved waste management facility.
- The soils underlying the Drum Management Building will be excavated as part of RMU-2 construction, in accordance with the requirements of the RMU-2 Soil Excavation Monitoring and Management Plan. Following completion of the closure activities, CWM will submit to the NYSDEC a certification that the Drum Management Building has been closed in accordance with the specifications in the Site-Wide Part 373 Permit within 60 days of final closure. Because existing operations will continue at the new Drum Management Building, it is anticipated that most mobile and stationary equipment utilized in the existing Drum Management Building will be transferred to the new

building for continued use. Any equipment not planned for reuse will be cleaned, tested and managed in accordance with the Site-Wide Part 373 Permit requirements.

The new Drum Management Building, to be located east of RMU-1, will also include a small laboratory and an area designated for transfer of waste organic liquids (i.e., fuels blending) from drums to bulk containers or vacuum trucks and an area designated for transformer flushing operations.

CWM will provide a more modern structure for container storage and consolidate several existing facility operations. The Secondary Containment Calculations for the new Drum Management Building are provided in Section D-1 of the Permit Modification Application.

B-1c(2) Empty Trailer Parking Area

The Empty Trailer Parking Area is used to stage trailers following the off-loading of wastes. The existing Empty Trailer Parking Area is located approximately 400 feet east of the existing Drum Management Building. The existing Empty Trailer Parking Area will be eliminated by the construction of RMU-2. Empty trailers will continue to be staged in an existing storage area northwest of SLF-12.

B-1c(3) Full Trailer Parking Area

The existing South Full Trailer Parking Area, located approximately 400 feet east of the existing Drum Management Building (south of the existing Empty Trailer Parking Area) is used for the storage of liquid and solid, RCRA regulated, TSCA regulated and non-hazardous containers. These containers consist of the following:

- Box trailers holding hazardous and non-hazardous, Department of Transportation- (DOT-) approved containers;
- Bulk tanker trailers, vacuum trailers or other bulk containers holding liquids;
- Covered rolloff trailers, covered dump trailers or other bulk containers holding solid materials; and
- Flatbed or lowboy trailers holding transformers or contaminated solid materials.

The existing Full Trailer Parking Area will be eliminated by the construction of RMU-2. A new Full Trailer Parking Area will be constructed immediately west of RMU-2. The Secondary Containment Calculations for the new Full Trailer Parking Area are provided in Section D-1 of the Permit Modification Application.

A portion of the existing South Trailer Parking Area is located within the footprint of RMU-2. As such, the existing South Trailer Parking Area will be removed and a new area will be installed along the western edge of RMU-2. The new Full Trailer Parking Area would include a reinforced concrete base with concrete curbing on three sides. Prior to construction of the new Full Trailer Parking Area, the existing South Trailer Parking Area

will be closed in accordance the closure requirements included in the Site-Wide Part 373 Permit. Closure activities to be implemented for the existing South Trailer Parking Area include the following:

- An initial inventory of all wastes within the South Trailer Parking Area will be performed to verify accuracy with current records, to confirm the integrity of all waste containers for removal and to identify, by visual observation, any potentially contamination areas.
- All trailers will be transported to the new Full Trailer Parking Area.
- Following removal of all waste containers, the existing South Trailer Parking Area will be decontaminated by sweeping or vacuuming the floors, followed by washing the floors. Any wastewater generated by the washing will be treated on site at the AWT facility.
- Once the cleaning process has concluded, the structure will be demolished. Following demolition of the structure, the demolition debris will be properly disposed at an approved waste management facility.
- Soils underlying the South Trailer Parking Area will be excavated as part of RMU-2 construction, in accordance with the requirements of the RMU-2 Soil Excavation Monitoring and Management Plan.

B-1c(4) Emergency Response Garage

The existing Emergency Response Garage, located along "M" Street will be relocated to the existing truck wash building west of RMU-2 along "M" Street. The existing structure, foundation and all existing utilities will be removed to facilitate construction of RMU-2. Operations associated with the existing Emergency Response Facility will be maintained at the new location.

B-1c(5) Heavy Equipment and Facility Maintenance/Rolloff Repair Building

The existing Heavy Equipment and Facility Maintenance/Rolloff Repair Building, located approximately 250 feet west of RMU-1, will be relocated to the area north of Fac Ponds 1 and 2. The existing structure, foundation and all existing utilities will be removed to facilitate construction of RMU-2. Operations associated with the existing Heavy Equipment and Facility Maintenance/Rolloff Repair Building will be maintained at the new location.

B-1c(6) Removal of Portions of McArthur and "M" Streets

To facilitate construction of RMU-2, approximately 2,000 linear feet of site roadway (portions of McArthur Street and "M" Streets) will be removed. Although portions of the roads may remain in service for use by construction vehicles, the road surface material, road base and all above and belowground utilities along the portions of the roads impacted by RMU-2 will be removed prior to the construction.

B-1c(7) Existing Utilities and Communications Services

In November 2002, Blasland, Bouck & Lee, Inc. performed a utilities investigation to identify all existing above and belowground utilities impacted by the construction of RMU-2. All existing utilities will be removed during either relocation of existing facilities or prior to construction of RMU-2.

B-1c(8) Fac Pond 8

Fac Pond 8, located immediately west of RMU-1 will be eliminated as part of site preparation for RMU-2 construction. Fac Pond 8 is currently out of service and undergoing closure, which is expected to be completed prior to RMU-2 permitting. A certification of the chemical clean closure of Fac Pond 8, in accordance with the Sitewide Closure Plan, was prepared by Golder Associates and submitted to the NYSDEC on November 9, 2009. Remediation of radiological contamination in Fac Pond 8 is currently in progress.

During 2010, a Radiological Characterization Investigation was performed of Fac Pond 8. During the investigation, Fac Pond 8 was divided into twelve, 2,000-square meter survey units. The investigation included gamma walkover surveys, the installation of 193 soil borings, and the collection of 207 soil samples from the soil borings. Readings above investigation levels were discovered within two of the survey units, and radiological contamination was verified through sampling and laboratory analyses. This effort demonstrated in accordance with MARSSIM guidance that all but two of the survey units are below the remedial standards developed for nearby FUSRAP sites and consistent with background concentrations.

A Remedial Action Plan (RAP) was prepared utilizing the data generated from the previous investigations to calculate the risk associated with various exposure scenarios and to derive an appropriate guideline level that can be used during Fac Pond 8 remedial activities. Remedial activities were performed between September and November 2011 and included the removal of soil with suspected MED material above established cleanup levels and the performance of a Final Status Survey (Completion Report for the Remediation of Facultative Pond 8, CWM Model City [Los Alamos Technical Associates, Inc., January, 2012]). Results of the remediation and FSS indicate that the area may be released for future development without the threat of MED radiological conditions above regulatory criteria.

During the remedial activities, a thin layer of soil (lens) with slightly elevated gamma radiation measurements and corresponding radioisotope concentrations was discovered by CWM's radiological consultant, Los Alamos Technical Associates, Inc (LATA). The layer was found within designated Survey Unit #9 (SU#9), which is the North berm of Fac Pond 8. Approximately 150 feet of the berm was excavated during the remediation, which exposed the approximate 18-inch thick lens of anomalous soil material. A sample was obtained and submitted to an independent off-site laboratory for radiological analysis. The results of the analysis indicated that the soil was different than the Manhattan Engineering District (MED) contaminated soil excavated and packaged during the remediation, and potentially from another

unknown source. However, the levels of radiological material present in the sample were above the cleanup levels established in the Remedial Action Plan (RAP (July 2011)) for Fac Pond 8. The purpose of the Work Plan was to outline the specific procedures to be utilized for performing an additional investigation to delineate the extent of the radiologically elevated soil layer in SU #9 of the fac pond North berm. An investigation of Survey Unit #9 was performed in April 2012. Results of the investigation indicated that that the soil was different than the MED contaminated soil excavated and packaged during the remediation, however, the levels of radiological material present in the sample were above the cleanup levels established in the RAP.

The NYSDEC has proposed a compliance schedule for the upcoming Sitewide Permit Renewal. The compliance schedule indicates that Fac Pond 8 must be fully radiologically characterized within one year of the effective date of the permit renewal (EDP) renewal, fully radiologically remediated within two years of the EDP renewal, and fully closed in accordance with the Sitewide Closure Plan within three years of EDP renewal.

After closure of Fac Pond 8, structural (as required) and general soil fill will be added to establish the excavation grades shown on Permit Drawing No. 4, included in the *RMU-2 Engineering Report* (ARCADIS, April 2003, Revised August 2009, January 2012, February & June 2013).

B-1c(9) Fac Pond 3

Fac Pond 3, located west of Fac Pond 8, is currently being used for storage of treated wastewater. Wastewater stored in Fac Pond 3 is discharged to the Niagara River following approval of prequalification testing. Fac Pond 3 will also be eliminated as part of site preparation for RMU-2 construction. Fac Pond 3 will be closed similar to Fac Pond 8, as described above. Fac Pond 3 lies within the footprint of RMU-2 and will be filled with structural (as required) and general soil fill to the excavation grades shown on Permit Drawing No. 4, included in the *RMU-2 Engineering Report* (ARCADIS, April 2003, Revised August 2009, January 2012, February, June & November 2013).

Fac Pond 3 will be closed in accordance with Model City Facility's Site-Wide Closure Plan. The closure of Fac Pond 3, as described in the Model City Facility's Site-Wide Closure Plan, consists of discharging treated effluent from the Fac pond following approval of the pre-qualification testing requirements included in CWM's SPDES Permit. Following discharge of treated effluent, the soils at the base of Fac Pond 3 will then be sampled in accordance the Site-Wide Closure Plan.

It will then be determined if removal of the soils and sediments from the bottom of Fac Pond 3 is needed based on the results of the initial sampling described above. If concentrations of hazardous constituents do not exceed Industrial Soil Cleanup Objectives provided in 6 NYCRR Part 375-6.8(b), the soils and sediments from the pond areas will be excavated to achieve design grades for RMU-2. In the event concentrations of hazardous constituents exceed Industrial Soil Cleanup Objectives provided in 6 NYCRR Part 375-6.8(b) in the surface

samples, but not in the samples collected at the 6-inch depth, a minimum of 6 inches of soil/sediment will be removed from the base of the pond and properly disposed. The remaining soils will be excavated to achieve design grades for RMU-2.

If concentrations of hazardous constituents exceed Industrial Soil Cleanup Objectives provided in 6 NYCRR Part 375-6.8(b) in the subsurface samples, but not in the surface samples, the upper twelve inches of material will be removed from the bottom of the facultative pond and disposed of properly. In the event that materials are removed, post-removal sampling will be conducted to confirm that the indicated criteria above have been achieved. The sampling and analysis program described in the Sitewide Closure Plan will be repeated (including sampling locations and analytical parameters) except that only the one inch surface samples will be collected.

Excavation and disturbance of soils associated with construction of Fac Pond 5 and closure of Fac Pond 3 will be performed in accordance with the requirements of the RMU-2 Soil Excavation Monitoring and Management Plan.

In order to compensate for the treated wastewater volume reduction due to the removal of Fac Pond 3, new Fac Pond 5 will be constructed between SLF-12 and SLF-7. New Fac Pond 5 will serve as the final qualification pond. Details for the construction of new Fac Pond 5 are shown on Permit Drawings No. 1 through 14, included in the *RMU-2 Permit Modification Application* (February 2013, revised August & November 2013).

A new transfer pipeline will be installed between Fac Ponds 1 and 2 and the new Fac Pond 5 to allow for transfer of liquid between the two Fac ponds and to allow Fac Pond 5 to discharge to the existing effluent piping near Fac Ponds 1 and 2. Additionally, the existing influent and effluent piping will be modified, as necessary, and a valve house will be constructed to accommodate the Fac pond transfer line construction.

New Fac Pond 5 will be constructed to the north of RMU-2 and between SLF-12 and SLF-7. The new Fac pond will provide storage lost due to the removal of Fac Ponds 3 and 8. Fac Pond 5 will include the a Part 373-compliant liner system. The perimeter berm of Fac Pond 5 will be established at elevation 335.0 feet amsl. Containment capacity to the top of the perimeter berm of the Fac pond is approximately 24.7 MG. Usable capacity for the Fac pond is approximately 21.9 MG. The usable capacity is based on the need to limit liquid elevation to elevation 333.0 feet amsl to provide 2 feet of freeboard.

Sideslope riser pipes will be installed at Fac Pond 5 that will allow for monitoring of liquid levels in the sump of the leak detection system and for removal of accumulated liquids. A prefabricated riser house will be installed near the top of the perimeter berm at the sideslope riser pipe location. The sideslope riser pipe will penetrate the wall of the riser house so that transfer piping from the submersible pumps is sheltered from inclement weather. The riser house will also contain a dual-walled tank for storage of liquids pumped from the leak detection system. A Design Assessment Report for these proposed tanks was submitted to the NYSDEC in April

2013 (Ensol, April 2013, revised August & November 2013). A ramp will be provided up to the perimeter berm to allow tanker truck access to the storage tank in the riser house and for other general maintenance access.

A new transfer line will be installed between Fac Ponds 1 and 2 and Fac Pond 5. The transfer line will include two parallel 6-inch-diameter double-walled HDPE pipes installed at grade or slightly below grade to minimize excavations, and covered with a minimum of 9-inches of soil. As indicated on Permit Modification Application Drawing Nos.5, 6, and 7, the pipeline will slope to low points in lines where leak detection manholes will be installed. At Fac Pond 5, the pipeline will terminate at the riser house and connective piping will be installed to allow either of the two parallel lines to be used to fill or drain the pond. At Fac Ponds 1 and 2, the pipeline will pass through a new valve house to the north of the Fac pond perimeter berm to allow for discharge to Outfall 001 discharge line or to discharge to the Fac pond. Piping will be installed to allow either of the two parallel lines to be used to transfer liquid from Fac Ponds 1 and 2 to Fac Pond 5 or vice versa, fill Fac Pond 5 with effluent from the site's treatment plant and to discharge liquid from Fac Ponds 1 and 2 or from Fac Pond 5 to the existing discharge piping leading to the Niagara River. The existing discharge filter system will be relocated from its current location at Fac Pond 3 to an area north of Fac Ponds 1 and 2.

B-1c(10) Stabilization Facility Parking Area

The existing Stabilization Trailer Parking Area consists of three separate concrete secondary containment areas, which are located west of the Stabilization Building. The south and west areas are currently permitted for bulk container storage similar to the Full Trailer Parking Area. The north area is currently used for storage of non-hazardous materials. The south and west areas are located within the footprint of RMU-2. Prior to RMU-2 construction, the existing north area will be removed and a new longer concrete secondary containment will be installed in that location, designed similar to the existing areas.

Prior to RMU-2 Cells 15 and 16 construction, the existing north area (Areas I & II) will be closed in accordance with the Site-Wide Part 373 Permit and removed and a new longer concrete secondary containment will be installed in that location, designed similar to the existing areas.

Following construction of the new Stabilization Trailer Parking Area, the existing west and south Stabilization Trailer Parking Areas will be closed in accordance with the closure requirements included in the Site-Wide Part 373 Permit. Closure activities to be implemented for the Stabilization Trailer Parking Areas include the following:

- An initial inventory of all wastes within the west and south Stabilization Trailer Parking Areas will be performed to verify accuracy with current records, to confirm the integrity of all waste containers for removal and to identify, by visual observation, any potentially contamination areas.
- All trailers will be transported to the new Stabilization Trailer Parking Area or alternative area.

- Following removal of all waste containers, the existing west and south Stabilization Trailer Parking Areas will be decontaminated by sweeping or vacuuming the floors, followed by washing the floors. Any wastewater generated by the washing will be treated on site at the AWT facility.
- Once the cleaning process has concluded, the structures will be demolished. Following
 demolition of the structures, the demolition debris will be properly disposed at an
 approved waste management facility.
- Soils underlying the west and east Stabilization Trailer Parking Areas will be excavated as part of RMU-2 construction, in accordance with the requirements of the RMU-2 Soil Excavation Monitoring and Management Plan.

The Secondary Containment Calculations for the new Stabilization Facility Parking Area are provided in Section D-1 of this Permit Modification Application.

B-1c(11) SLF-10 Leachate Building Unloading Ramp

The existing unloading ramp for the SLF-10 Leachate Building is currently situated on the north side of the building, within the footprint of RMU-2. For this project, the existing unloading ramp will be removed and reconstructed on the south side of the SLF-10 Leachate Building. The new unloading ramp will include a 8-inch-thick reinforced concrete slab, extending approximately 71 feet from the southern edge of the SLF-10 Leachate Building. Additional details for the new unloading ramp for the SLF-10 Leachate Building are provided on Permit Application Drawing No.D-12A, included in the *RMU-2 Permit Modification Application* (February 2013, revised August 2013).. The Secondary Containment Calculations for the new SLF-10 Leachate Building Unloading Ramp are provided in Section D-1 of the Permit Modification Application. Following construction of the new ramp, the existing ramp will be closed in accordance with the closure requirements included in the Site-Wide Part 373 Permit and demolished. Closure activities to be implemented for the SLF-10 Unloading Ramp include the following:

- Following construction of the new ramp, the existing ramp will be decontaminated by sweeping or vacuuming the floor, followed by washing the floor. Any wastewater generated by the washing will be treated on site at the AWT facility.
- Once the cleaning process has concluded, the ramp structure will be demolished.
 Following demolition of the structure, the demolition debris will be properly disposed at an approved waste management facility.
- Soils underlying the ramp will be excavated as part of RMU-2 construction, in accordance with the requirements of the RMU-2 Soil Excavation Monitoring and Management Plan.

B-1c(12) SLF 1-11 Oil/Water Separator Building Unloading Ramp

The existing unloading ramp for the SLF 1-11 Oil/Water Separator Building is located on the northern side of the building. Due to the construction of new Fac Pond 5, the unloading ramp for this building will be relocated to the east side of the building. The new unloading ramp for the SLF 1-11 Oil/Water Separator Building will include a 8-inch-thick reinforced concrete slab, extending approximately 71 feet along the eastern edge of the building. Additional details for the new

unloading ramp for the SLF 1-11 Oil/Water Separator Building are provided on Permit Drawing No. D-14A38, included in the *RMU-2 Permit Modification Application* (February 2013, revised August 2013).. The Secondary Containment Calculations for the new SLF 1-11 Oil/Water Separator Building Unloading Ramp are provided in Section D-1 of the Permit Modification Application. . Following construction of the new ramp, the existing ramp will be closed in accordance with the closure requirements included in the Site-Wide Part 373 Permit and demolished. Closure activities to be implemented for the SLF1-11 Oil/Water Separator Building Unloading Ramp include the following:

- Following construction of the new ramp, the existing ramp will be decontaminated by sweeping or vacuuming the floor, followed by washing the floor. Any wastewater generated by the washing will be treated on site at the AWT facility.
- Once the cleaning process has concluded, the ramp structure will be demolished. Following demolition of the structure, the demolition debris will be properly disposed at an approved waste management facility.
- Soils underlying the ramp will be excavated as part of RMU-2 construction, in accordance with the requirements of the RMU-2 Soil Excavation Monitoring and Management Plan.

B-2 TOPOGRAPHIC MAP [6 NYCRR 373-1.5(a)(2)(xix)]

Figure B-3 provides topographic details of the entire site.

B-2a Local Topography

The Towns of Porter and Lewiston are part of the Ontario Plain. The plain is located north of the Niagara escarpment, the northernmost major topographic feature in Niagara and Erie Counties. Both the elevation and relief of the land surface tend to increase from north to south. The Model City Facility is located on a flat plain forming a portion of the extended Lake Ontario shoreline natural grade. Ground elevations on the Model City Facility vary from 308 feet to 338 feet above mean sea level.

B-2b Local Geology

The bedrock formation underlying the Model City Facility is the Queenston Shale. The Queenston Shale is approximately 1,200 feet thick, with only the uppermost part exposed in the region. It underlies all of Niagara County north of the Niagara escarpment, including the Towns of Porter and Lewiston, and can be seen in the Lower Gorge of the Niagara River. It is characterized by brick-red shale that varies from argillaceous (high in clay-sized particles) to sandy (high in sand-sized particles). The Queenston Shale is not exploited for economic purposes. Approximately 50 feet of unconsolidated deposits overlie the bedrock formations. This material was deposited during several Pleistocene glacial periods and consists of alluvial glacial till and glaciolacustrine deposits.

The alluvial deposits are the uppermost units where they occur and consist of clay and silt. They are found sporadically across the Model City Facility. Where the alluvial deposits do not occur, the uppermost units are glacial tills and contain a variety of particle sizes, including silts, clays, sands and gravels. The glaciolacustrine deposits underlie the glacial tills and are made up of silts, clays and sands.

Due to past regrading of the Model City Facility, several feet of fill overlie the original surface soils in some areas. This fill is quite similar to the deeper soils in composition and hydrogeologic properties. Also, a relatively thin veneer of alluvial deposits exists over some portions of the site. The alluvial deposits typically consist of laminated clayey silt, silt and fine sand.

There are two original surface soil associations (types) found on the Model City site. The association covering the largest area is the Rhinebeck-Ovid-Madalin association. This consists of deep, somewhat poorly drained to very poorly drained soils having a fine-textured or moderately fine-textured subsoil that is predominantly brown or olive in color. The other soil association, covering a lesser area, is the Appleton-Hilton-Sun association. This consists of deep, moderately well drained to very poorly drained soils having medium-textured subsoil.

Additional information can be found in the *RMU-2 Engineering Report* (ARCADIS, April 2003, Revised August 2009, January 2012, February & June 2013).

B-2c Hydrology

Groundwater conditions at the Model City Facility have been investigated and are discussed in detail in the 1993 Ground Water Level Interpretation Report (RUST Environment and Infrastructure, February, 1994), Groundwater Monitoring Program Model City Facility (Golder Associates, May 1988), the RMU-1 Groundwater Monitoring Plan (Golder Associates, February 1991) and in many additional reports, which have all been previously submitted to the New York State Department of Environmental Conservation (NYSDEC). In association with the proposed RMU-2 development, a subsurface investigation was performed in the specific area of proposed RMU-2. The results and findings of this investigation are presented in the reports entitled Letter Report on Geotechnical Investigation for Proposed Residuals Management Unit Number 2 - Western Expansion Area (Golder Associates, December 2002) and Landfill Footprint Analytical Data Study and Western Boundary Relocation Investigation (Golder, July 2009). Copies of these reports are presented in Appendix A of the RMU-2 Engineering Report and are discussed in Section 2.2 therein. In general, the 2002 and 2009 Golder reports confirmed the geologic and hydrogeologic findings presented in the previous 1985, 1988 and 1993 site-wide investigations The groundwater monitoring program developed by Golder for the proposed RMU-2 Phase I and Fac Pond 5 was submitted January 26, 2010 and an Addendum No. 1 was submitted June 10, 2011.

Within the several documented reports, potentiometric maps were used to estimate the primary groundwater flow direction and rate under the Model City Facility for the Upper Tills unit and the Glaciolacustrine Silt/Sand unit.

Within the Upper Tills unit, groundwater flow is generally directed to the north-northwest, following the topographic surface. A minor flow component to the south can be found in areas of groundwater mounding; however, the overall net flow direction is to the north-northwest. In the proposed RMU-2 area, the Golder reports indicate that lateral flow of shallow groundwater in this unit is predominantly north-northwest.

The general flow direction of the Glaciolacustrine Silt/Sand unit is also north-northwest toward Lake Ontario, with a northwest component influenced by the higher transmissivity in the northwest portion of the site. In the proposed RMU-2 area, the Golder reports indicate that the lateral flow of groundwater in this unit is predominantly north-northwest.

B-2d Surface Water

The Model City site is located in the Eighteenmile Creek Drainage Subbasin. This subbasin is a portion of the Lake Ontario Drainage Basin, which includes the Eighteenmile Creek Subbasin and other tributaries of Lake Ontario entering the lake between the hamlet of Olcott and the mouth of the Niagara River. The basin drains an area of 233 square miles. Twelvemile Creek drains 45 square miles including a small part of the Model City Facility property, but the major part of the property drains to Fourmile Creek through Sixmile Swale.

Surface drainage and runoff is collected on site in a series of retention basins and drainage channels with control gates. Runoff collected from process areas is directed to the existing wastewater treatment system. Drainage from non-operational areas is collected in the drainage channels and, via a series of manually

controlled gates, is held and tested prior to discharge to nearby surface waters. Discharges from surfacewater outfalls are also included in CWM's State Pollutant Discharge Elimination System (SPDES) Permit.

In addition, the Model City Surface-Water Sampling and Analysis Plan covers surface drainage, runoff and stormwater monitoring in detail.

B-2e Land Use

B-2e(1) Erie and Niagara Counties

The region encompassing Erie and Niagara Counties is bounded by Lake Erie and the Niagara River on the west; by Lake Ontario on the north; by Cattaraugus Creek on the south and Orleans, Genesee and Wyoming Counties on the east. The Erie/Niagara region covers approximately 1,589 square miles with a population in excess of 1.2 million people. The primary use of land in the region is agricultural, comprising approximately 46 percent of the land regionally and approximately 66 percent, or two-thirds, of the land in Niagara County alone.

B-2e(2) Town of Lewiston

The Town of Lewiston, occupying a land area of approximately 40 square miles, is located to the south of the Town of Porter. Approximately 75 percent of the land is undeveloped, and overall residential density is very low, with the majority of town land having a maximum density of one person per acre. With no geographical constraints, development has occurred along major arterials in strip fashion. Agriculture is the primary land use, with crops consisting of grapes, peaches and vegetables. Residential land uses in the western part of the county are mostly concentrated adjacent to the Niagara River, above and below the escarpment and in the Village of Lewiston, although both areas have a low population density compared to most urban areas. The Tuscarora Indian Reservation and Power Reservoir dominate the southern half of the town. The few commercial and industrial facilities are located in the northwestern section.

No regulated units are located in the Town of Lewiston, and no portion of the proposed RMU-2 unit will be located in the Town of Lewiston.

B-2e(3) Town of Porter

The Town of Porter is located in the northwest corner of Niagara County, with a total land area of 33 square miles. Primarily an agricultural town with some industrial land uses, Porter is developing as a residential suburb of Niagara Falls. Public/semipublic land uses in this area include 102 acres used for the Lewiston-Porter School District, located 1.9 miles west of the Model City Facility.

The Town of Porter has zoned the portion of the Model City Facility situated in the town to permit heavy industrial use surrounded by medium industrial and light industrial zones. In these areas, residential uses are not permitted. This land-use designation allows hazardous waste disposal operations. To the southwest and east, the land is zoned with a "one family residential-large lot" requirement interspersed with agricultural districts.

B-2e(4) Site History

CWM's facility in Model City, New York has operated as a hazardous waste treatment, storage and disposal site since 1971. Over that period of time, the corporation has been known by several names, as described in Section B-1a.

The Model City Facility is permitted as a TSDR facility for hazardous and industrial non-hazardous wastes (USEPA ID NYD04983679). The Model City Facility accepts a variety of liquid, solid and semisolid organic and inorganic hazardous wastes and a variety of industrial non-hazardous wastes. In addition, the Model City Facility is approved by the USEPA to store and dispose PCBs.

The Model City Facility serves a market primarily located within approximately a 500-mile radius of the facility. A significant portion of the wastes handled at the Model City Facility is generated in New York State, particularly in the western New York area. Additional wastes from other surrounding states, primarily the northeastern United States, and Canada are also accepted.

Prior to operation as a commercial waste facility, the site was owned by the United States Government (early 1940s through the mid 1960s) and was part of the Lake Ontario Ordnance Works. United States Government activities at and in the vicinity of the site included:

- Explosives and solid/liquid fuel propellant research, development and production;
- Research and development and waste storage related to the Manhattan Project; and
- Detonation of outdated or off-specification explosives.

Some of these activities resulted in the contamination of certain areas of the site with organic and inorganic chemicals and low-level radioactive wastes. However, during the 1960s, initial efforts were made by the Atomic Energy Commission (AEC) to decontaminate these areas, and in the early to mid-1980s, additional areas on the site were remediated by the Department of Energy (DOE). The New York State Department of Health and the NYSDEC oversaw these remedial efforts by the AEC and DOE.

B-2f Wind Rose

Meteorological data collected from 1948 to 1978 at the Buffalo, New York weather station were utilized in preparation of the wind rose, illustrated on Figure B-4. A wind rose prepared from on-site data taken between January 1, 1994 and December 31, 1994 is shown on Figure B-5.

B-3 LOCATION INFORMATION [6 NYCRR 373-1.5(a)(2)(xi) and 373-2.2(8)]

As noted in Section B-1a, the Model City Facility is located near Model City in the Towns of Lewiston and Porter in Niagara County, New York. It is situated along Balmer Road, 1.9 miles east of its intersection with New York Route 18 (Creek Road). The Model City Facility's regional and local positions are illustrated on Figures B-1 and B-2, respectively.

The Model City site encompasses approximately 710 acres of rural land, of which, 630 acres have been permitted for hazardous waste management activities. The site was a part of a United States Government Department of Defense installation, formerly known as the Lake Ontario Ordnance Works. General use of surrounding land includes government-related industrial and military activities and some agriculture.

B-3a Seismic Considerations

The Model City Facility is located in the Towns of Lewiston and Porter, Niagara County, New York. As such, this facility is not located in an area listed in Appendix VI of 40 CFR 264. Facilities that are located in political jurisdictions other than those listed in 40 CFR 264, Appendix VI, are not required to demonstrate compliance with 40 CFR 264.18(a). However, seismic analyses were performed for RMU-2 and Facultative Pond 5 according to 6 NYCRR Part 360-2.7(b)(7). These analyses are included in the Engineering Report for RMU-2.

B-3b Floodplain Standard [6 NYCRR 373-1.5(a)(2)(xi)(a)] and [6 NYCRR 373-2.2(i)]

Based on operational experience at the Model City Facility, no history of on-site flooding and flood-related problems have been identified since the facility began operations in 1971 as Chem-Trol.

Additionally, Federal Emergency Management Agency Flood Insurance Rate Maps for the facility have not been printed due to the fact that the area has been considered an area of minimal flooding.

However, during development of the design for RMU-1, CWM became aware of a flood study conducted for Twelvemile Creek by Wehran-Envirotech (Wehran) on behalf of the Modern Landfill Facility, which borders the Model City Facility to the south. Results of the Wehran study suggested that the proposed location of RMU-1 might include a portion of the 100-year floodplain of Twelvemile Creek. Consequently, CWM contracted Wehran to perform a detailed floodplain study of Twelvemile Creek, specifically with respect to RMU-1. The conclusions of the resultant Wehran report, dated February 16, 1993, are summarized below.

Wehran used the United States Army Corps of Engineers' (USACE's) Hydrologic Engineering Center computer program titled HEC-2, coupled with site-specific information, to perform the floodplain analyses. In the report, Wehran concluded that the 100-year floodwater surface elevations, flow velocities and floodplain boundaries demonstrate that the Model City Facility, as required by regulation, has been designed to prevent encroachment of floodwaters and will not result in the washout of waste. However, the analyses confirmed that the southeast corner of the RMU-1 site is included in the fringe area of the 100-year floodplain of Twelvemile Creek. The floodplain "fringe" is defined as that area

between the limits of the 100-year floodplain and floodway. Wehran also determined that the area impinged by RMU-1 constitutes an area of "ineffective flow" (i.e., an area that provided some level of floodwater storage capacity, but does not provide an effective downstream route for floodwater flow). Thus, while RMU-1 would remove approximately 15.9-acre-feet of temporary floodwater storage capacity, the unit is not located in the floodway and does not result in an increase in the 100-year floodwater surface elevation. The floodplain and floodway limits that will exist after full development of RMU-1 are nearly identical to the prior conditions. In 2000, CWM constructed a 16.7-acre-feet Compensatory Flood Storage Area within the 100-year floodplain of Twelvemile Creek to mitigate the loss of storage capacity attributable to RMU-1.

The proposed location of RMU-2 does not fall within the 100-year floodplain of Twelvemile Creek. As such, floodplain mitigation will not be required for the construction of RMU-2.

B-3c State and Federal Delineated Freshwater Wetlands

In November 2002, a Wetlands Investigation was performed by Environmental Design & Research, P.C. (EDR) at the Model City Facility in the area of the proposed RMU-2 site and at the proposed locations for new and relocated facilities. During this investigation, EDR determined that RMU-2 and the new and relocated facilities would have no impact to state regulated wetlands, as verified by the NYSDEC. EDR also concluded that RMU-2 and the new and proposed locations for relocated facilities would impact less than 2 acres of jurisdictional federal wetlands (comprised of manmade ditches and isolated pockets of wetland areas).

EDR updated the RMU-2 wetlands delineation in April 2009. The investigation areas were redefined based on the current scope of the RMU-2 project (i.e., slightly redesigned landfill footprint and new locations of relocated facilities) as compared to the 2002 investigation. Results of this investigation are described in the *Wetland Delineation Report*, *RMU-2 Landfill Expansion Area*, *dated June 2009*. Again, EDR concluded that the RMU-2 project would have no impact to state wetlands and impact less than 2 acres of federal wetlands, pending confirmation by the USACE. EDR again updated the RMU-2 wetlands delineation in April 2011 to include an area within the RMU-2 development area that was not included in the previous delineations. Results of this supplemental delineation are described in the *Supplemental Wetland Delineation Report*, *RMU-2 Landfill Expansion Area*, *dated April 2011*. Again, EDR concluded that the RMU-2 project would have no impact to state wetlands and impact less than 2 acres of federal wetlands, pending confirmation by the USACE.

The less than 2 acres of wetlands delineated by EDR consist of man-made roadside ditches and isolated pockets of wetland areas, which provide limited function and value (primarily stormwater detention and flood storage). The limited function and value is due to the small size, shallow depth and seasonal inundation/saturation of these delineated wetlands. The wetlands on site provide no aesthetic, recreational or educational value and appear to have little, if any, groundwater recharge or discharge function. The wetlands have little beneficial effect on water quality and do not provide spawning areas for fish, waterfowl habitat or shoreline erosion control. The wetlands also provide limited value for wildlife due to the lack of habitat diversity, water level fluctuations and adjacent disturbance.

A jurisdictional determination was received from the USACE on September 13, 2011. Approximately 2.5 acres of jurisdictional wetlands, as determined by the USACE, are located within the RMU-2 development area.

During the detailed design of the site grading plan for the New Drum Management Building, a supplemental wetlands delineation was performed in the proposed area by EDR in July 2012. The supplemental delineation indicated that a wetland on the north side of the development area extends beyond the delineated area and outside of the study area into an NYSDEC-protected wetland (RV-8).

On November 7, 2012, CWM subsequently requested a jurisdictional determination from the NYSDEC that no state freshwater wetlands would be impacted by the construction of RMU-2, including the New Drum Management Building area. Based on a field delineation by an NYSDEC wetlands biologist, the NYSDEC determined that a portion of the new Drum Management Building Development will be in the 100-adjacent area of a state freshwater wetland (RV-8). Additionally, the NYSDEC issued a determination on February 4, 2013 that no other state freshwater wetlands or 100-adjacent areas are in the RMU-2 development area. The EDR supplemental wetlands delineation and the jurisdictional determinations from the NYSDEC are also included in Appendix D of the DEIS.

Based on the information contained in the EDR Reports (Appendix D of the DIES), the construction of RMU-2, Fac Pond 5 and the proposed relocation of existing structures, buildings and operational areas would impact the 100-foot adjacent area of an NYSDEC wetland and approximately 2.5 acres of federal wetlands. The USACE has indicated that mitigation measures will be necessary for impacts to wetlands in the RMU-2 development area. The NYSDEC has indicated that a vegetative buffer will be constructed and maintained between the new Drum Management Building operational area and the state freshwater wetland. A revised application for a permit in accordance with Section 404 of the CWA was submitted to the USACE on July 8, 2013 for project impacts to jurisdictional wetlands. Compensatory mitigation may be accomplished through one of the following three ways: Mitigation Banks, In-Lieu Fee Mitigation or Permittee-Responsible Mitigation. CWM will pursue a permittee-responsible mitigation through construction of replacement wetlands at an on-site location. The revised Section 404 application will be a joint application with a request for NYSDEC Section 401 water quality certification and a State Article 24 application for impacts to NYSDEC freshwater wetlands (100-foot adjacent area).

To mitigate for the unavoidable permanent loss of wetlands within the Project area, CWM is proposing the creation of a 4.3-acre successional wetland on a 21-acre parcel of land owned by CWM immediately west of the Fac Ponds 1 & 2. This parcel is currently dominated by successional deciduous forest, but also includes areas of disturbed land used for topsoil stockpiles, successional old field, and approximately 5 acres of forested and emergent wetland communities. The successional wetlands to be created on-site will be designed to succeed from scrub-shrub into forested wetlands. This represents a mitigation ratio of approximately 1.7 to 1 (mitigation to impact) for direct impacts to wetlands/streams.

CWM shall place a perpetual deed restriction, in the form of a conservation easement, on the mitigation site to protect the compensatory wetland mitigation area and adjacent uplands in perpetuity and guarantee its preservation. The conservation easement will protect a total of 15.94 acres.

The mitigation of impacts to the 100-foot adjacent area for development of the New Drum Management Building will be accomplished by the construction and maintenance of a vegetated buffer between the buildings operational area and the New York State Freshwater Wetland RV-8.

B-4 TRAFFIC INFORMATION [6 NYCRR 373-1.5(a)(2)(x)]

At present, all incoming and outgoing shipments are handled by truck. All waste-hauling vehicles are independently owned and operated.

The primary access routes for waste shipments to the Model City Facility include the New York State Thruway (I-90), I-290, I-190, New York Route 104, New York Route 18 and Balmer Road. As a condition of accepting hazardous wastes transported to the Model City Facility, CWM requires all waste transporters to use one designated route to the Model City Facility. Transporters of non-waste may use alternate routes to the facility. Approximately 90% of all shipments (including all waste shipments) to the site use these routes; the remainder use local roads to reach the site. The New York State Thruway (I-90) provides Niagara County with access to the New England states to the east and to the central states to the west. Four regionally located bridges provide direct connections to Canada over the Niagara River.

Shipment vehicles include box-type trailers carrying 55-gallon containers and other approved containers. Bulk solids shipments are generally received in rolloff boxes and dump trailers. Bulk liquid trailers are used for large quantities of liquids.

The roads inside the plant are of stone and asphalt construction. These have been subject to heavy loadings for several years and are in excellent condition. The speed limit is 10 miles per hour (mph). Signs are posted on Marshall Street, J Street, M Street and on the Balmer Road entrance to the Model City Facility. Landfill access roads generally consist of stone and on-site soils and are constructed to embankment specifications, generally 6- to 9-inch lifts compacted to 90 percent or greater density. The roads are designed for a load-bearing capacity equivalent to DOT H 20 loading.

The construction of RMU-2 will require the removal of portions of M Street and McArthur Street; however, removal of these roads will not impact facility operations.

All incoming waste shipments enter the Model City Facility at the main entrance at 1550 Balmer Road. The security guard performs an initial inspection of each load that includes an inspection of the truck exterior for leaks, confirmation that the driver has the proper safety gear for entrance to the Model City Facility and the proper paperwork (e.g., manifests, work orders) accompany the shipment. Trucks are not scheduled to arrive after normal operating hours and drivers are so informed. Waste-hauling vehicles entering and leaving the Model City Facility are not allowed to stage on Balmer Road or other roads in Niagara County.

Once admitted at the front gate, vehicles proceed to the scale and quality control (QC) station. After having their paperwork verified and logged in, and being sampled for QC purposes, vehicles containing waste for landfill disposal within the active landfill are directed to the entrance ramp for access to the operating cells within the unit. If QC tests or the manifest indicates that in-plant stabilization is required to meet landfill restrictions, the truck proceeds to the Stabilization Building, rather than directly to the landfill. After stabilization of the load, the truck proceeds to its final disposal location within the active landfill or to a designated short-term storage area until tests to determine the adequacy of the stabilization operation can be completed.

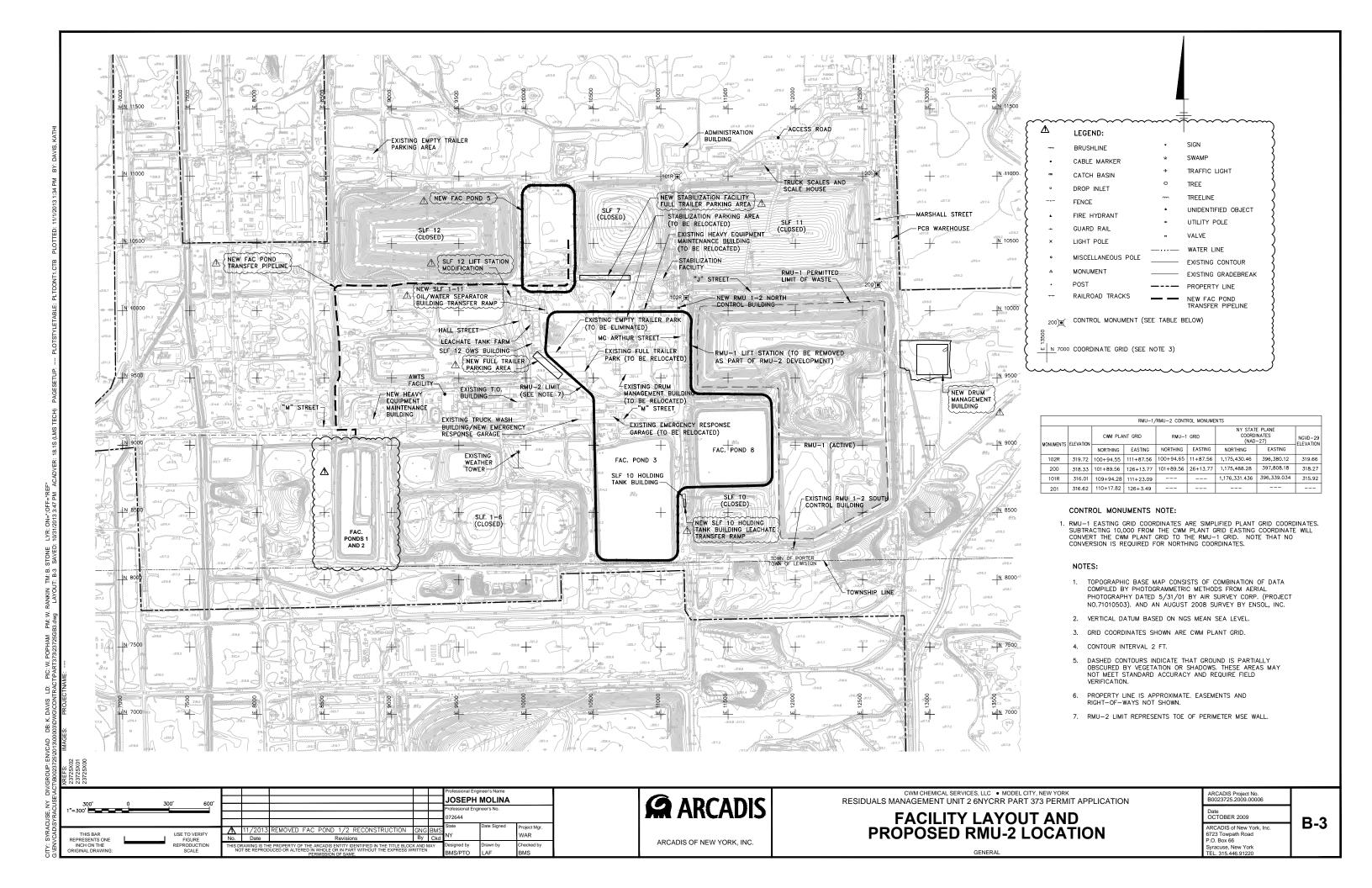
Following completion of the tests, the load is either placed in the landfill or return to the Stabilization Building for further treatment. After making their delivery to the landfill, vehicles are decontaminated, exit the landfill, proceed to the outbound scales and then exit from the Model City Facility via the guardhouse to Balmer Road.

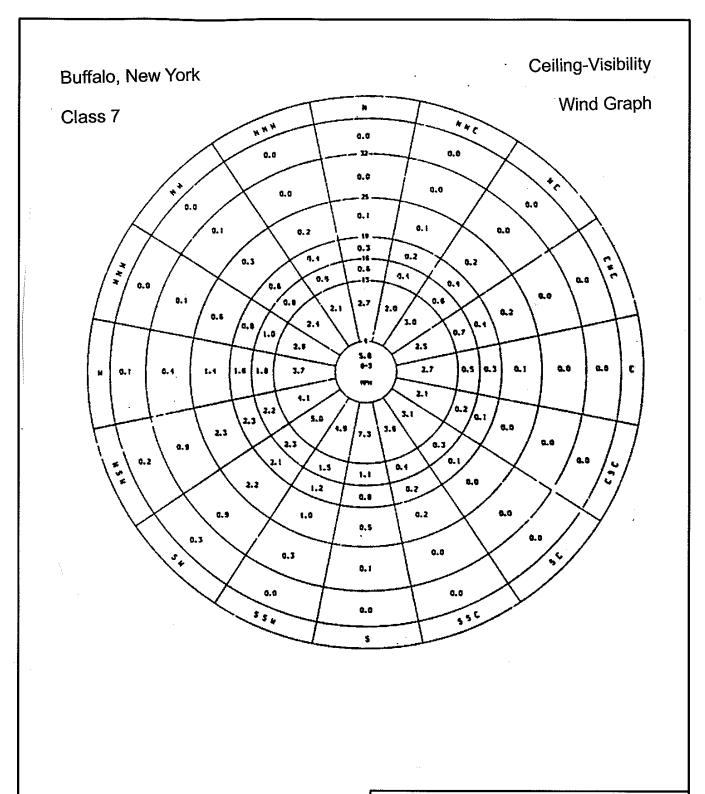
All trucks are decontaminated prior to exiting the landfill. The exterior of trucks that have not come in contact with hazardous waste or have been previously decontaminated may be washed at the Truck Wash Building. The truck access routes to and around the proposed RMU-2 unit are depicted on Figure B-6.

In July 1993, CWM agreed to certain traffic restrictions as part of the Community Advisory Committee (CAC) Agreement. The CAC consists of representatives from the Town of Lewiston, Town of Porter, Niagara County and the Residents Organized for Lewiston-Porter's Environment, Inc.. Traffic routes to and from the Model City Facility, days and hours when trucks may be scheduled for arrival or departure, the maximum number of daily and hourly waste trucks and penalties for violating these restrictions are specified. A copy of the most recent CAC Agreement is available at the Model City Facility.

CITY: CLE DIVIGROUP: AIT 40 DB:L.GREENE LD: EAL PIC: WP PM: TM: GNG TR:
MODEL CITY 23725.003
Friday, June 19, 2009 1:37:16 PM

CITY: CLE DIV/GROUP: AIT 40 DB: L.GREENE EAL LD: EAL PIC: WP PM: TM: GNV MODEL CITY 23725 003





CWM CHEMICAL SERIVCES, LLC MODEL CITY, NEW YORK

6NYCRR PART 373 PERMIT APPLICATION

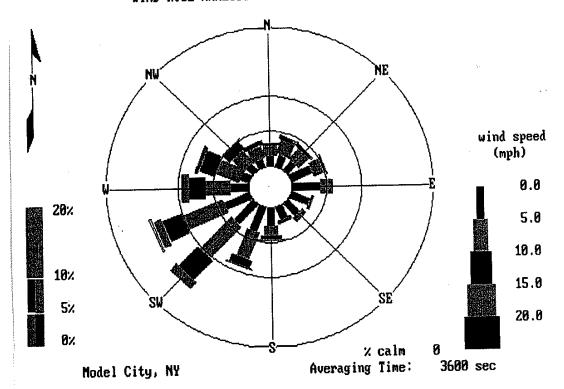
CLASS 7 WIND ROSE BUFFALO, NEW YORK AREA



FIGURE B-4

CWM CHEMICAL SERVICES, INC. ANNUAL 1994

WIND ROSE ANALYSIS FOR 01/01/94 TO 12/31/94



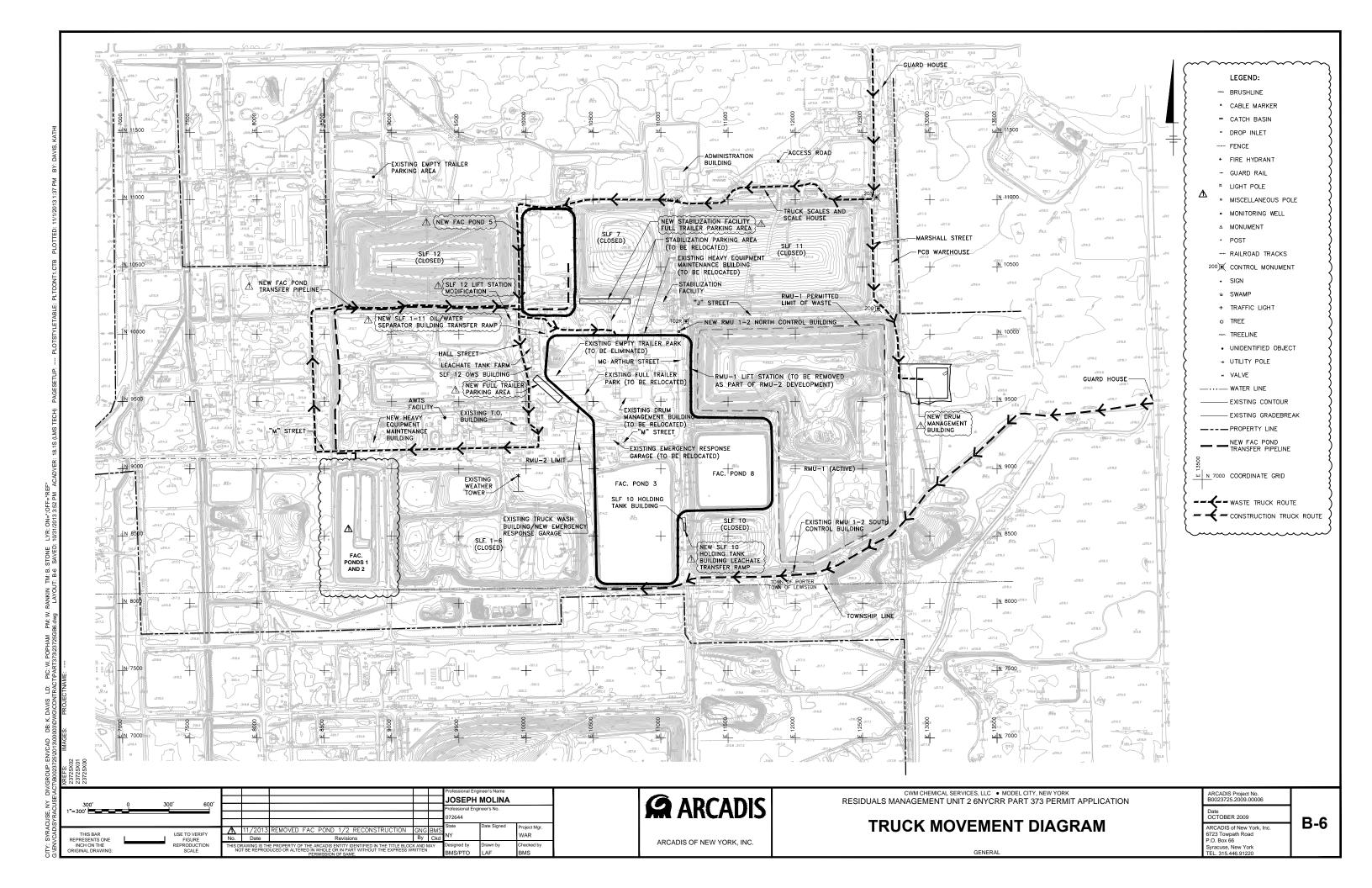
CWM CHEMICAL SERIVCES, LLC MODEL CITY, NEW YORK

6NYCRR PART 373 PERMIT APPLICATION

WIND ROSE ANALYSIS FOR MODEL CITY 01/01/94 TO 12/31/94



FIGURE B-5



FACULTATIVE POND TANK ASSESSMENT T-9001

Tank System Design and Assessment Report for Fac Pond 5 Tank T-9001



CWM Chemical Services, LLC Model City, New York

> April 2013 (Revised August 2013) (Revised November 2013)

> > Prepared by

EnSol, Inc.

Environmental Solutions

Professional Engineering • Business Consulting

Ph (716) 285-3920 • Fx (716) 285-3928 E-Mail bshiah@ensolinc.com

Transmitted Via Electronic Mail and Hand Delivery

November 7, 2013

Mr. Stephen Rydzyk Maintenance Manager / Engineer CWM Chemical Services, LLC 1550 Balmer Road, P.O. Box 200 Model City, New York 14107

Re: Tank System Design and Assessment Report for Fac Pond 5

Tank T-9001

Model City, New York EnSol Project #: 13-7006

Dear Mr. Rydzyk:

Enclosed please find two copies of the Final Report titled, *Tank System Design and Assessment Report for Fac Pond 5 Tank T-9001* dated April 2013 (revised August 2013 and November 2013), as prepared by EnSol, Inc. (EnSol). This report is provided to present applicable design and construction information for the proposed Tank T-9001 system, as described herein, to allow for storage of collected water from the secondary containment system of proposed Fac Pond 5.

The report includes an assessment and review of the structural integrity of the proposed tank system and compatibility of the materials of construction with the material expected to be handled. This assessment is intended to satisfy the State and Federal Regulations listed under 6 NYCRR Part 373-2.10(c), and 40 CFR 264.192, respectively, with regards to design and installation of new tank systems or components.

The intent of this report is to provide sufficient information to the New York State Department of Environmental Conservation (NYSDEC) for review of the proposed system design and usage, and for subsequent approval to construct and operate the tank system.

If you have any questions or require additional information, please contact me at (716) 285-3920, ext. 212.

Sincerely,

ENSOL, INC.

Brian D. Shiah, P.E.

Bran Shif

President

Enclosures

Tank System Design and Assessment Report for Fac Pond 5 Tank T-9001



CWM Chemical Services, LLC Model City, New York

> April 2013 (Revised August 2013) (Revised November 2013)

> > Prepared by **EnSol, Inc.** 661 Main Street Niagara Falls, New York 14301

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- 1. Regional Location Map
- 2. Facility Location Detail
- 3. Facility Layout Plan

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- A. Proposed Fac Pond 5 Permit Drawings (Arcadis)
- B. Proposed Secondary Containment Storage Tank Information (Snyder)
 - Tank Product Data
 - Snyder Specification #199901
 - Tank Chemical Resistance Chart
 - Fac Pond Water Physical / Chemical Analysis
- C. Proposed Pump, Piping, and Equipment Information
 - Secondary Containment Submersible Pump Data (Goulds)
 - Pump Cart Shop Drawing (CWM)
 - Flex Hose Cut Sheet (Goodyear)
 - Level Transmitter (Viatram)
 - Programmable Limit Alarm (Moore)
 - High Level Switch (Madison)
 - Turbine Flow Sensor and Flow Meter Cut Sheet (Seametrics)
 - HDPE Pipe Data (Phillips Chevron)
 - Ball Valve & Hose Adapter (Grainger)

1. Introduction

1.1 General Site Information

CWM Chemical Services, LLC (CWM) owns and operates a commercial hazardous waste treatment, storage, and disposal facility (TSDF) in Model City, Niagara County, New York. This TSDF began operating in 1972 as ChemTrol Pollution Services, Inc. Due to corporate acquisitions and name changes, CWM, a subsidiary of Waste Management, Inc., is the present owner and operator of the facility. Waste Management, Inc. is based in Houston, Texas.

The facility is located on Balmer Road in Model City, New York, approximately 1.9 miles east of New York State Route 18 (Creek Road), and occupies land in the towns of Lewiston and Porter. A Regional Location Map and Facility Location Detail are presented in Figures 1 and 2, respectively. All existing waste management units on the site are located within the Town of Porter. The contiguous property along Balmer Road is also the location of offices for the Administrative, Sales and Marketing, Data Processing, Accounting, Environmental, and Engineering Departments.

The CWM Model City facility is permitted as a TSDF under the Resource Conservation and Recovery Act (RCRA). Numerous units at the site are used to store, treat, and dispose of a variety of liquid and solid organic and inorganic hazardous wastes. Storage, treatment, and disposal capabilities include an Aqueous Wastewater Treatment System (AWTS) utilizing chemical, physical, and biological treatment processes from which treated wastewater is discharged to the Niagara River in accordance with the facility's State Pollutant Discharge Elimination System (SPDES) Permit; secure landfilling of approved waste solids and semisolids, including polychlorinated biphenyls (PCBs); waste stabilization; container and tank storage; transformer decommissioning; and PCB treatment and storage. Figure 3 presents a Facility Layout Plan.

1.2 Project Purpose and Objective

The purpose of this report is to present applicable design and construction information for the proposed Fac Pond 5 secondary containment storage tank (SCS Tank), and to document the results of an assessment conducted by EnSol, Inc. (EnSol) for this tank system. The proposed SCS Tank is a double walled premanufactured High Density Linear Polyethylene (HDLPE) storage tank, to be located in the Fac Pond Riser House at Fac Pond 5. Fac Pond 5 will be a newly constructed surface impoundment constructed with a double liner system. This will include leachate collection and removal system between such liners. Any liquids that reach the secondary containment will drain to a low point or sump and be pumped into the proposed SCS Tank. The SCS Tank will be housed within a Riser House at the top of the perimeter embankment of the fac pond. The proposed tank will be known as T-9001. It is intended that this report be used by CWM to aid in obtaining an approval from the New York State Department of Environmental Conservation (NYSDEC) as per 6 NYCRR 373-2.10(c) to install the tank, piping, and appurtenances, and to operate the SCS Tank system for the purpose stated above.

The objective of the assessment is to satisfy the applicable State and Federal Regulations for the installation of new tank systems as required by CWM's Sitewide Part 373 Permit #9-2934-020022/00097. As required by 6 NYCRR 373-2.10(c)(1), the owner or operator of a new tank system must obtain and submit to the NYSDEC a written assessment attesting that the tank system has sufficient structural integrity and is acceptable for storing hazardous waste.

The following information is included in this report for the proposed SCS Tank system: location, configuration, design parameters, operating procedures, materials of construction, provisions for secondary containment and leak detection, and the results of EnSol's assessment.

1.3 Tank Inspection/Assessment Requirements and Guidelines

An assessment of the subject tank system is required by State and Federal Regulations listed under 6 NYCRR 373-2.10(c) and 40 CFR 264.192, respectively, pertaining to Hazardous Waste Management Facilities. These regulations identify the assessment requirements to be met and associated activities to be performed related to the design and installation of new tank systems or components. The assessment procedure also requires an evaluation of the system design, as it pertains to the containment and detection of releases, in accordance with State and Federal Regulations listed under 6 NYCRR 373-2.10(d) and 40 CFR 264.193, respectively. Additional site-specific permit requirements may also be developed between the owner and the regulatory agencies, such as the CWM Tank and Sump Assessment Schedule included in CWM's Sitewide Permit.

In addition to general regulations and/or site-specific permit requirements, there are several recommended or applicable guidance documents pertaining to tank inspections, assessments, and design. EnSol personnel have used the primary guidance documents referenced below to conduct previous site inspections, assessments, and designs for tank systems, and to aid in the design and assessment contained herein.

- i. Guide for Inspection of Refinery Equipment, Chapter XIII, Atmospheric and Low Pressure Storage Tanks, American Petroleum Institute (API) publication, 4th edition, 1991.
- ii. Tank Inspection, Repair, Alteration, and Reconstruction, API Standard 653, 3rd Edition, December 2001.
- iii. Requirements for Tank and Container Storage, NYSDEC, Technical and Administrative Guidance Memorandum No. 3019, April 23, 1991.
- iv. *Concrete Secondary Containment for Tank and Container Storage*, NYSDEC, Technical and Administrative Guidance Memorandum No. 3021, March 11, 1991.
- v. Chemical Plant and Petroleum Refinery Piping, American Society of Mechanical Engineers (ASME) Standard B31.3-1990

2. Tank Location and Description

2.1 Location

The SCS Tank will be located in the proposed Fac Pond Riser House located along the perimeter berm of Fac Pond 5. Fac Pond 5 will be constructed new as part of the RMU-2 development project. Fac Pond 5 will be located between closed landfills SLF 12 and SLF 7 to the north of the existing Leachate Tank Farm. The location of the fac pond is shown on the set of design drawings by Arcadis included in Appendix A.

2.2 Dimensions and Capacity

The SCS Tank will be a single chamber, dual walled, cylindrical vessel with a flat bottom and a flat roof, with exterior dimensions of 6 feet - 4 inches diameter x 8 feet - 10 inches high. The design capacity of the tank is 1,100 gallons.

2.3 Structural Support and Foundation

The tank will be a free standing flat bottomed tank which will be supported by a 6-inch thick reinforced concrete slab system within the Riser House. The concrete slab will be underlain with a minimum 6-inch thick layer of compacted stone. The tank will not require additional supports or tie-downs as it will not be subject to any wind, snow, significant seismic, or other external loads, however, as an added measure, tie-downs will be included to anchor the tank to the Riser House floor slab using the manufacturer provided cable restraint system or an orequal approved system..

2.4 Materials of Construction

The SCS Tank is a 1,100 gallon High Density Linear Polyethylene (HDLPE) tank manufactured by Snyder Industries, Inc. The design shell thickness will be a minimum 0.187 inches (3/16 inch). Refer to Appendix B for additional design and construction specifications and manufacturers information.

2.5 Miscellaneous Attachments

As shown on the reference drawings in Appendix A, the SCS Tank will have one inlet and one outlet on the top of the tank and one top vent opening with breather valve. Nozzle diameters will all be 2-inches. The tank will also include an 18-inch top manway.

2.6 Process Description, Piping, and Pumping System

The proposed use of the SCS Tank will be for the storage of liquid generated from the secondary collection sump in Fac Pond 5. The liquid will be pumped up the 18-inch diameter HDPE sideslope riser pipe from the secondary collection sump via a submersible pump. The pump will be connected to the tank piping using a 2-inch diameter chemical flex hose. The tank will be equipped with a 2-inch diameter HDPE inlet pipe and flow meter to measure any liquid that is pumped into the tank. The tank will store the liquid until it can be pumped out of the tank via vacuum truck utilizing the 2-inch dip tube on the top of the tank. This liquid will then be transferred to the on-site AWTS for processing.

2.7 Overpressure/Vacuum and Overfill Protection

Primary overpressure/vacuum protection, under normal operating conditions (i.e., tank filling, content withdrawal, and diurnal breathing), will be provided by a 2-inch diameter pipe vent open to the atmosphere.

Overfill protection for the tank is provided by a high level float switch inside the tank. This switch will inhibit the inlet pump and signal an alarm light on the exterior of the building.

2.8 Protective Coatings

The tank is constructed of HDLPE resin and is inherently resistant to corrosion or chemical degradation by the anticipated liquids (Fac pond water) without the addition of any protective coatings. Chemical analysis of Fac Pond water was provided by CWM and is included in Appendix B. The tank will be housed within the Riser House, which is a heated structure; therefore, the tank will not require any additional external coatings to protect it from UV degradation or other environmental factors. Manufacturer's Specifications, including chemical resistance data and chart are included in Appendix B.

2.9 Secondary Containment and Leak Detection

Secondary containment for the SCS Tank is provided by a double walled tank construction. In the event of a leak from the primary tank, the liquid would be contained within the secondary tank. The tank's double walled design meets all volume requirements for secondary containment and will provide a minimum of 100% of the normal fill capacity of the primary tank.

Leak detection for the SCS Tank will be provided by an electronic moisture sensor placed within the interstitial space of the double walled tank. This sensor will activate a visible alarm (light) on the exterior of the Riser House which will be seen by visual means through daily inspection by CWM personnel. The tank sides, top, nozzles, and system piping are all visible for easy inspection. A drain valve located near the bottom of the secondary containment tank wall will also be available to check for liquids in the secondary containment area as an additional measure.

3. Assessment and Certification

EnSol conducted an assessment and review of the proposed SCS Tank system components at CWM's Model City facility in order to assess the integrity and to confirm the compatibility of the components with materials that are to be handled.

3.1 Design and Record Information

EnSol reviewed available design and record information that were provided by CWM and/or the various equipment and tank manufacturers. Information regarding design standards, materials of construction, structural supports, hazardous characteristics of the waste stream to be handled, and corrosion protection systems (internal and external) was obtained from these sources. EnSol did not perform compatibility studies or materials testing for the proposed system components, however; a close review and comparison of the system's specific materials of construction compared to available manufacturers published chemical compatibility and resistance data, tables, charts, and test results clearly indicates adequate compatibility with the materials expected to be handled and no chemical compatibility issues are expected. It is also noted that EnSol's extensive familiarity and experience with these materials (see Appendix C) in similar applications at CWM and elsewhere, combined with our knowledge of the materials/liquids expected to be handled within the Fac pond allows EnSol to judge the tank materials of construction to be compatible with the waste to be stored.

3.2 Summary and Conclusions

The SCS Tank system is to be used by CWM for the storage of liquids generated from the secondary containment sump in proposed Fac Pond 5. Chemical analysis of the Fac pond water typically handled, provided by CWM, does not contain constituents or concentrations harmful to the tank or piping systems. The proposed tank was specified and designed as a chemical-resistant tank that will provide maximum performance, within the specified limits, to contain aggressive chemicals at atmospheric pressures. The tank is expected to meet or exceed the conditions it will be exposed to.

In accordance with the requirements listed under 6 NYCRR 373-2.10(c)(2), the new tank system will be inspected by an independent, qualified, installation inspector or registered New York Professional Engineer prior to placing the system in use. During start up CWM will visually inspect the system components to insure they are free of leaks and any deficiencies immediately addressed.

The assessment for the proposed SCS Tank system, as prepared by EnSol and presented in this report, includes consideration of the proposed tank's foundation, structural supports, secondary containment, leak detection, tank design standards, proposed equipment, and existing conditions. EnSol considers each of these items to be adequately designed and/or constructed for the intended use and, where applicable, to have sufficient structural strength. Proposed materials of construction for the systems appear to be sufficiently compatible with the materials expected to be handled. Considering the proposed use and service, the proposed tank system identified herein were judged by EnSol to be adequate for its intended service, providing the tank system operating temperature and chemical exposure limitations are not exceeded.

TANK SYSTEM DESIGN AND ASSESSMENT REPORT FOR FAC POND 5 TANK T-9001

CWM Chemical Services, LLC Model City, New York Facility

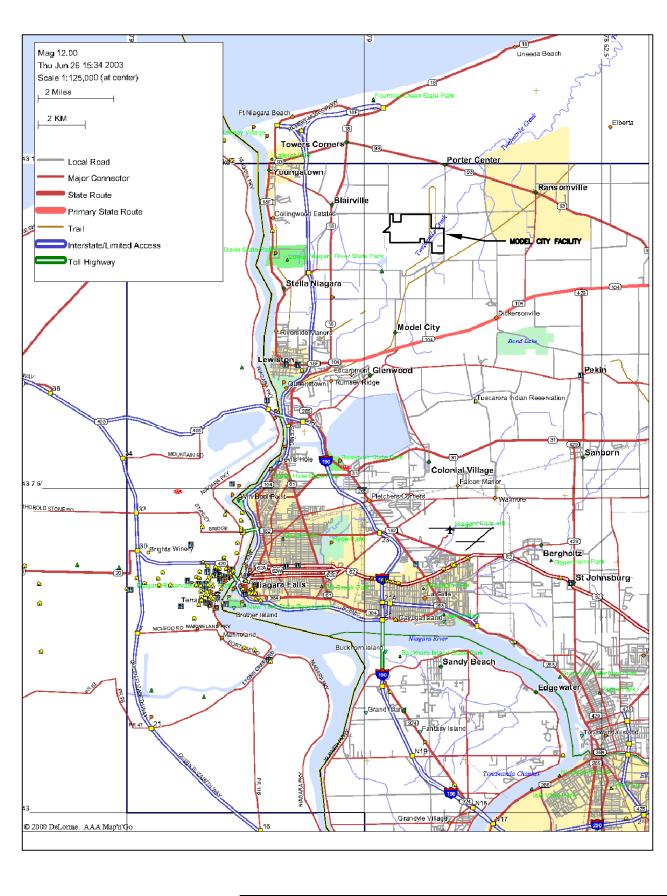
CERTIFICATION

I certify under penalty of law that this document and all attachments were prepared under my direction or supervision according to a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate and complete. I am aware that there are significant penalties for submitting false information, including the possibility of the and impresonment for knowing violations.

Brian D. Shiah, P.E. ENSOL, INC.

 $\frac{11/7/13}{\text{Date}}$

Figures





EnSol, Inc.

Environmental Solutions

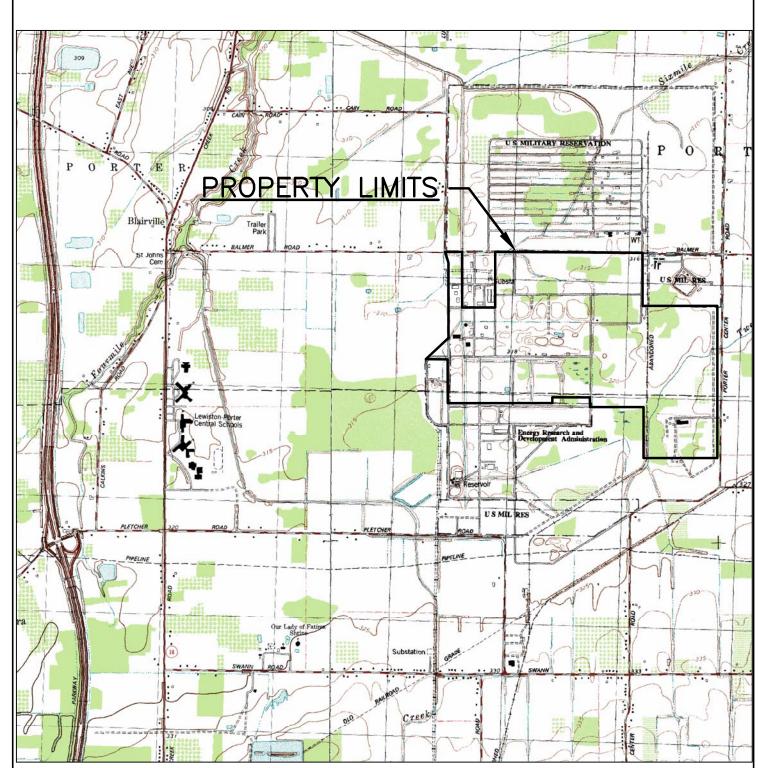
661 MAIN STREET NIAGARA FALLS, NY 14301 PHONE (716) 285-3920 FAX (716) 285-3928

REGIONAL LOCATION MAP

CWM CHEMICAL SERVICES, LLC. MODEL CITY, NY

FIGURE

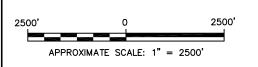
1



REFERENCE: BASE MAP USGS QUADS.,7.5 MINUTE SERIES RANSOMVILLE AND LEWISTON, NY 1980.

NOTES:

- 1. PROPERTY LINES ARE APPROXIMATE.
- 2. NO DRINKING WATER WELLS EXIST WITHIN 1/4 MILE OF THE FACILITY.
 3. THE TREATED EFFLUENT DISCHARGE IS LOCATED AT THE
- NIAGARA RIVER (SHOWN ON USGS LEWISTON QUADRANGLE).
- 4. 710 TOTAL ACRES5. 630 RCRA PERMITTED ACRES.



EnSol, Inc. **Environmental Solutions**

661 MAIN STREET

NIAGARA FALLS, NY 14301

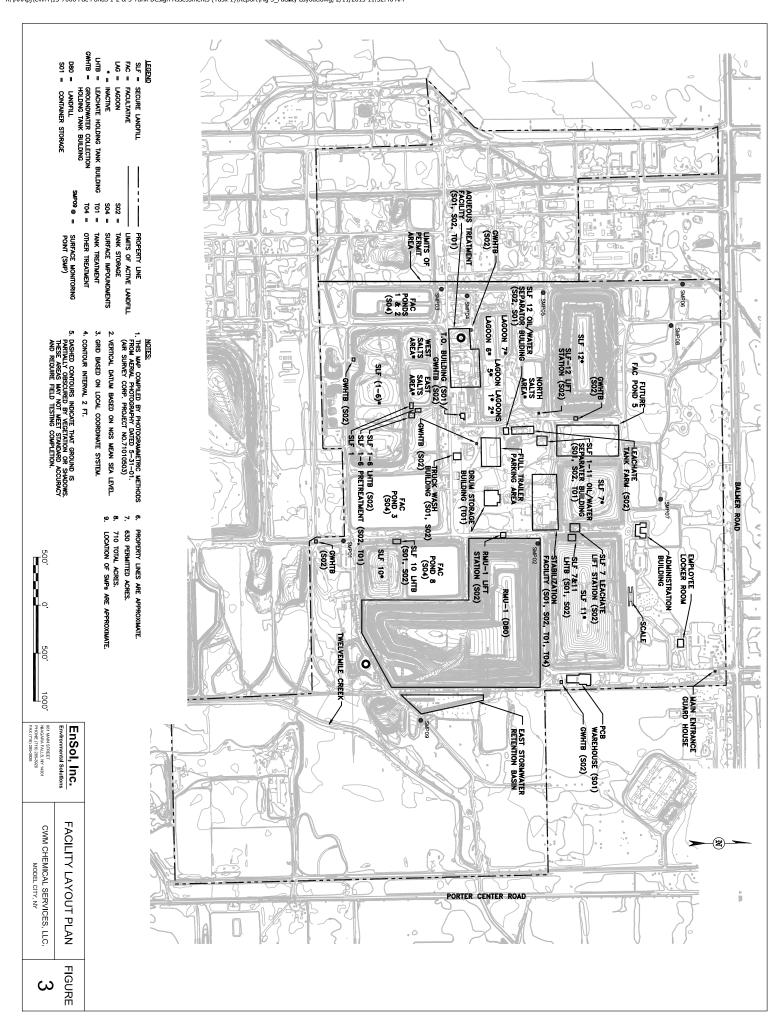
PHONE (716) 285-3920 FAX (716) 285-3928

FACILITY LOCATION MAP

CWM CHEMICAL SERVICES, LLC. MODEL CITY, NY

FIGURE

2



Appendix A

Proposed Fac Pond 5 Permit Drawings (Arcadis)

PERMIT DRAWINGS

FAC POND 5 PERMIT DRAWINGS

CWM CHEMICAL SERVICES, LLC MODEL CITY, NIAGARA COUNTY NEW YORK

FEBRUARY 2013



INDEX TO DRAWINGS

- TITLE AND INDEX
- FAC POND GRADING PLAN

- SITE ELECTRICAL FEED RELOCATION PLAN SITE WATER SUPPLY RELOCATION PLAN
- FAC POND RISER HOUSE MECHANICAL INSTALLATION DETAILS
- FAC POND RISER HOUSE ELECTRICAL INSTALLATION DETAILS
- VALVE HOUSE DETAILS
- FAC POND TRANSFER PIPELINE DETAILS

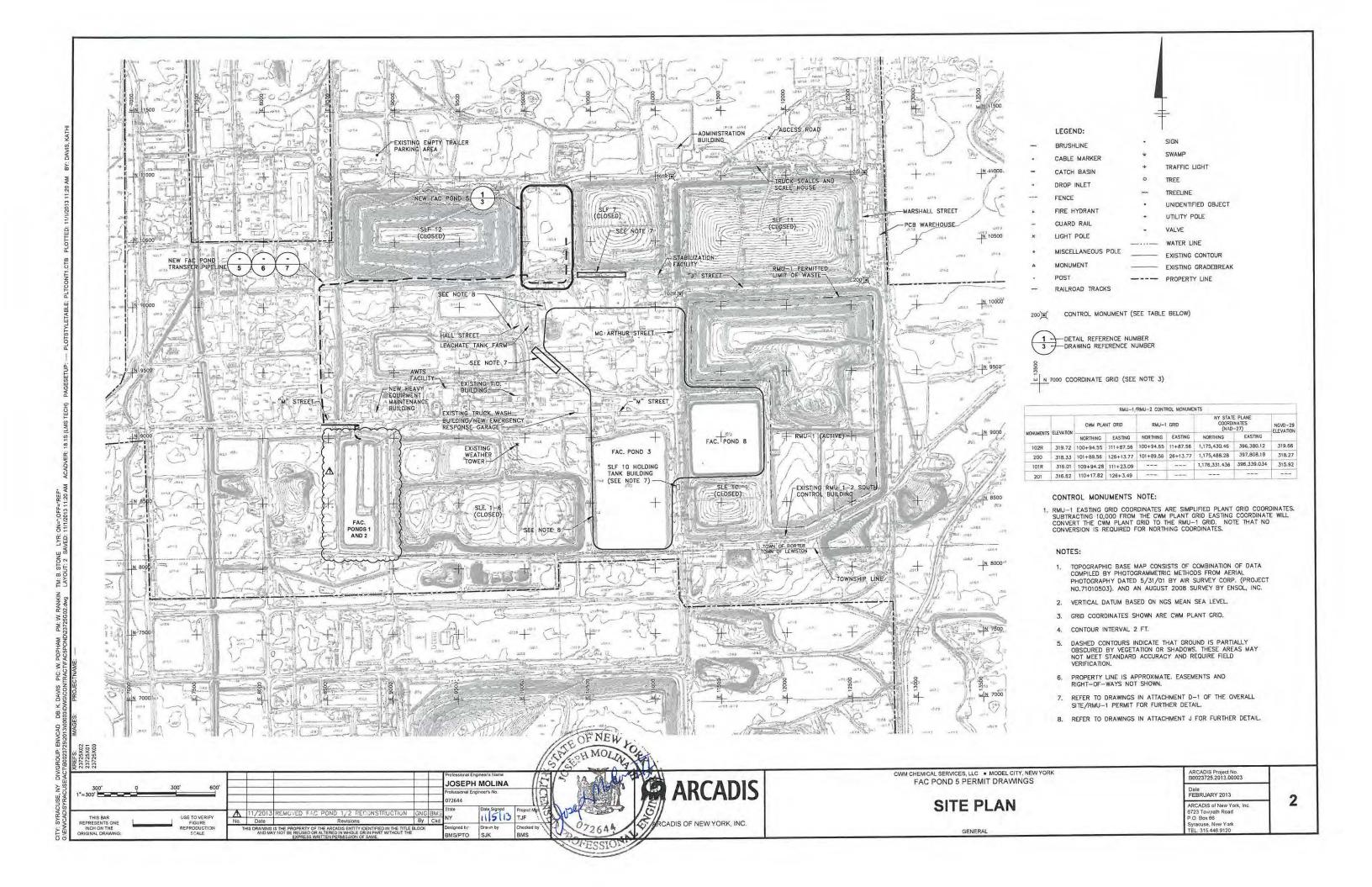
JOSEPH MOLINA **ARCADIS** NOT TO SCALE CADIS OF NEW YORK, INC.

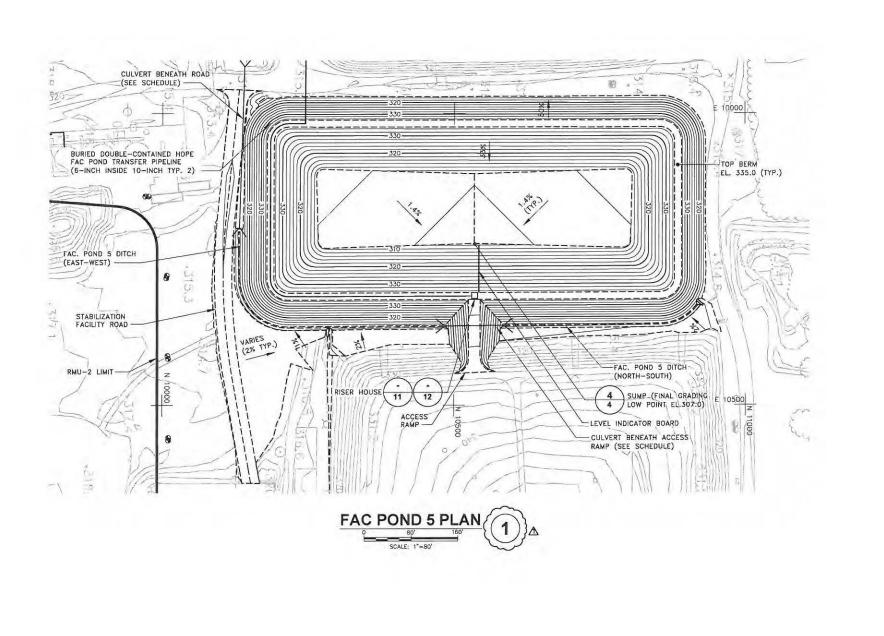
CWM CHEMICAL SERVICES, LLC • MODEL CITY, NEW YORK FAC POND 5 PERMIT DRAWINGS

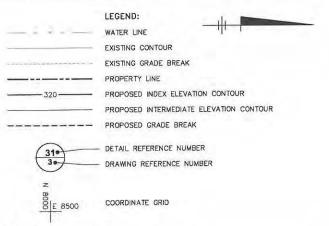
TITLE AND INDEX

ARCADIS of New York, Inc

1



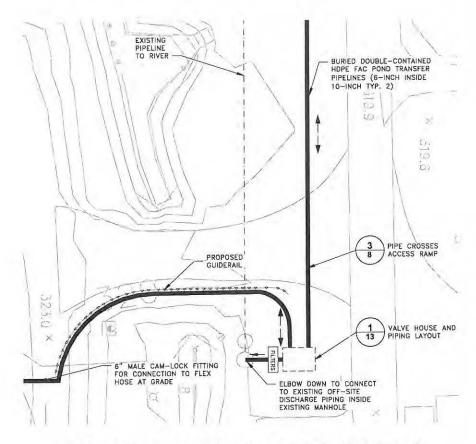




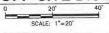
NOTES:

- SEE DRAWING 2 FOR BASEMAP INFORMATION.
- PROPOSED GRADES REPRESENT FINAL GRADING (TOP OF BALLAST LAYER ON FLOOR AND TOP OF PRIMARY LINER ON INTERIOR SIDESLOPES).

CULVERT ID	SIZE	SLOPE %
BENEATH ACCESS RAMP	24"	0.3%
BENEATH ROAD	36"	0.3%









ARCADIS Project No B0023725.2013.00003

ARCADIS

CWM CHEMICAL SERVICES, LLC • MODEL CITY, NEW YORK FAC POND 5 PERMIT DRAWINGS

FAC POND GRADING PLAN

ARCADIS of New York, Inc. 6723 Towpath Road P.O. Box 66 Syracuse, New York TEL. 315.446.9120

3

SCALE(S) AS INDICATED

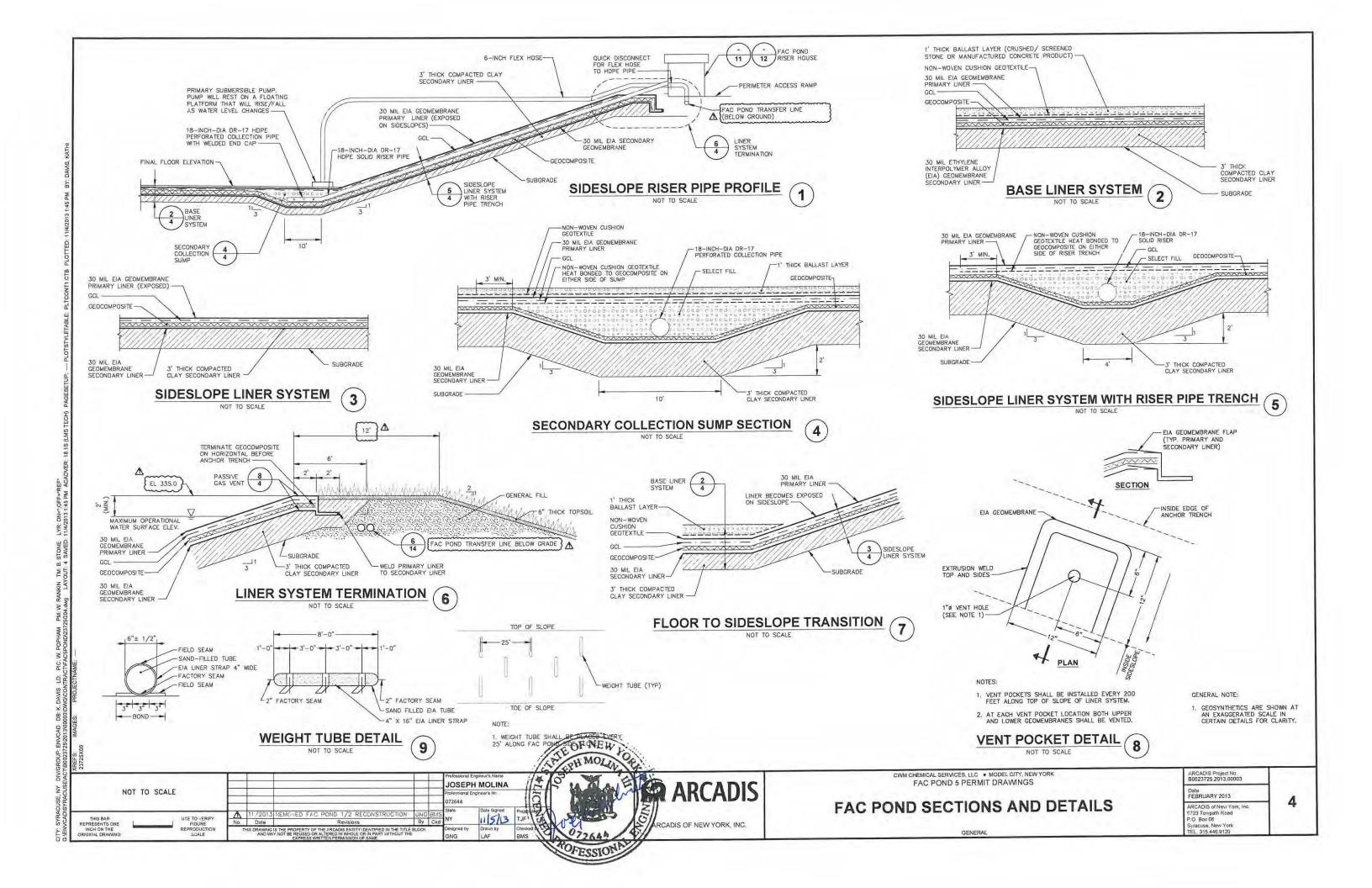
USE TO VERIFY FIGURE REPRODUCTION SCALE

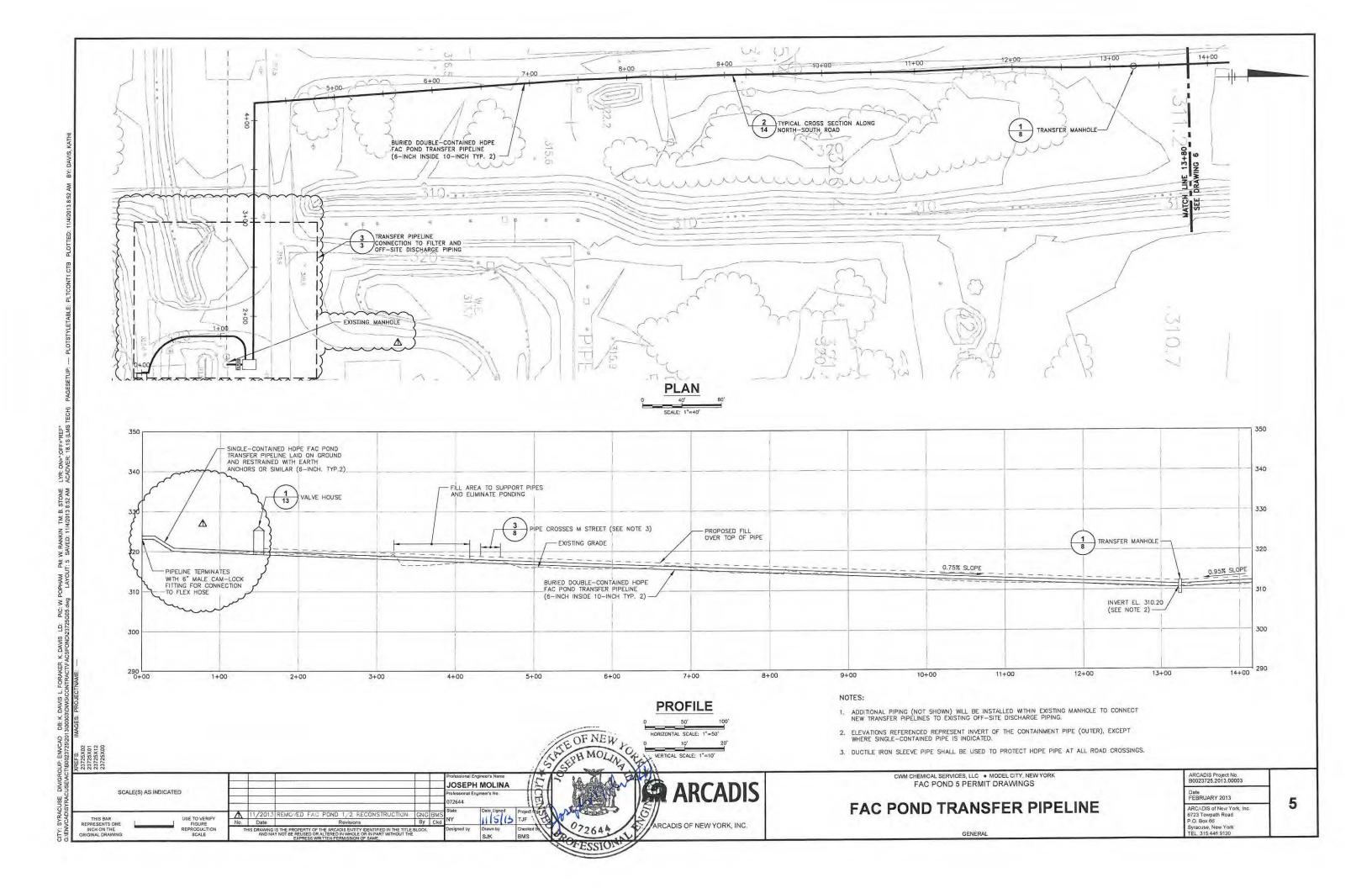
11/2013 F No. Date

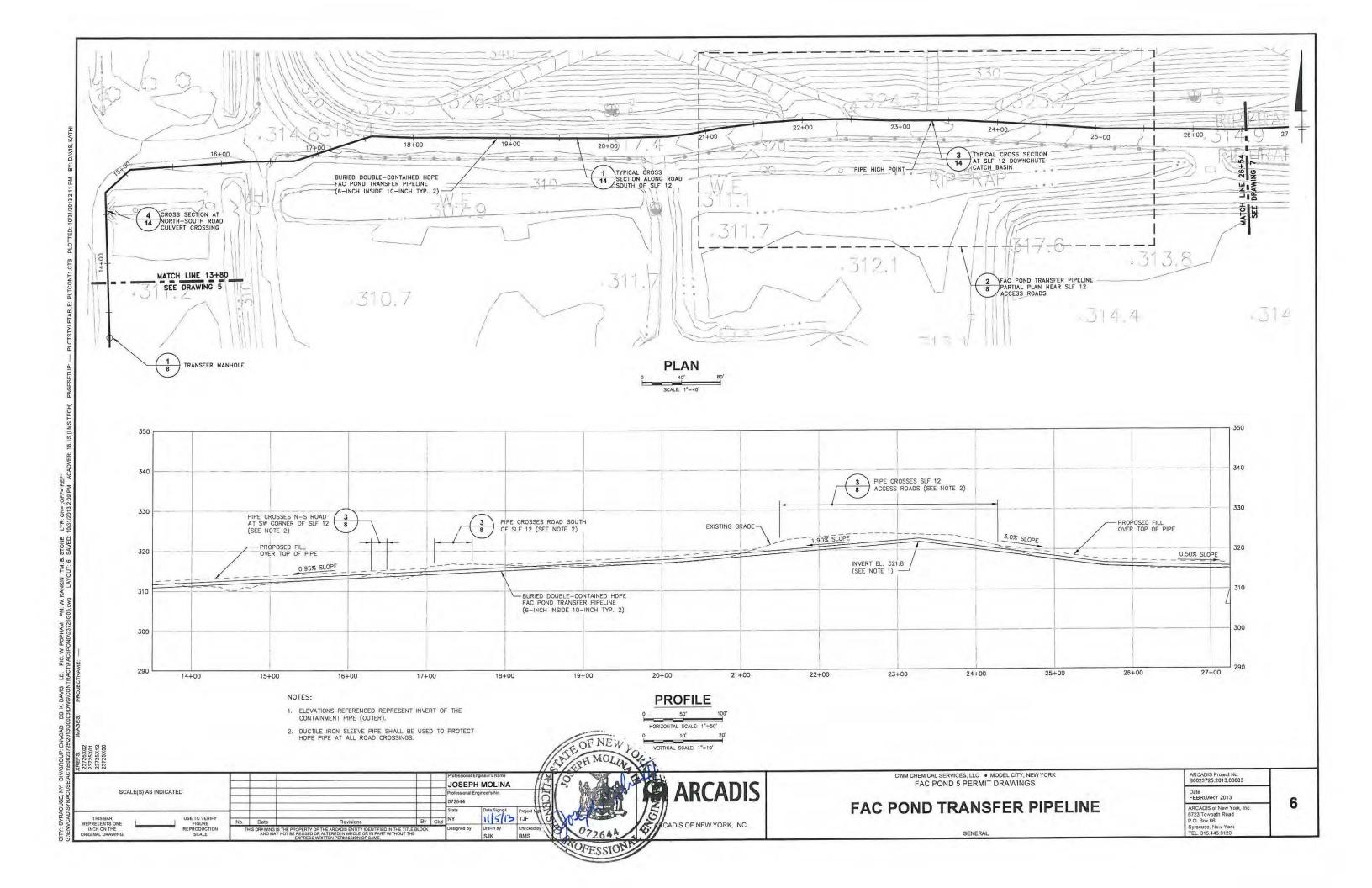
Date Signed Project Mal

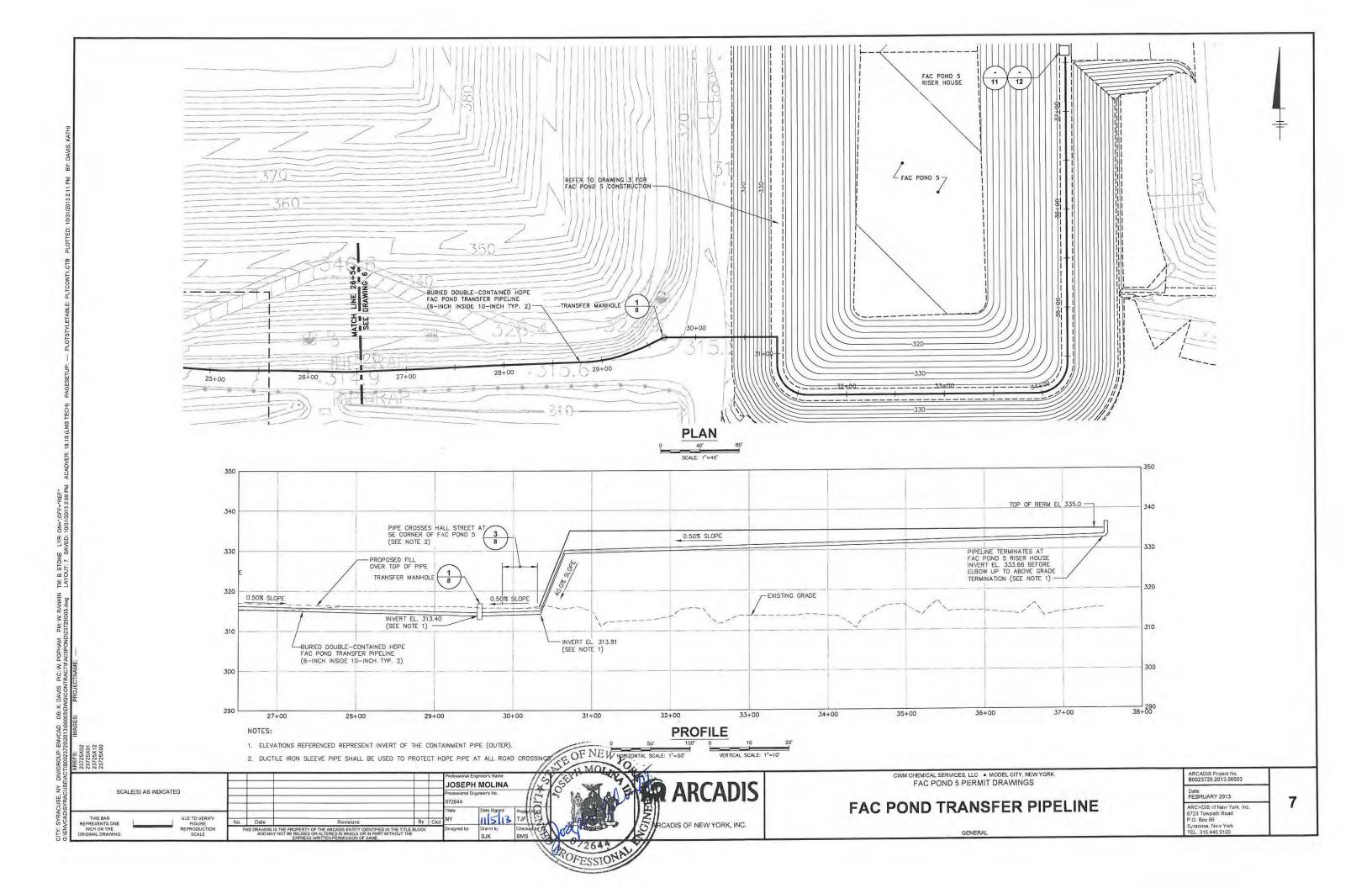
JOSEPH MOLINA

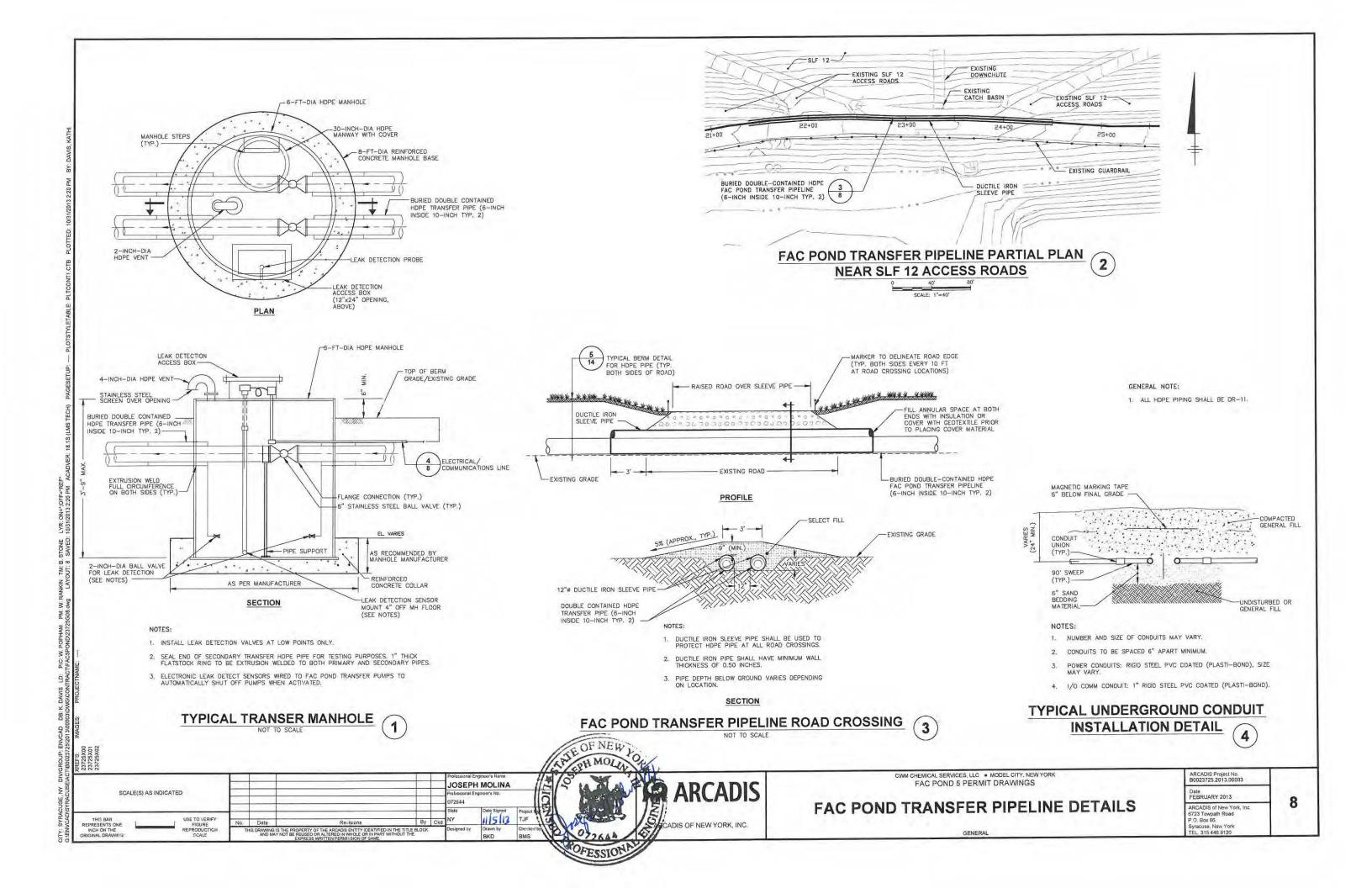
ARCADIS OF NEW YORK, INC.

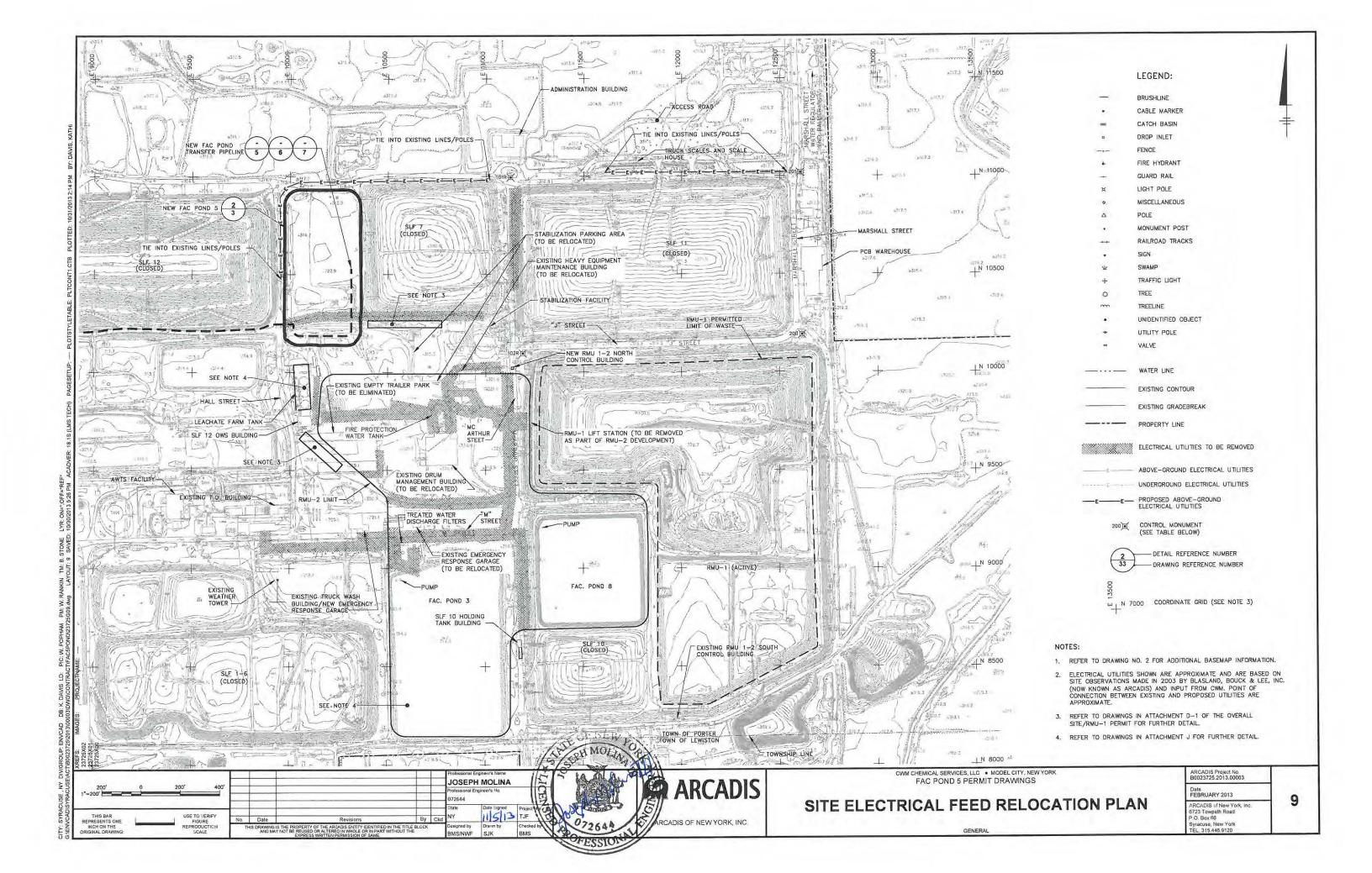


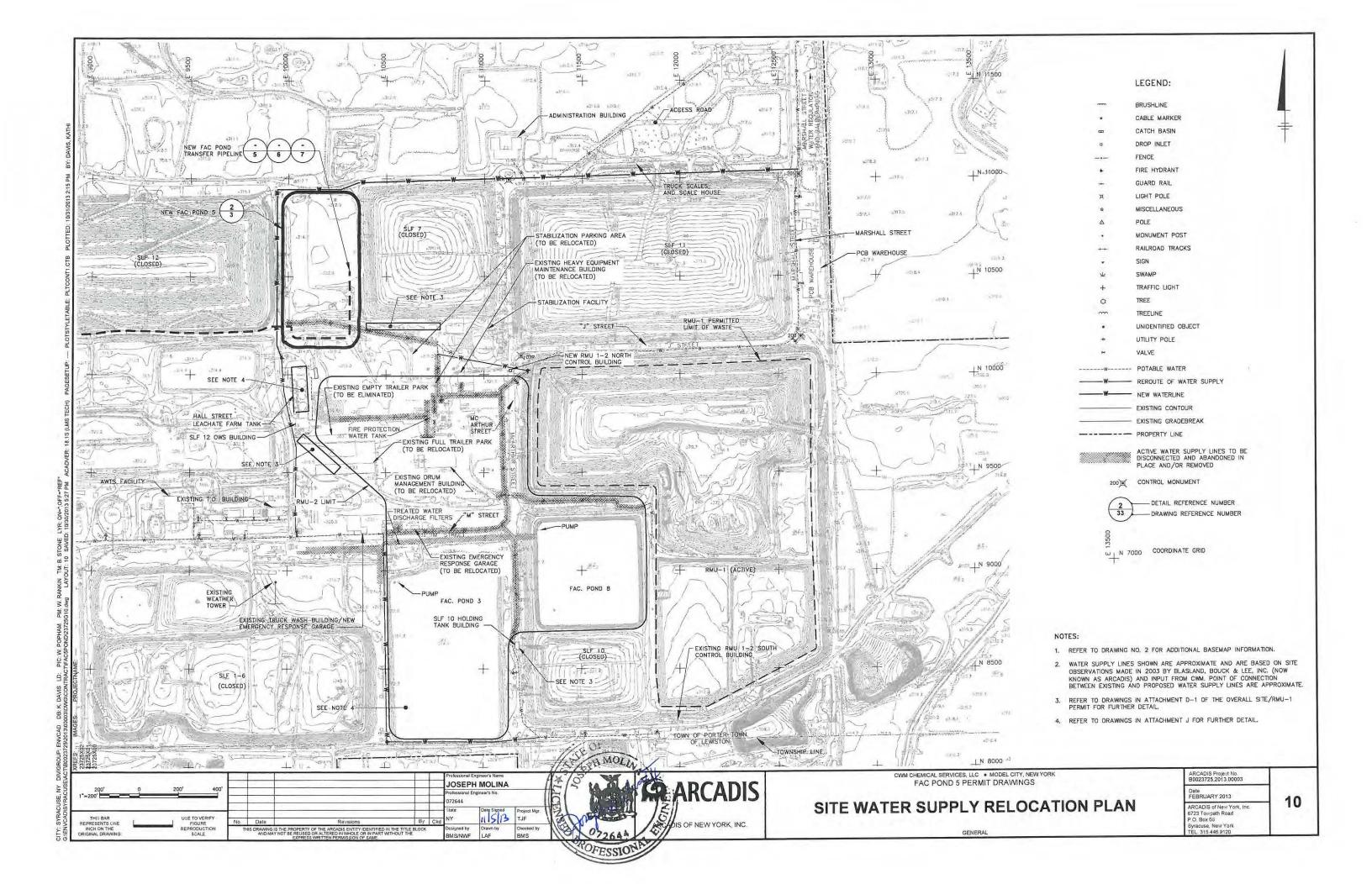


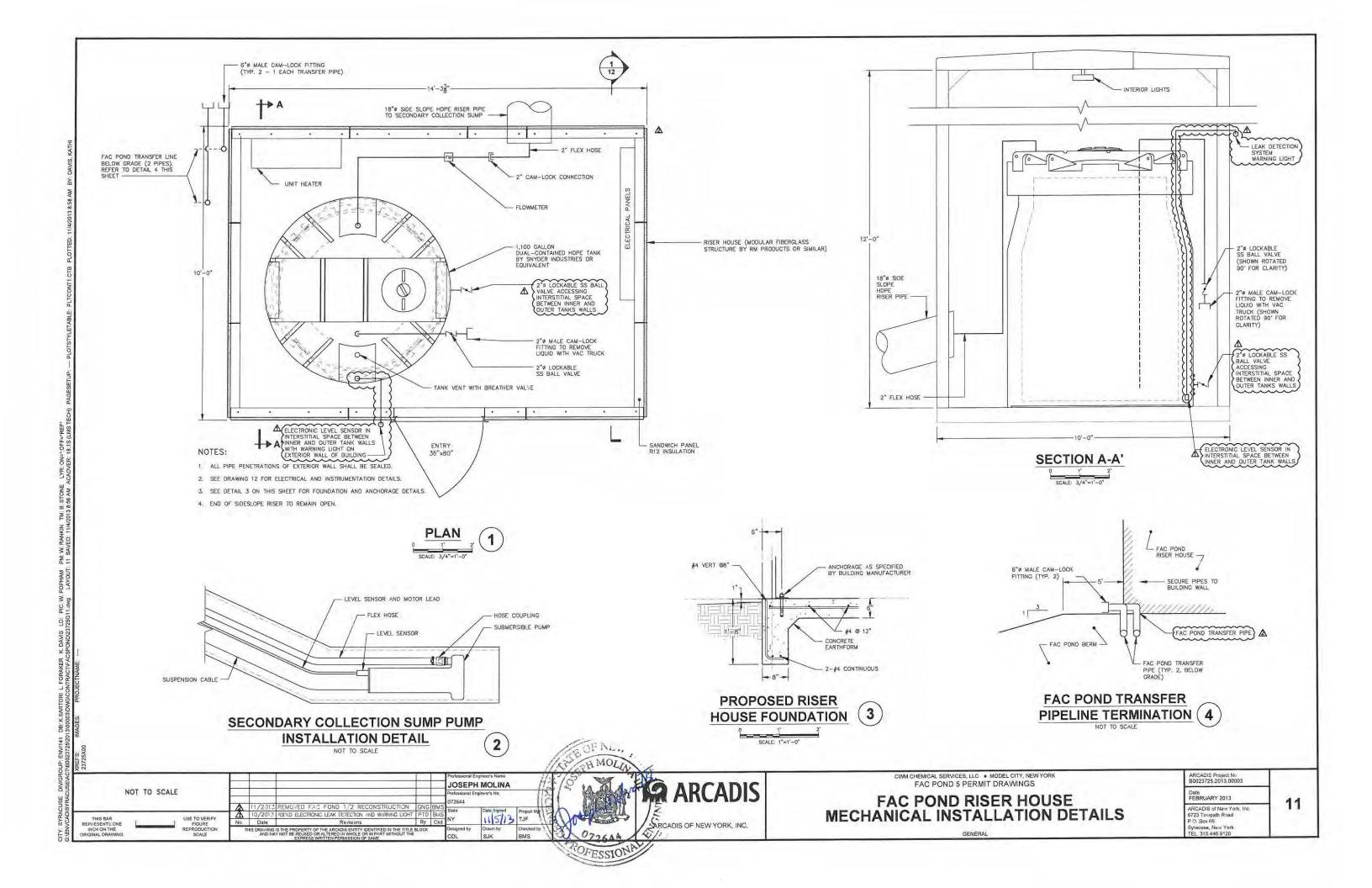


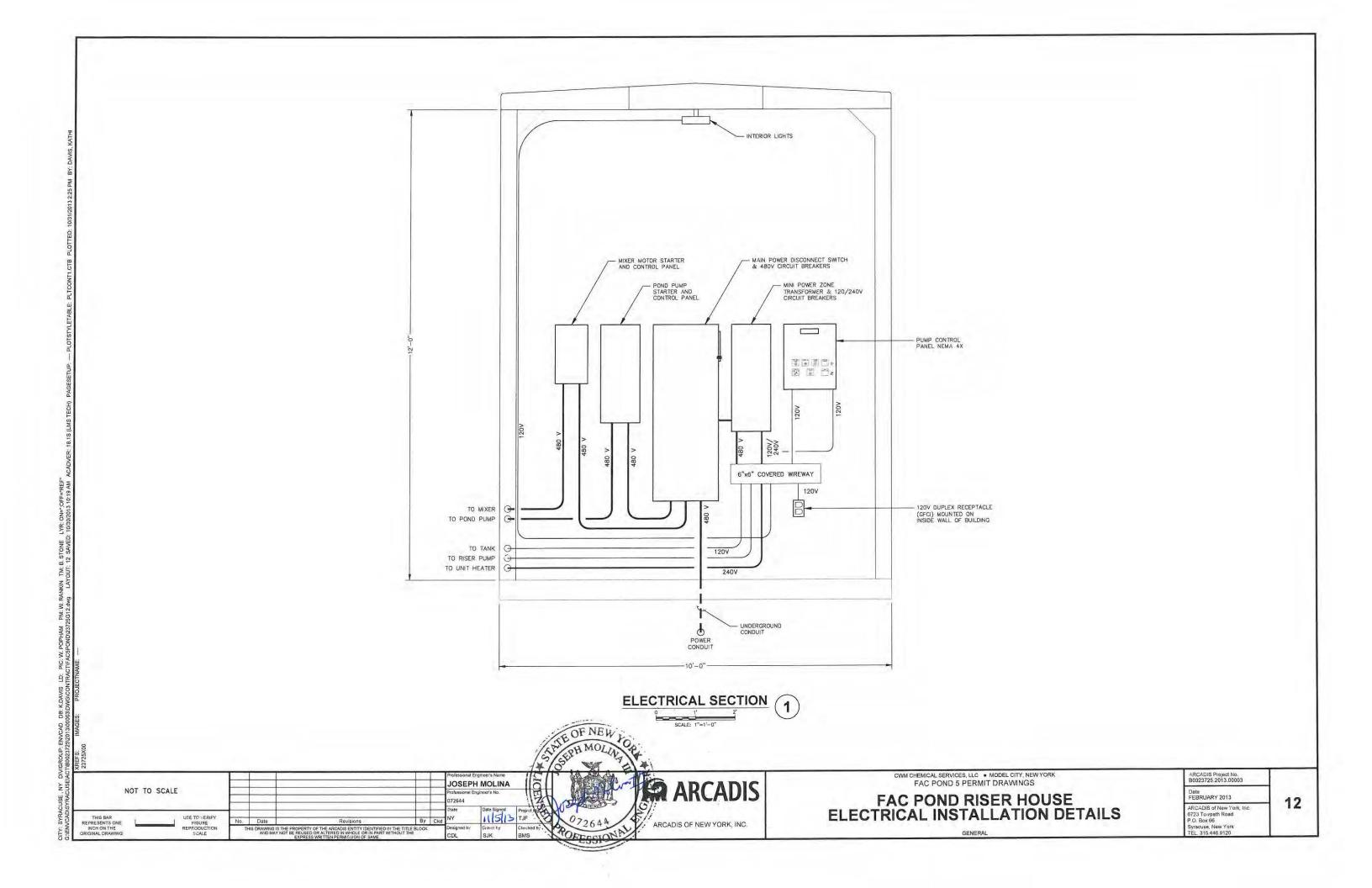


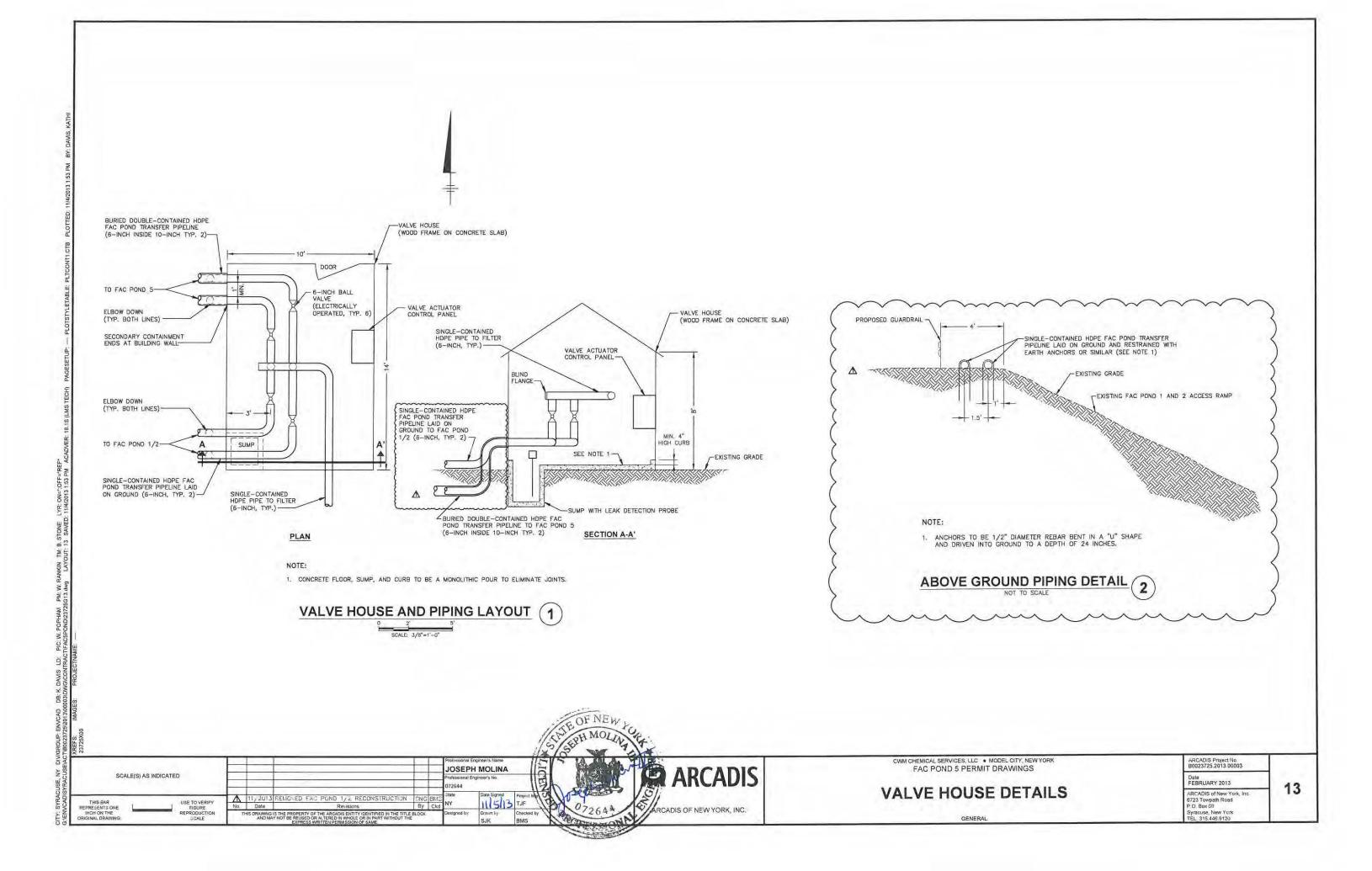


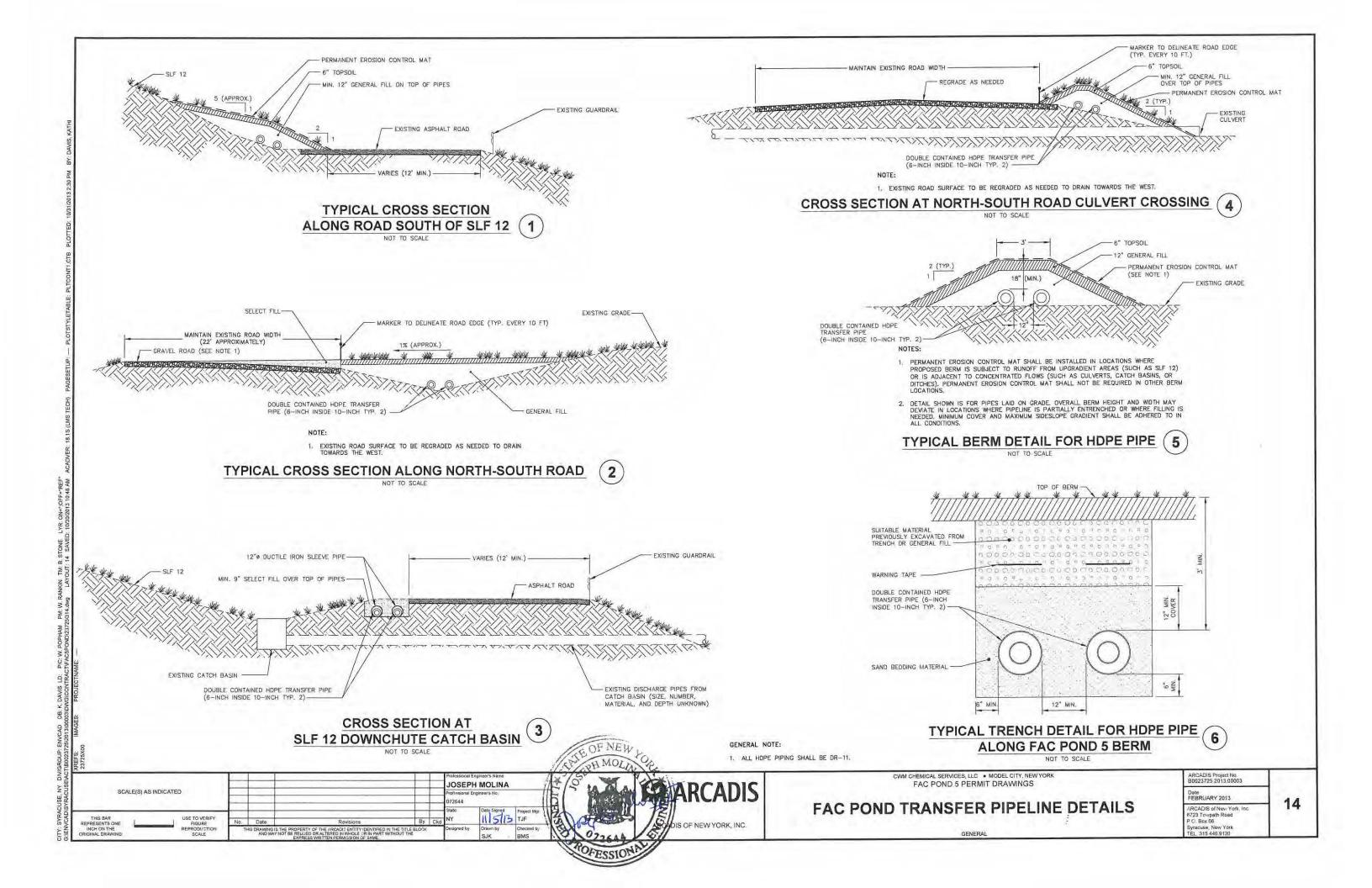












Appendix B

Proposed Secondary Containment Storage Tank Information (Snyder)

Tank Product Data

(Snyder)

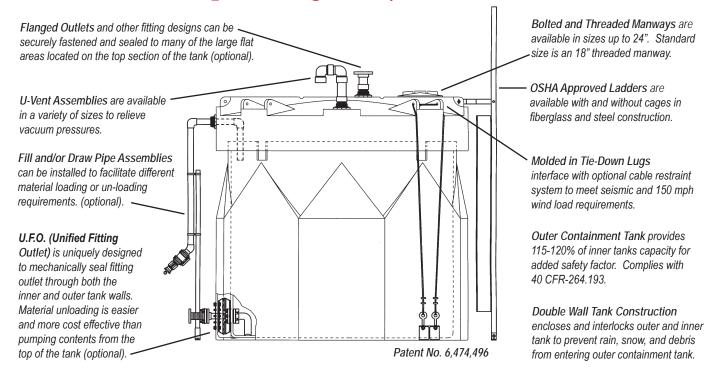
Captor Containment



www.snydernet.com

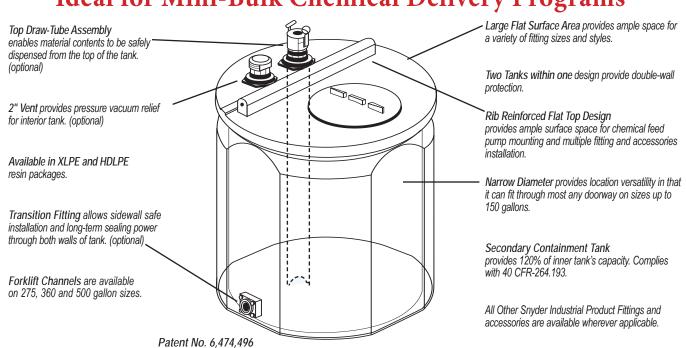
Captor Containment System

Protects Bulk Storage Profits Without Jeopardizing Safety or the Environment



Mini-Captor Containments

Double Wall Tank System Ideal for Mini-Bulk Chemical Delivery Programs



Captor Options/Accessories



Leak Detection Sensor Capacitive proximity sensor detects and communicates the smallest of leaks with an easy to understand warning signal.



Level Indicator Ultrasonic level indicator with digital display measures the inner tank's slightest liquid level changes.



Fill Pipe Assembly
Modified to accommodate
double wall construction and
take advantage of our outer
containment capability.



Other Options
Bolted and sealed manways,
heat trace and insulation, and
most other Snyder tank fittings
and accessories.



Transition Fitting U.F.O. (Unified Fitting Outlet) design allows side wall fittings to be installed and safely sealed through both walls of the Captor Containment System.



Seismic Restraints and Ladders Molded-in tie-down lugs and cable tie-down system meet seismic and 150 mph wind load requirements. OSHA-approved ladders are also available.

Tank Material Options High Density linear polyethylene (HDLPE) or cross-linked polyethylene (XLPE).

SPECIFICATIONS

Captor Containment System							
Part No.	Gallons	Diameter	Height				
504/503	550	76"	65"				
547/545	1,100	76"	104"				
549/546	1,550	76"	136"				
557/550	2,000	102"	103"				
558/551	2,500	102"	122"				
559/552	3,000	102"	142"				
560/553	3,500	102"	158"				
561/554	4,000	102"	178"				
562/555	4,500	102"	197"				
563/556	5,000	102"	216"				
566/564	5,500	120"	172"				
567/565	6,500	120"	199"				
10064/10065	8,700	142"	197"				
10066/10067	10,000	142"	226"				



All Snyder specific gravity ratings meet or exceed ASTM D-1998. Consult your Snyder representatives on material construction recommendations for your company's particular application.

Mini-Captor Options/Accessories



Leak Detection Sensor Capacitive proximity sensor detects and communicates the smallest of leaks with an easy to understand warning signal.



Forklift and Pallet Jack Accessible Design Larger 275, 360 and 500 gallon sizes are equipped with forklift channels designed to help move the containers when full and empty.



Transition Fitting
Allows safe sidewall installation and longterm sealing power through both walls of tank.



Level Indicator Ultrasonic level indicator with digital display measures the inner tank's slightest liquid level changes.



Mini-Captor tank systems (35-275 gals.) can be mounted on elevation stands, creating more room for plumbing and other system requirements without utilizing additional floor space. Patent No. 7,059,575



Other Fittings and Accessories All applicable Snyder Industries fittings and accessories can be integrated to complete tank system.

Tank Material Options High-density linear polyethylene (HDLPE) or cross-linked polyethylene (XLPE).

SPECIFICATIONS

Mini-Captor Tank Systems						
Part No.	Gallons	Diameter	Height	Lid		
1010100N	15	23"	23"	8"		
1010300N	30	23"	35"	8"		
1000200N	35	22"	36"	6"		
1010500N	55	28"	36"	8"		
1000300N	60	26"	41"	14"		
1010700N	100	33"	44"	8"		
5980000N	120	34"	49"	14"		
1010900N	140	32" X 32"	48"	8"		
1000400N	150	34"	60"	14"		
1000500N	275	47"	60"	14"		
1000600N	360	53"	60"	14"		
1000800N	500	53"	79"	14"		

Double Strength Protection

Protect Your Liquid Assets!

Regulation is becoming increasingly stringent in the formulation and enforcement of chemical containment legislation. Berm and tank-in-a-basin containment systems, thought to be modern, are now found to be inadequate and not compliant.

There is an answer. Snyder's polyethylene tanks with secondary containment systems can safely store a wide range of hazardous chemicals. Our double wall (tank-in-a-tank) designs are being increasingly utilized as a supplement or alternative to secondary containment requirements. The design features built into Snyder's Captor and Mini-Captor Tank Systems increase safety and protect the environment without jeopardizing your profits.



Consider the Benefits...

- Tank-in-a-tank design provides TOTAL containment protection in one space-saving unit.
- The system consists of a primary tank with a secondary outer containment tank with a capacity
 of 115%-120% of the inner tank's capacity, exceeding EPA standards.
- Double-wall construction is completely enclosed so that external matter such as rainwater, snow and debris is prevented from collecting in the outer containment tank making it ideal for outdoor chemical storage.
- Shipped fully-assembled on either a standard or wide-load flatbed trailer which reduces field assembly costs.
- Available in sizes ranging from 15 to 10,000 gallons.
- Available in High Density Linear Polyethylene (HDLPE) or Cross Link Polyethylene (XLPE) construction. Having a choice provides ultimate chemical compatibility and performance.
- Tanks designed with wall thickness equal to or greater than ASTM D-1998 standards.

Your Snyder Double Wall Tank can be customized with these options...

- Seismic restraint system (for 35-10,000 gallon sizes).
- 150 MPH wind load restraint system (for 35-10,000 gallon sizes).
- Ultrasonic level indicators.
- · Leak detection sensors.
- Heat tracing and insulation.
- OSHA compliant ladders (for 550 -10,000 gallon sizes).
- Variety of manway sizes and styles.
- · Bottom sidewall outlets.
- Top inlet connections and vents.

SOLUTIONS IN BULK HANDLING



Transportation containers hold from 60 to 550 gallons.

UN/DOT-APPROVED IBCs

Snyder intermediate bulk containers (IBCs) are durable, corrosion-resistant and economical. These long-term, reusable containers are ideal for the transportation of both hazardous and non-hazardous liquid materials.



Stationary tanks store from 8 to 16,500 gallons.

BULK STORAGE & PROCESSING TANKS

For larger stationary applications, Snyder offers the industry's broadest range of tanks – from 8 to 16,500 gallons – in shapes that meet your specific needs. To match your special function requirements, we also market a complete line of accessories, such as stands, seismic tie-downs, ladders, fittings, gaskets, sight gauges, heat tracing and insulation.



Customized mini-bulk containers

CUSTOM CONTAINER DESIGNS

In addition to Snyder's extensive standard product offering, some of our greatest success stories stem from custom container designs to meet specific customer requirements. Snyder's engineering team is a recognized leader in design innovation, and is driven to work with customers to develop the best performing container at the lowest possible cost.

ONE SOURCE DOES IT ALL

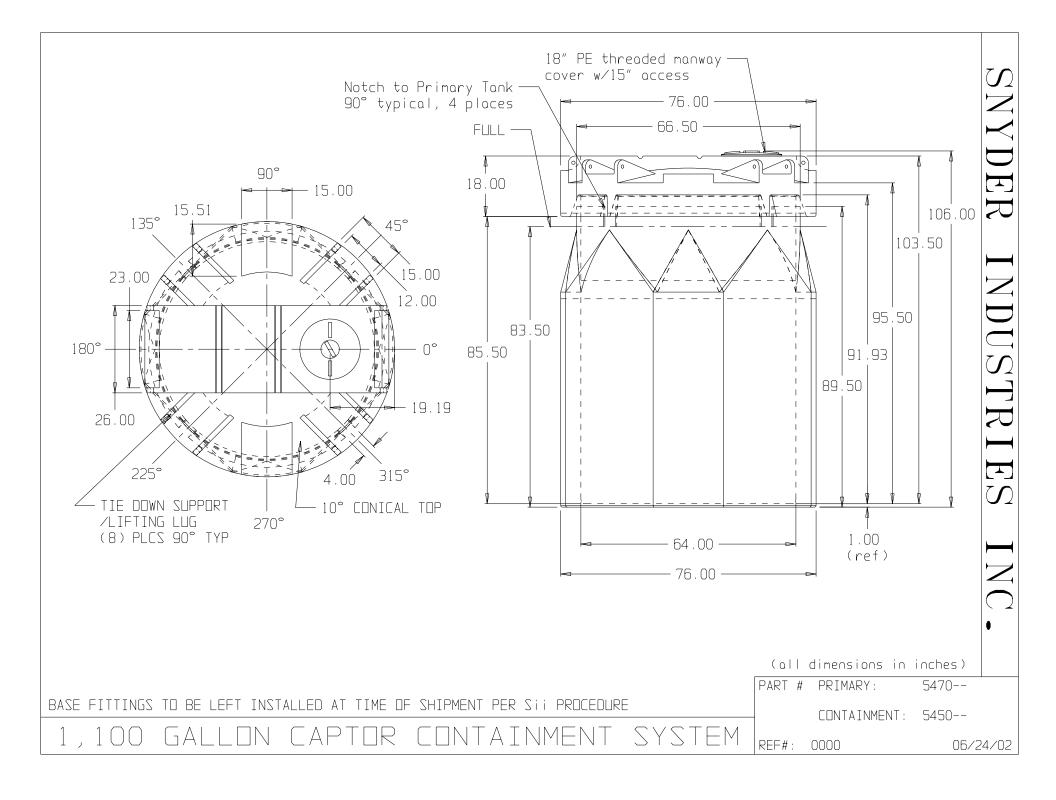
Whether you are a manufacturer or distributor, Snyder Industries can help you improve the function, economics and performance of your company's bulk handling systems.



SOLUTIONS IN BULK HANDLING

P.O. Box 4583 • Lincoln, Nebraska 68504 • 402-467-5221 • FAX: 402-465-1220 • www.snydernet.com • email: sales@snydernet.com

Other manufacturing facilities: Marked Tree, Arkansas * Chowchilla, California * Philippi, West Virginia * Mancelona, Michigan





ExxonMobil™ HDPE HD 8660 Series **High Density Polyethylene Resin**

Product Description

HD 8660 Series are high density hexene copolymers designed to offer superior toughness and stiffness. They are ideally suited for applications that require the optimum balance of low temperature toughness, creep resistance, stiffness, ESCR, and tear properties.

General				
Availability 1	Latin America	North America	South America	
Additive	 HD 8660.29: Long Term UV-15 Stabilizer: Yes 	HDP8660.29: Long Term UV-15 Stabilizer: Yes		
Applications	 Industrial Products 	Intermediate Bulk Containers	Large Agricultural Tanks	
Revision Date	• July 2011	and Dank Goridaniers	- Large Agriculturar ranks	
Resin Properties	Typical Value (English) Typical Value (SI)	Test Based Or	
Density	0.942 g/cm³	0.040 -/-		

Resin Properties	Typical Value	(English)	Typical Value	(SI)	Test Based On
Density		g/cm³		g/cm³	
Melt Index (190°C/2.16 kg)		g/10 min		_	ASTM D4883
(2.0	g/10 min	2.0	g/10 min	ASTM D1238
Thermal	Typical Value	(English)	Typical Value	(SI)	Test Based On
Deflection Temperature Under Load (DTUL) at 66psi - Unannealed					ASTM D648
	153	°F	67	°C	
Deflection Temperature Under Load (DTUL) at 264psi - Unannealed			.	Ü	ASTM D648
	106	°F	41	*C	
Melting Temperature	264	°F	129	°C	ASTM D3418
Molded Properties	Typical Value	(English)	Typical Value	(SI)	Test Based On
Tensile Strength at Yield			7,5,001 70100	(01)	
2.0 in/min (51 mm/min)	3000	nsi	20	140	ASTM D638
Elongation at Yield		•		MPa	
Floring March 1 407 6	20	%	20	%	ASTM D638

Environmental Stress-Crack Resistance	130000	psi	890	MPa	ASTM D790B ASTM D1693A
10% Igepal, F50	50	hr	50	hr	AS TWI D TOSSA
100% Igepal, F50	550	hr _	550		
Impact	Typical Value	(English)	Typical Value	(SI)	Test Based On
Impact Strength				()	ARM
-40°F (-40°C), 0.125 in (3.18 mm)	80	ft·lb	108	Л	VIVIAI
0.250 in (6.35 mm)	180	ft·lb	244	-	

130000 psi

Additional Information

Flexural Modulus - 1% Secant

All physical properties were measured on 3 mm. rotomolded samples unless a different value is shown, except for ESCR, which was measured on compression molded samples,

Tensile testing was conducted at a crosshead speed of 50 mm/min. The tensile strength reported refers to the maximum stress reached

the test.

Test procedures may be modified to accommodate operating conditions or facility limitations.

Typical properties: these are not to be construed as specifications.

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ExxonMobil Chemical ExxonMobil™ HDPE HD 8660 Series High Density Polyethylene Resin

Legal Statement

Contact your ExxonMobil Chemical Customer Service Representative for potential food contact application compliance (e.g. FDA, EU, HPFB).

This product is not intended for use in medical applications and should not be used in any such applications.

Notes

¹ Product may not be available in one or more countries in the identified Availability regions. Please contact your Sales Representative for complete Country Availability.

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Worldwide and the Americas ExxonMobil Chemical Company 13501 Katy Freeway Houston, TX 77079-1398 USA 1-281-870-6050 Asia Pacific ExxonMobil Chemical Singapore Pte. Ltd. 1 HarbourFront Place #06-00 HarbourFront Tower One Singapore 098633 86 21 240-75380

Europe, Middle East and Africa ExxonMobil Chemical Europe Hermeslaan 2 1831 Machelen, Belgium 420-239-016-274

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Snyder Specification #199901

Snyder Industries, Inc. Specification #199901 For Polyethylene Upright Double Wall Storage Tanks (10-19-2012)

1. Scope

- 1.1 This specification covers upright, double wall, flat bottom storage tank assemblies. The assembly consists of one cylindrical inner primary tank and one blended form octagonal outer secondary tank. Each tank is molded in one-piece seamless construction by rotational molding (laminated or fabricated tanks will not be accepted). The tanks are designed for above-ground, vertical installation and are capable of containing chemicals at atmospheric pressure. The assembly shall be designed to prevent rainwater from entering the containment tank. The design shall allow direct primary tank base retention for up to seismic conditions per IBC code requirements. The containment tank shall be designed to hold a minimum of 115% of the normal fill capacity of the primary tank. Included in this specification are requirements for material properties, design, construction, dimensions, tolerances, workmanship, and appearance. Tank capacities are from 550 gallons (2082 L) up to 10,000 gallons (37,851 L).
- 1.2 This specification does not cover the design of vessels intended for use at pressures above or below atmospheric conditions. It is also not for vessels intended for use with liquids heated above their flash points, temperatures above 140 degrees Fahrenheit for Type I materials, or temperatures above 130 degrees Fahrenheit for Type II materials (see section 6.1 for material classifications).

2. Applicable Documents

- 2.1 ASTM (American Society for Testing and Materials) Standards:
 - D618 Conditioning Plastics and Electrical Insulating Materials for Testing
 - D638 Tensile Properties of Plastics
 - D790 Flexural Properties of Unreinforced and Reinforced Plastics and
 - **Electrical Insulating Materials**
 - D883 Definitions of Terms Relating to Plastics
 - D1505 Density of Plastics by the Density-Gradient Technique
 - D1525 Test Method for Vicat Softening Temperature of Plastics
 - D1693 Test Method for Environmental Stress-Cracking of Ethylene Plastics
 - D1998 Standard Specification for Polyethylene Upright Storage Tanks
 - D2765 Degree of Crosslinking in Crosslinked Ethylene Plastics as
 - Determined by Solvent Extraction
 - D2837 Method for Obtaining Hydrostatic Design Basis for Thermoplastic Pipe Materials
 - D3892 Practice for Packaging/Packing of Plastics
 - F412 Definitions of Terms Relating to Plastic Piping Systems
- 2.2 ARM (Association of Rotational Molders) Standards: Low Temperature Impact Resistance (Falling Dart Test Procedure)
- 2.3 ANSI Standards: B-16.5 Pipe Flanges and Flanged Fittings
- 2.4 OSHA Standards: 29 CFR 1910.106 Occupational Safety and Health Administration, Flammable and Combustible Liquids
- 2.5 UBC CODE: Uniform Building Code 2006 Edition
- 2.6 IBC CODE: International Building Code 2009 Edition

- 2.7 CBC Code: California Building Code 2010 Edition
- 2.8 NSF/ANSI Standard 61 Drinking Water System Components (Type II resin)
- 2.9 40 CFR-264.193

3. Submittals

- 3.1 Drawings and Data: The manufacturer's shop drawings shall be approved by the engineer or contractor prior to the manufacturing of the tank(s). Data and specifications for the equipment shall include, but shall not be limited to the following.
- 3.2 Contractor shall submit for review sufficient literature, detailed specifications, and drawings to show dimensions, materials used, design features, internal construction, weights and any other information required by the ENGINEER for review of storage tanks and accessories.
- 3.3 Information to be included with submittals are specified below:
 - 3.3.1 Shop drawings for the tanks shall include as a minimum the following:
 - a) Service Conditions: Chemical environment and temperature.
 - b) Statement that fabrication shall be in accordance with ASTM D 1998, where applicable.
 - c) Sizing and description of the fittings and accessories for each tank that are to be supplied by the tank manufacturer.
 - d) Layouts and assembly schedules for each tank identifying the location and elevation from the bottom of the tank for all connections and appurtenances supplied by the tank manufacturer.
 - 3.3.2 Resin A copy of the resin data sheet from the resin manufacturer for the tank is to be supplied and the tank manufacturer is to certify that it will be the resin used in the manufacture of the tank. Verification may be required if the resin is to be FDA or NSF 61 listed.
 - 3.3.3 Wall thickness Prior to the manufacture of the tank the designed wall thickness audit is to be supplied based upon 600 psi hoop stress (ASTM D 1998) @ 100 degrees F. (Note: See 7.1.2 for chemicals being stored above 100 degrees F)
 - 3.3.4 Tank restraint If supplied, the drawings and calculations for the system are to be provided. Note: Wet stamped or site specific drawings and calculations may be required.
 - 3.3.5 Supporting information on fittings and accessories to be supplied; heat system, insulation, mastic coating, etc.
- 3.4 Technical Manuals: The tank manufacturer's "Guideline for Use & Installation" is to be submitted for review.
- 3.5 Installation certificate: Once installed the installer is to certify that the tank system has been installed according to the tank manufacturer's Guidelines for Use & Installation.
- 3.6 Manufacturer's warranty

- 3.7 Manufacturer Qualifications: The manufacturer is to have rotationally molded polyethylene tanks based upon ASTM D 1998 utilizing Type I and Type II resins for the last 10 years.
- 3.8 Factory Test Report: Upon completion of the tank the manufacturer's inspection report is to be supplied for each tank.
 - a. Verification of wall thickness (See 8.5)
 - b. Impact test (See 8.3.1)
 - c. Gel test (Type I resin only) (See 8.4)
 - d. Hydrostatic test (See 8.6)
 - e. Verification of fitting placement (See 8.2.4)
 - f. Visual inspection (See 8.7)
 - g. Verification of materials

4. Service Conditions

Note: The tank color will be based upon the chemical application and UV exposure of the installation. Tank color is to be natural, black or opaque white.

Table I – Service Conditions

Tank #	Chemical Stored	Concentration / Specific Gravity	Tank Location Inside / Outside	Operating Temperature (Temperature of chemical)	Fitting Material	Gasket Material	Bolt Material

5. Chemical Compatibility

5.1 Chemical compatibility shall be according to the following chemical resistance guides:

Compass Publications -

Pruett, Kenneth M., "Chemical Resistance Guide for Plastics"

Pruett, Kenneth M., "Chemical Resistance Guide for Metals and Alloys"

Pruett, Kenneth M., "Chemical Resistance Guide for Elastomers III"

5.2 These references shall be considered as general guidelines only. In many cases, combinations of these chemicals are used in such a way that only the customer (by testing molded product samples) can make a determination in regards to acceptability.

Note: Contact the manufacturer for applications that are not listed below.

Chemical	Concentration	Resin	Design Info	Fitting Material	Gasket Material	Bolt Material
Acetic Acid	60	HDLPE & XLPE	1.5/600	PP/PVC	EPDM	316SS/Hastelloy/Titan.
Acetic Acid	80	HDLPE	1.9/600	PP	EPDM	316SS/Hastelloy/Titan.
Acrylic Emulsions	50	XLPE	1.9/600	PVC	EPDM	316SS
Aluminum Sulfate	50	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS**/Hastelloy/Titan.
Ammonium Sulfate	40	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS**/Hastelloy/Titan.
Calcium Carbonate	Saturated	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS

Calcium Chloride	40	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS**/Hastelloy/Titan.
DEF (Diesel Exhaust Fluid)	32.5	HDLPE & XLPE	1.35/600	PP/PVC	EPDM	316SS
Deionized Water < 5 Megohm		HDLPE & XLPE	1.5/600	PVC	EPDM	316SS
Deionized Water >5 Megohm		HDLPE & XLPE	1.5/600	PVC	EPDM	316SS
Ethyl Alcohol	100	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS
Ethylene Glycol	100	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS
Ferric Chloride	50	HDLPE & XLPE	1.9/600	PVC	EPDM	Hastelloy/Titan.
Ferric Sulfate	60	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS**/Hastelloy/Titan.
Ferrous Chloride	Saturated	HDLPE & XLPE	1.9/600	PVC	EPDM	Hastelloy/Titan.
Ferrous Sulfate	20	HDLPE & XLPE	1.5/600	PVC	EPDM	Hastelloy
Hydrochloric Acid	37	HDLPE	1.9/600	PVC	Viton	Hastelloy
Hydrofluoric Acid	48	HDLPE	1.9/600	PP/PVC	Viton	Hastelloy
Hydrofluosilicic Acid	26	HDLPE/XLPE*	1.9/600	PP/PVC	Viton	Hastelloy
Hydrogen Peroxide	50	HDLPE	1.9/600	PVC	Viton	316SS/Hastelloy/Titan.
Isopropyl Alcohol	100	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS
Magnesium Chloride	30	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS**/Hastelloy/Titan.
Methyl Alcohol	100	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS
Motor Oil	100	HDLPE & XLPE	1.9/600	316SS	Viton	316SS
Phosphoric Acid	85	HDLPE	1.9/600	PVC	Viton	316SS
Phosphoric Acid	50	HDLPE	1.9/600	PVC	Viton	316SS
Polymers (Deposition)		XLPE	1.5/600	PVC	EPDM	316SS
Potable Water		HDLPE	1.5/600	PVC	EPDM	316SS
Potassium Carbonate	50	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS
Potassium Hydroxide	Saturated	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS
Sodium Carbonate	30	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS**/Hastelloy/Titan.
Sodium Carbonate	Saturated	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS**/Hastelloy/Titan.
Sodium Hydroxide	50	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS
Sodium Hypochlorite-in(Non-UV)	<16.5	HDLPE	1.9/600	PVC	Viton	Titanium
Sodium Hypochlorite-out (UV)	<16.5	HDLPE #880059	1.9/600	PVC	Viton	Titanium
Sodium Hypochlorite-out (UV)	<16.5	HDLPE Insulated	1.9/600	PVC	Viton	Titanium
Sodium Thiosulfate	40	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS
Sulfuric Acid	98	HDLPE #880046*	1.9/600	CPVC	Viton	Hastelloy
Sulfuric Acid	93	HDLPE #880046*	1.9/600	CPVC	Viton	Hastelloy
Surfactants		XLPE	1.5/600	PVC	EPDM	316SS
Urea Solution	50	HDLPE & XLPE	1.35/600	PP/PVC	EPDM	316SS
Water w/Ozone up to 10 PPM		HDLPE & XLPE	1.5/600	PVC	EPDM	316SS

Note: Ambient Temperature / atmospheric pressure.

Chart applies to Industrial ASTM designed tanks.

High purity chemical applications are limited to natural tank color or special hot compounded resins.

For chemicals or chemical blends not listed on the above chart, please contact Snyder Industries.

6. Materials - Resin Classification

- 6.1 Tanks are classified according to type as follows and it is the responsibility of the purchaser to specify Type I or Type II.
 - 6.1.1 Type I Tanks molded from cross-linkable polyethylene resin.
 - 6.1.2 Type II Tanks molded from linear polyethylene resin (not cross-linkable resin).
- 6.2 The material used shall be virgin polyethylene resin as compounded and certified by the manufacturer. Type I tanks shall be made from crosslinked polyethylene (XLPE) resin as manufactured by ExxonMobil Chemical, or resin of equal physical and chemical properties. Type II tanks shall be made from high density linear polyethylene (HDLPE) resin as manufactured by ExxonMobil Chemical, or resin of equal physical and chemical properties.

^{*}Chemical may cause tank material to discolor.

^{** 316}SS may pit upon drying. Not recommended for SUMOs.

- 6.3 All polyethylene resin material shall contain a minimum of a U.V. 8 stabilizer as compounded by the resin manufacturer. Pigments may be added at the purchaser's request, but shall not exceed 0.25% (dry blended) of the total weight.
- 6.4 Mechanical Properties of Type I tank material: Cross-linked (XLPE)

PROPERTY	ASTM	VALUE
Density (Resin)	D1505	0.938-0.946 g/cc
Tensile (Yield Stress 2"/min)	D638	2830 - 3000 PSI
Elongation at Break (2"/min.)	D638	700 - 800%
ESCR (100% Igepal, Cond. A, F50)	D1693	>1000 hours
ESCR (10% Igepal, Cond. A, F50)	D1693	>1000 hours
Vicat Softening Degrees F. Temperature	D1525	250
Flexural Modulus	D790	87,000 – 110,000 PSI

6.5 Mechanical Properties of Type II tank material: High density Linear (HDLPE)

PROPERTY	ASTM	<u>VALUE</u>
Density (Resin)	D1505	0.941-0.948 g/cc
Tensile (Yield Stress 2"/min)	D638	3000 PSI
Elongation at Break (2"/min.)	D638	>1000%
ESCR (100% Igepal, Cond. A, F50)	D1693	550 hours
ESCR (10% Igepal, Cond. A, F50)	D1693	50 hours
Vicat Softening Degrees F. Temperature	D1525	235
Flexural Modulus	D790	130,000 PSI

7. Design Requirements

7.1 The minimum required wall thickness of the cylindrical shell at any fluid level shall be determined by the following equation, but shall not be less than 0.187 in. thick.

T = $P \times O.D./2 SD = 0.433 \times S.G. \times H \times O.D./2 SD$

T = wall thickness

SD = hydrostatic design stress, PSI P = pressure (.433 x S.G. x H), PSI

H = fluid head, ft.

S.G. = specific gravity, g/cm^3 O.D. = outside diameter, in.

7.1.1 The hydrostatic design stress shall be determined by multiplying the hydrostatic design basis, determined by ASTM D2837 using rotationally molded samples, with a service factor selected for the application. The hydrostatic design stress is 600 PSI at 73 degrees

Fahrenheit for Type I and Type II materials. In accordance with the formula in 7.1, the tank shall have a stratiform (tapered wall thickness) wall.

- 7.1.2 The hydrostatic design stress shall be derated for service above 100 degrees Fahrenheit and for mechanical loading of the tank.
- 7.1.3 The standard design specific gravity shall be 1.5 or 1.9.
- 7.1 The minimum required wall thickness for the cylinder straight shell must be sufficient to support its own weight in an upright position without any external support. Secondary containment tanks shall be designed per SII standard containment thickness requirements. The secondary containment shall be configured to allow shipment of the primary tank inside of the secondary tank. The shipment shall be done without the aid of additional spacer blocks which can be lost during shipment causing tank damage.
- 7.2 The top head must be integrally molded with the cylinder shell. The minimum thickness of the top head shall be equal to the top of the straight wall. The primary tank top shall be configured to prevent rain water from entering the secondary containment tank. The top head of tanks with 550 or more gallons of capacity shall be designed to provide a minimum of 1300 square inches of flat area for fitting locations. The primary tank shall be keyed to the secondary tank preventing primary tank rotation. The secondary containment shall have 115% of the normal fill capacity of the primary tank.
- 7.3 Tanks with 550 or more gallons of capacity shall have a minimum of 3 lifting lugs integrally molded into the top head. The lifting lugs shall be designed to allow erection of empty primary and secondary tanks. Tanks shall be capable of being lifted into position as a unit (primary and secondary tanks).
- 7.4 The tank shall be designed to provide a minimum of 4 tie-down lugs integrally molded into the top head. The tie-down lugs shall be designed to allow tank retention in wind and seismic loading situations without tank damage. The primary/secondary tank unit shall be configured to allow direct primary tank base retention for seismic load conditions. The base retention unit shall be anchor bolted to an appropriate structure and not require additional spacer blocks. Refer to section 12.0 for tank tie-down accessories.

Table II - Tank Schedule

Tank Reference #		
Quantity		
Capacity - Side Wall		
Specific Gravity– designed		
Primary Tank		
Secondary Tank		
Diameter (nominal)		
Height (feet) maximum		
Tank Resin (primary/secondary)		
Type I XLPE		
Type II HDLPE		
Color		
Manway Type		

Fitting Material		
Gasket Material		
Bolt Material		

8. Test Methods

Quality Assurance & Testing

- 8.1 The tanks of the same material furnished under this Section shall be supplied by a manufacturer who has been regularly engaged in the design and manufacturing of rotationally molded polyethylene chemical storage tanks using cross-linked and high density linear polyethylene tanks for over ten years.
- 8.2 Dimensions and Tolerances
 - 8.2.1 All dimensions will be taken with the tank in the vertical position, unfilled. Tank dimensions will represent the exterior measurements.
 - 8.2.3 The tolerance for the outside diameter, including out of roundness, shall be per ASTM D1998.
 - 8.2.4 The tolerance for fitting placements shall be \pm 0.5 in. in elevation and 2 degrees radial at ambient temperature.
- 8.3 Test Methods

Test specimens shall be taken from fitting location areas.

- 8.3.1 Low Temperature Impact Test
 - 8.3.2 Test specimens shall be conditioned at (- 40) degrees Fahrenheit for a minimum of 2 hours.
 - 8.3.3 The test specimens shall be impacted in accordance with the standard testing methods as found in ASTM D1998. Test specimens $< \frac{1}{2}$ " thickness shall be tested at 100 ft. lb. Test specimens $> \frac{1}{2}$ " thickness shall be tested at 200 ft. lb.
- 8.4 Degree of Crosslinking Test (% Gel Type I Resin Only)
 - 8.4.1 The test method used is to be the o-xylene insoluble fraction (gel test) per ASTM D2765 Method C. This test method is for determination of the ortho-xlene insoluble fraction (gel) of crosslinked polyethylene.
 - 8.4.2 The percent gel level for Type I tanks on the inside 1/8 in. of the wall shall be a minimum of 65%.
- 8.5 Ultrasonic Tank Thickness Test
 - 8.5.1 All tanks 2000 gallons or larger shall be measured for tank wall thickness at 6", 1ft., 2ft. and 3ft. on the tank sidewall height at 0° and 180° around the tank circumference with 0° being the tank manway and going counter-clockwise per ANSI standard drafting specifications. A copy of this test report can be ordered when placing the original tank order. All tanks shall meet design thickness requirements and tolerances.
 - 8.5.2 Tanks smaller than 2000 gallons are only periodically measured at the start of a production run or after any design changes. Customers can place an order for tank wall

thickness measurements on smaller tank sizes when placing the original order. A copy of the test report will be provided if ordered.

8.6 Hydrostatic Water Test

8.6.1 The hydrostatic water test shall consist of filling the primary tank to brim full capacity for a minimum of four hours and conducting a visual inspection for leaks. A hydrostatic water test will be conducted if ordered by the customer.

8.7 Workmanship

- 8.7.1 The finished tank wall shall be free, as commercially practicable, of visual defects such as foreign inclusions, air bubbles, pinholes, pimples, crazing, cracking and delaminations that will impair the serviceability of the vessel. Fine bubbles are acceptable with Type II tanks to the degree in which they do not interfere with proper fusion of the resin melt.
- 8.7.2 All cut edges where openings are cut into the tanks shall be trimmed smooth.

Table III – Fitting and Accessory Schedule

<u></u>		1	T	
Tank Number	TNK -	TNK -	TNK -	TNK -
Description	Quantity / Size	Quantity / Size	Quantity / Size	Quantity / Size
Inlet nozzle				
Top draw outlet nozzle				
Drain (transition fitting)				
Overflow				
Vent				
Surge Protection Lid				
Fill				
External fill pipe				
Internal fill pipe				
Manway				
Threaded/ vented				
Threaded				
Hinged				
Bolted / Sealed				
Ladder FRP / Galvanized Steel				
Lifting Lugs				
Tie-down Lugs				
Seismic/Wind Tie-down				
Galvanized Steel				
304 SS				
316 SS				
Level Indicator				
Ultrasonic				
Flexible tube				
Mechanical Reverse Float				

Leak Detection System		
Heat System		
Maintenance Temperature		
Min. Ambient Temperature		
Insulation w/mastic coating (gray in color)		

9. Tank Fittings (Nozzles)

- 9.1 Fittings Threaded Bulkhead
 - 9.1.1 Threaded bulkhead fittings are available for above liquid installation depending on the tank diameter and the placement of the fitting in the tank. Fittings must be placed away from tank knuckle radius' and flange lines. Consult SII for placement questions. The maximum allowable size for bulkhead fittings placed on a curved cylindrical section of tanks 48 in. to 142 in. in diameter is 2 inch. Tank wall thickness must be considered for bulkhead fitting placement. The maximum wall thickness for each fitting size is shown below.

Fitting Size	Maximum Wall Thickness
<u>1/2 in.</u>	<u>2 in.</u>
<u>3/4 in.</u>	<u>2 in.</u>
<u>1 in.</u>	<u>2 in.</u>
<u>1 1/4 in.</u>	<u>2 in.</u>
<u>1 1/2 in.</u>	<u>2 in.</u>
<u>2 in.</u>	<u>2 in.</u>
<u>3 in.</u>	2.125 in. (Flat Surface Only)

- 9.1.2 The bulkhead fittings shall be constructed of PVC, PP, or other specified material.

 Gaskets shall be a minimum of 1/4" thickness and constructed of 40-50 durometer EPDM, 60-70 durometer Viton[♦], or other specified material.
- 9.2 Fittings Bolted Double 150 lb. Flange Fittings
 - 9.2.1 Bolted double flange fittings are available for below liquid level installation for sizes 2 in. through 4 in. depending on the placement of the fitting in the tank. Fittings must be placed away from tank knuckle radius' and flange lines. Consult SII for placement questions. Bolted double flange fittings provide the best strength and sealing characteristics of any tank fitting available. Allowable fittings sizes based on tank diameter for curved surfaces are shown below.

Tank Diameter	Maximum Bolted Fitting
	Size Allowable
48 in 86 in.	3 in.
90 in 102 in.	6 in.
120 in 142 in.	8 in.

The bolted double flange fittings shall allow tank wall thickness up to 2 1/2 in.

9.2.2 The bolted double flange fitting shall be constructed with 2 ea. 150 lb. flanges, 2 ea. 150 lb. flange gaskets, and the correct number and size of all-thread bolts for the flange specified by the flange manufacturer. The flanges shall be constructed of PVC Type I, Grade I, or other specified material. Gaskets shall be a minimum of 1/4" thickness and

constructed of 40-50 durometer EPDM, 60-70 durometer Viton or other specified material. There shall be a minimum of 4 ea. full thread bolts. The bolts may have gasketed flanged metal heads or bolt heads encapsulated in Type II polyethylene material. The encapsulated bolt shall be designed to prevent metal exposure to the liquid in the tank and prevent bolt rotation during installation. The polyethylene encapsulation shall fully cover the bolt head and a minimum of 1/4" of the threads closest to the bolt head. The polyethylene shall be color coded to distinguish bolt material (white - 316 S.S., yellow - Hastelloy C276, red - Monel, green - Titanium). Each encapsulated bolt shall have a gasket to provide a sealing surface against the inner flange.

- 9.2.3 Standard orientation of bolted double flange fittings shall have bolt holes straddling the principal centerline of the tank in accordance with ANSI/ASME B-16.5 unless otherwise specified.
- 9.3 Fittings Bolted Stainless Steel Fittings
 - 9.3.1 Bolted stainless steel fittings are available for below liquid level installation depending on the tank diameter and the placement of the fitting in the tank. Fittings must be placed away from tank knuckle radius' and flange lines. Consult SII for placement questions. Allowable fittings sizes based on tank diameter for curved surfaces are shown below.

Maximum Bolted Fitting Size
<u>Allowable</u>
3 in.
4 in.

The bolted stainless steel fittings shall allow tank wall thickness up to 2 1/2 in.

- 9.3.2 The bolted stainless steel fittings shall be constructed with a minimum of 4 fully threaded 3/8 in. studs. Each fitting shall have two gaskets and two flanges. One gasket shall be compressed between the inside of the tank wall surface and the inside flange of the fitting. The other gasket shall be compressed between the outside tank wall surface and the outside flange of the fitting. The stainless steel fittings come standard with female pipe threads on both the inner and outer flanges. Other threading arrangements may be specified. The fittings shall be constructed of Type 316 stainless steel. Gaskets shall be a minimum of 1/4" thickness and constructed of 40-50 durometer EPDM, 60-70 durometer Viton or other specified material.
- 9.4 Fittings Unified Fitting Outlet (UFO™)
 - 9.4.1 The UFO shall provide a flexible containment seal between the inner primary tank and the outer secondary containment tank. This fitting outlet when used in combination with fittings as per sections 9.2 and 9.3 provides access for connecting piping to the inner primary tank while maintaining containment integrity between the inner primary tank and the outer secondary containment tank. This fitting outlet may be used for 2, 3, and 4 in. fitting sizes.
 - 9.4.2 The fitting outlet shall consist of 1 ea. flexible polyethylene containment boot, 1 ea. appropriate fitting gasket, 1 ea. UFO gasket, 1 ea. solid 304 stainless steel UFO flange, 1 ea. split 304 stainless steel UFO flange, and 12 ea. 3/8 in. 304 stainless steel bolt assemblies. Gaskets shall be a minimum of 1/4" thickness and constructed of 40-50 durometer EPDM, 60-70 durometer Viton or other specified material.
- 9.5 Fittings Siphon Tube Fittings
 - 9.5.1 Siphon tubes may be added to the fittings specified in sections 9.2 and 9.3. A siphon tube will allow these fittings, when used as drainage fittings, to provide better tank drainage.
- 9.6 Vents
 - 9.6.1 Each tank must be properly vented for the type of material and flow rates expected. Vents must comply with OSHA 1910.106 (f) (2) (iii) or other accepted standard. All tanks

must be vented for atmospheric pressure as well as any pressure created by filling and emptying the tank. Some applications may require a sealed tank with a vent line going to a scrubber system for proper chemical safety. Venting equipment should be sized to limit pressure or vacuum in the tank to a maximum of 1/2" of water column (0.02 psi). U-Vents are offered in sizes from 1 in. to 6 in. with or without mesh insect screening. U-Vents with mesh screening may require additional sizing due to reduced air-flow rates. Consult the manufacturer for necessary venting and placement information.

- 9.6.2 All u-vents shall be constructed of PVC or other specified materials.
- 9.6.3. When a tank is being filled from a pressurized tanker truck or rail car steps need to be taken to avoid pressurizing the tank. The tank may require a secondary surge protection lid to avoid any pressure build up. The surge protection lid is to be a 14" or 18" hinged and be design that it is self-closing.

9.7 Flange Adapters

9.7.1 Flange adapters may be purchased as optional equipment to adapt threaded or socket fitting outlets to 150 lb. flange connections for connection to piping system components. Flange adapters are available in PVC, CPVC or other specified materials. Flange adapter construction shall utilize schedule 80 components in sizes ranging from 3/4" to 8" depending on material required.

9.8 Fittings - Self-Aligning Threaded Bulkhead

9.8.1 Self-Aligning fittings are available for installation in vapor phase applications on curved surfaces depending on the spherical dome radius and the placement of the fitting on the tank dome. Fittings must be placed away from tank radius'. Consult SII for placement questions. The maximum allowable size for self-aligning fittings placed on a spherical section of the tank is shown below.

Tank Diameter	Maximum Fitting Size
	<u>Allowable</u>
45 in. – 48 in.	2 in.
64 in. – 142 in.	3 in.

Tank thickness and fitting angle may need to be considered for self-aligning fitting placement. The maximum thickness and installation angles for each fitting size are shown below.

Fitting Size	<u>Maximum Angle</u>	Maximum Thickness
1 in.	27 degrees	1.000 in.
2 in.	25 degrees	0.750 in.
3 in.	20 degrees	1.000 in.

9.8.2 The self-aligning fittings shall be constructed of PVC or CPVC. Gaskets shall be a minimum of 1/4" thickness and constructed of 40-50 durometer EPDM, 60-70 durometer Viton[†], or other specified material.

9.9 Flexible Connections

- 9.9.1 All tank fitting attachments shall be equipped with flexible couplers or other movement provisions provided by the tank customer. The tank will deflect based upon tank loading, chemical temperature and storage time duration. Tank piping flexible couplers shall be designed to allow 4% design movement. Movement shall be considered to occur both outward in tank radius and downward in fitting elevation from the neutral tank fitting placement.
- 9.1.2 The flexible connection is to be manufactured of the same material as the tank or a compatible material approved by the project engineer. If an elastomer flexible connection is used control bolts are required if recommended by the manufacturer. The flexible

connection is to be designed for a minimum of 4% movement. The flexible connection is to be designed with 150# flange connections to allow for attachment to the tank and the piping system. The flexible connection is to be attached as close as possible to the tank to reduce stress.

10. Tank Attachments

10.1 Tank Attachments - Ultrasonic Level Indicator

10.1.1a. The ultrasonic enclosure is to be an all plastic design with a NEMA 4X rating. The ultrasonic transducer is to have a 12" dead band and beam with a 20 ft range. The supply voltage can be 110, 220 VAC or 24 VDC. The connection to the tank is to be 2" NPT.

The ultrasonic level indicator shall provide a visual display of liquid level in the tank showing gallonage in measurement of hundreds of gallons along with 4-20 mA output for other alarm or control systems as well as four independent contacts capable of handling 10 amps each. Each contact can be programmed to operate in different opening and closing methods (7 modes). Contacts can be used to control pumps, valves, alarms, etc.

10.2 Tank Attachments - Leak Detector Unit

10.2.1 The leak detector unit shall consist of a proximity sensor, a welded 2 in. fpt connection, a 2 in. bung plug with a ¾ in strain relief, and an indicator box. The sensor is placed in the interstitial space between the primary and secondary tanks approximately 1 in. above the tank bottom. The indicator box shall be Nema 4 rated and factory pre-wired for 110 VAC power. All connections shall be labeled to prevent errors in field installation. The indicator box will show a green light when power is on and the sensor is not detecting a liquid. The light is a push to test light allowing the operator to test for power outage or malfunction. If the green light goes out there are two possibilities. The green light does not come on when the button is pushed. This would indicate a lack of power to the unit or the light bulb is burned out. If the green light comes on when pushed, then a possible leak condition is indicated.

10.3 Level Indication

10.3.1 Sight Level Gage

a. The sight level gage shall be constructed of flexible PE or PVC tubing to allow for tank contraction and expansion due to loading and temperature changes. The level gage shall be connected to the tank at the top of the tank with 1ea. appropriate 3/4" fitting as described in section 9.1 or 9.2. and to a tee off of the drain / transition fitting. Each fitting can have valves installed for isolation or drainage purposes.

10.3.2 Manway and Fill Cap (Non-sealed)

- 10.3.1 Fill caps are available in a 10 in. vented-threaded style on various tank sizes with a minimum opening diameter of 7.125 in. Cap attachment shall be provided with all standard 10 in. cap placements with a polyurethane cap tie. Check the manufacturer's specification drawing for availability and position.
- 10.3.2 Manways are available in an 18 in. vented or non-vented threaded design or hinged style (minimum opening diameter of 15 in.) and a 24 in. vented or non-vented threaded or hinged style (minimum opening diameter of 22 in.) on various tank sizes. Check the manufacture's specification drawing for availability and position.
- 10.3.3 All caps and manways shall be constructed of polyethylene material.

10.4 Bolted Sealed Top Manway

10.4.1 Sealed manways are available in 14, 18, 20 and 24 in. sizes on certain tanks in selected positions. Consult the manufacturer for placement positions.

10.4.2 The sealed manway shall be constructed of polyethylene material. The bolts shall be polypropylene or other specified material. The gaskets shall be closed cell, crosslinked polyethylene foam and Viton orings to seal the bolts.

10.5 Surge Protection Lid

10.5.1 The hinged lid is to be manufactured of polyethylene. The lid will be a 14 in. size with 11 in. access opening or 18" with 15" access. The opening of the lid is to be restricted by a tether. The lid is to be designed so that is will close when the pressure has been released. Check SII specification drawing for availability and position.

10.6 Tank Attachments - External Fill Pipes

- 10.6.1 External fill pipes shall be prepared per the customer approved drawings and specifications. All external fill pipes shall be supported at 3 ft. maximum intervals with a support structure independent of the tank (ground supported). All designs shall be done according to the specific needs of the customer.
- 10.6.2 All external fill pipes shall be constructed of PVC or other specified materials.

10.7 Tank Attachments – Internal Down Pipes

- 10.7.1 Internal down pipes shall be prepared per the customer approved drawings and specifications. All internal down pipes shall be supported at 5 ft. maximum intervals with a support structure welded to the inside of the primary tank (only available in tanks constructed with Type II resin). The support design may utilize a PVC clamp or other specified materials for support. All designs shall be done according to the specific needs of the customer.
- 10.7.2. All internal down pipes shall be constructed of PVC or other specified materials.

11. Tank Accessories

11. Ladders

- 11.1 Ladders shall be constructed of galvanized mild steel or FRP.
- 11.2 Safety cages shall be provided with ladders as optional equipment unless required by OSHA standards.
- 11.3 All ladders shall be designed to meet applicable OSHA standards. Reference: OSHA 2206; 1910.27; fixed ladders.
- 11.4 Ladders must be mounted to the tank to allow for tank expansion and contraction due to temperature and loading changes. All top ladder mounts shall be connected to integrally molded in attachment lugs that allow for tank movement due to temperature and loading changes.
- 11.5 Mild steel parts shall be deburred and galvanized.

12.0 Tie Down Systems

- 12.1 The tie down system shall be designed to withstand 150 MPH wind loads. Tie down systems must meet seismic requirements per IBC 2009 / CBC 2010 code with seismic loads ≤ .445g (Seismic Design Category "D" Fa=1.0, Fv=1.5, Ss=1.4, S1=0.5). Anchor bolts shall be provided by the contractor per the calculations and the base plates for the system. A registered engineer's wet stamped calculations and or drawings may be required.
- 12.2 The tie down system shall be offered galvanized, 304 or 316 stainless steel.
- 12.3 Mild steel parts shall be deburred and galvanized.
- 13.0 Tank Accessories Tank Heating Systems

- 13.1 Heating systems for use with polyethylene tanks shall be designed to meet specific requirements such as tank material type, tank size, low ambient temperature, and desired maintenance temperature.
- 13.2 All control components of the heating system shall be mounted in water tight, high impact plastic box(es) with a gasketed cover.
- 13.3 All heating system components shall be Nema 4 rated and factory pre-wired for 110 VAC. All connections shall be labeled to prevent errors in field installation.
- 13.4 Each control box shall carry a decal attached to the inside surface of the cover, on which an electrical wiring diagram will be printed.
- 13.5 Each control box shall contain two temperature controls. One control shall regulate the maintenance temperature setting and the other control shall regulate the high temperature setting. The maintenance temperature setting should be set at the desired maintenance temperature. The high temperature setting shall be adjusted to 10 degrees above the desired maintenance temperature to a maximum of 130 degrees Fahrenheit. All control systems must be designed with a power off failure mode.
- 13.6 The heating panels shall be designed to wrap around and lie flat against the surface of the secondary containment tank. The heating panels shall have a maximum heating density of 0.022 watts per square centimeter. All heating panels and sensor bulbs shall be attached to the tank with 2" wide duct tape. The high temperature sensor shall directly sense the temperature of the heating panels on the secondary containment tank. The maintenance temperature sensor shall directly sense the temperature of the inner primary tank. Under no circumstances shall cable type heaters be used with polyethylene tanks.
- 13.7 Insulation used shall be polyurethane foam with a density of 2.0 3.0 lb./ft ^3 with a "R" value of 8.33/in. The foam shall be applied with a nominal thickness of 2" to all external tank surfaces except the tank bottom shell.
- 13.8 Upon completion of application and curing of the insulation, two full coverage coats of latex mastic coating shall be applied to the surface of the insulation in such manner as to seal the insulation from the outside environment.

14. Warranty

14.1 The tank shall be warranted for three years in regards to defects in materials and workmanship. The warranty on fittings and accessories that are supplied by the tank manufacturer will be for one year. The warranty will begin at time of shipment.

15. Marking, Packing and Packaging

- 15.1 The tanks shall be marked to identify the product, date (month and year) of manufacture, capacity, and serial number. The tank shall be shipped with a 3 of 9, HRI bar code label containing tank description, manufacturing order number, part number, serial number, manufacturer, and date.
- 15.2 The proper caution or warning signs as prescribed by OSHA standard 29 CFR 1910.106 shall be customer determined and supplied.
- 15.3 All packing, packaging, and marking provisions of ASTM Practice D3892 shall apply to this standard.
- 15.4 Customer specified labeling is available.
- 15.5 Tank shrink wrapping and bagging is available upon customer request.

15.6 All fittings that do not interfere with tank shipment shall be installed unless otherwise specified. Fittings and accessories that interfere with tank shipment or could be broken during shipment are shipped separately.

16. Shipping

- 16.1 Since there are variations in methods of shipping, SII's instructions shall be followed in all cases.
- 16.2 Consult the SII "Guidelines for Use and Installation" booklet included with your tank for unloading instructions on specific tanks. This booklet can be found attached to the cap or manway area on the inside of the tank. Tanks with capacities of 2000 gallons or more have molded-in lifting lugs provided to assist with tank handling. All tank units are shipped with shipping cables allowing the two tanks to be handled as a unit during shipping and tank handling. Once the tank is put into position the shipping cables are to be removed to allow the tank to fully contact the tank pad/support area.
- 16.3 Upon arrival at the destination, the purchaser and/or his agent shall be responsible for inspection for damage in transit. If damage has occurred, a claim should be filed with the carrier by the purchaser, and the manufacturer should be notified prior to the tank being put into service.

17. Delivery & Storage

- 17.1 Installation
- 17.1.1 Transportation, handling, storage of the tanks, and installation shall be in accordance with the manufacturer's printed instructions.
- 17.1.2. Repair any damage to tank components or the insulation due to transportation or installation.
- 17.1.3. All tank fitting attachments shall be equipped with flexible couplers or other movement provisions provided by the tank customer. The tank will deflect based upon tank loading, chemical temperature and storage time duration. Tank piping flexible couplers shall be designed to allow 4 percent design movement. Movement shall be considered to occur both outward in tank radius and downward in fitting elevation from the neutral tank fitting placement.
- 17.1.4. The installer is to certify in writing that the tank system has been installed according to the tank manufacturer's Guidelines for Use & Installation.

T	ank Chemical	Resistance	Chart
		(S	nvder)



CHEMICAL RESISTANCE RECOMMENDATIONS

			Design	Fitting	Gasket	Bolt
Chemical	Concentration	Resin	Info	Material	Material	Material
Acetic Acid	60	HDLPE & XLPE	1.5/600	PP/PVC	EPDM	316SS/Hastelloy/Titan.
Acetic Acid	80	HDLPE	1.9/600	PP	EPDM	316SS/Hastelloy/Titan.
Acrylic Emulsions	50	XLPE	1.9/600	PVC	EPDM	316SS
Aluminum Sulfate	50	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS**/Hastelloy/Titan.
Ammonium Sulfate	40	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS**/Hastelloy/Titan.
Calcium Carbonate	Saturated	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS
Calcium Chloride	40	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS**/Hastelloy/Titan.
DEF (Diesel Exhaust Fluid)	32.5	HDLPE & XLPE	1.35/600	316SS	EPDM	316SS
Deionized Water < 5 Megohm		HDLPE & XLPE	1.5/600	PVC	EPDM	316SS
Deionized Water >5 Megohm		HDLPE & XLPE	1.5/600	PVC	EPDM	316SS
Ethyl Alcohol	100	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS
Ethylene Glycol	100	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS
Ferric Chloride	50	HDLPE & XLPE	1.9/600	PVC	EPDM	Hastelloy/Titan.
Ferric Sulfate	60	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS**/Hastelloy/Titan.
Ferrous Chloride	Saturated	HDLPE & XLPE	1.9/600	PVC	EPDM	Hastelloy/Titan.
Ferrous Sulfate	20	HDLPE & XLPE	1.5/600	PVC	EPDM	Hastelloy
Hydrochloric Acid	37	HDLPE	1.9/600	PVC	Viton	Hastelloy
Hydrofluoric Acid	48	HDLPE	1.9/600	PP/PVC	Viton	Hastelloy
Hydrofluosilicic Acid	26	HDLPE/XLPE*	1.9/600	PP/PVC	Viton	Hastelloy
Hydrogen Peroxide	50	HDLPE	1.9/600	PVC	Viton	316SS/Hastelloy/Titan.
Isopropyl Alcohol	100	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS
Magnesium Chloride	30	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS**/Hastelloy/Titan.
Methyl Alcohol	100	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS
Motor Oil	100	HDLPE & XLPE	1.9/600	316SS	Viton	316SS
Phosphoric Acid	85	HDLPE	1.9/600	PVC	Viton	316SS
Phosphoric Acid	50	HDLPE	1.9/600	PVC	Viton	316SS
Polymers (Deposition)		XLPE	1.5/600	PVC	EPDM	316SS
Potable Water		HDLPE	1.5/600	PVC	EPDM	316SS
Potassium Carbonate	50	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS
Potassium Hydroxide	Saturated	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS
Sodium Carbonate	30	HDLPE & XLPE	1.5/600	PVC	EPDM	316SS**/Hastelloy/Titan.
Sodium Carbonate	Saturated	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS**/Hastelloy/Titan.
Sodium Hydroxide	50	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS
Sodium Hypochlorite-in(Non-UV)	<16.5	HDLPE	1.9/600	PVC	Viton	Titanium
Sodium Hypochlorite-out (UV)	<16.5	HDLPE #880059	1.9/600	PVC	Viton	Titanium
Sodium Hypochlorite-out (UV)	<16.5	HDLPE Insulated	1.9/600	PVC	Viton	Titanium
Sodium Thiosulfate	40	HDLPE & XLPE	1.9/600	PVC	EPDM	316SS
Sulfuric Acid	98	HDLPE #880046*	1.9/600	CPVC	Viton	Hastelloy
Sulfuric Acid	93	HDLPE #880046*	1.9/600	CPVC	Viton	Hastelloy
Surfactants		XLPE	1.5/600	PVC	EPDM	316SS
Urea Solution	50	HDLPE & XLPE	1.35/600	PP/PVC	EPDM	316SS
Water w/Ozone up to 10 PPM		HDLPE & XLPE	1.5/600	PVC	EPDM	316SS

Note: Ambient Temperature.

Chart applies to Industrial ASTM designed tanks.

** 316SS may pit upon drying. Not recommended for SUMOs.

High purity chemical applications are limited to natural tank color or special hot compounded resins.

For chemicals or chemical blends not listed on the above chart, please contact Snyder Industries.

^{*}Chemical may cause tank material to discolor.

Fac Pond Water Physical / Chemical Analysis

(CWM)

2012 PHYSICAL / CHEMICAL ANALYSES FACULATIVE POND # 3

EFFLUENT PARAMETER	DISCHARGE LIMIT	FACULTATIVE POND #3 CONCENTRATION	PRACTICAL QUANTITATION LIMIT	UNITS
pH (RANGE)	(6.5 to 8.5)	7.6	0.01	SU
SPECIFIC CONDUCTANCE	Monitor	10,567	1	µmhos/cm
ALKALINITY, TOTAL (as CaCO3)	Monitor	123.3	1	mg/l
HARDNESS, TOTAL (as CaCO3)	Monitor	715	5	mg/l
TEMPERATURE	90	62	0.1	° F
SOLIDS, TOTAL SUSPENDED	60	12	1.0	mg/l
SOLIDS, TOTAL DISSOLVED	13,000	6,420	10	mg/l
SOLIDS, VOLATILE DISSOLVED	Monitor	583	10.0	mg/l
SOLIDS, SETTLEABLE	0.2	<0.1	0.1	ml/l/hr
BOD, 5-DAY	45	4.3	6	mg/l
DISSOLVED OXYGEN	2.0 (min)	6.6	0.01	mg/l
CARBON, TOTAL ORGANIC	Monitor	21	10	mg/l
NITROGEN, TOTAL ORGANIC (as N)	Monitor	4.3	1.00	mg/l
AMMONIA (as N)	20	2.8	0.5	mg/l
NITRITE, TOTAL (as N)	1.5	1.05	0.10	mg/l
NITRITE + NITRATE, TOTAL (N)	10	4.4	0.01	mg/l
OIL & GREASE	15	<1.0	1.0	mg/l
SURFACTANTS (MBAS)	1.0	0.04	0.02	mg/l
ALUMINUM, TOTAL	4,000	<100	100	μg/l
ANTIMONY, TOTAL	90	<60	60	μg/l
ARSENIC, TOTAL	80	22	5	μg/l
BARIUM, TOTAL	1,000	77	10	μg/l
BERYLLIUM, TOTAL	20	<5	5	μg/l
CADMIUM, TOTAL	50	<5	5	μg/l
CHLORIDE, TOTAL	Monitor	3,210,000	100,000	μg/l
CHLORINE, RESIDUAL	1,000	<324	324	μg/l
CHROMIUM, TOTAL	370	<5	5	μg/l
COBALT, TOTAL	75	<50	50	μg/l
COPPER, TOTAL	300	14	5	μg/l
CYANIDE, TOTAL	400	<10	10	μg/l
FLUORIDE, TOTAL	12,000	1,850	100	μg/l
IRON, TOTAL	3,100	318	50	μg/l
LEAD, TOTAL	100	<5	5	μg/l
MANGANESE, TOTAL	1,100	182	20	μg/l
MERCURY, TOTAL	2,000	<200	200	ng/l
MERCURY, TOTAL LOW LEVEL	Monitor	36	25	ng/l
MOLYBDENUM, TOTAL	410	135	10	μg/l

2012 PHYSICAL / CHEMICAL ANALYSES FACULATIVE POND # 3

EFFLUENT PARAMETER	DISCHARGE LIMIT	FACULTATIVE POND #3 CONCENTRATION	PRACTICAL QUANTITATION LIMIT	UNITS
NICKEL, TOTAL	550	57	20	μg/l
PHOSPHOROUS, TOTAL	5,000	133	20	μg/l
SELENIUM, TOTAL	40	<5	5	μg/l
SILVER, TOTAL	60	<10	10	μg/l
STRONTIUM, TOTAL	4000	1600	50	μg/l
SULFATE, TOTAL	Monitor	1,300,000	200000	μg/l
SULFIDE, TOTAL	2000	<100	100	μg/l
THALLIUM, TOTAL	50	<10	10	μg/l
TIN, TOTAL	10	<10	10	μg/l
TITANIUM, TOTAL	1000	<10	10	μg/l
VANADIUM, TOTAL	42	<20	20	μg/l
ZINC, TOTAL	500	<10	10	μg/l
AROCLOR 1016	Nondetect	<65	65	ng/l
AROCLOR 1221	Nondetect	<65	65	ng/l
AROCLOR 1232	Nondetect	<65	65	ng/l
AROCLOR 1242	Nondetect	<65	65	ng/l
AROCLOR 1248	Nondetect	<65	65	ng/l
AROCLOR 1254	Nondetect	<65	65	ng/l
AROCLOR 1260	Nondetect	<65	65	ng/l
ACENAPHTHLYENE	20	<5	5	μg/l
BENZIDINE	200	<25	25	μg/l
BENZO[A]ANTHRACENE	40	<5	5	μg/l
BENZO[B]FLUORATHENE	20	<5	5	μg/l
BENZOTHIAZOLE	10	<10	10	μg/l
BENZO[GHI]PERYLENE	5.5	<5	5	μg/l
BIS(2-CHLOROETHOXY)METHANE	30	<5	5	μg/l
BIS(2-CHLOROETHYL)ETHER	30	<5	5	μg/l
BIS(2-CHLOROISOPROPYL)ETHER	30	<5	5	μg/l
BIS(2-ETHYL HEXYL)PHTHALATE	50	<5	5	μg/l
4-CHLORO-3-METHYLPHENOL	20	<5	5	μg/l
2-CHLOROPHENOL	20	<5	5	μg/l
4-CHLOROPHENYL PHENYL ETHER	20	<5	5	μg/l
1,4-DICHLOROBENZENE	20	<5	5	μg/l
3,3'-DICHLOROBENZIDINE	70	<10	10	μg/l
2,4-DICHLOROPHENOL	20	<5	5	μg/l
DIETHYLPHTHALATE	40	<5	5	μg/l
2,4-DIMETHYPHENOL	20	<5	5	μg/l

2012 PHYSICAL / CHEMICAL ANALYSES FACULATIVE POND # 3

EFFLUENT PARAMETER	DISCHARGE LIMIT	FACULTATIVE POND #3 CONCENTRATION	PRACTICAL QUANTITATION LIMIT	UNITS
2,4-DINITROPHENOL	120	<25	25	μg/l
2,4-DINITROTOLUENE	30	<5	5	μg/l
HEXAMETHYLBENZENE	8	<5	5	μg/l
INDENO[1,2,3-C,D]PYRENE	5.5	<5	5.0	μg/l
2-METHYL-4,6-DINITROPHENOL	100	<25	25	μg/l
2-NITROPHENOL	20	<5	5.0	μg/l
PENTACHLOROPHENOL	20	<20	20.0	μg/l
PHENANTHRENE	30	<5	5.0	μg/l
2,4,6-TRICHLOROPHENOL	20	<5	5.0	μg/l
SEMI-VOLATILE ORGANICS (1)	10	<10	(10)	μg/l
PHENOLICS, TOTAL RECOVERABLE	220	<4	2	μg/l
2-CHLOROETHYLVINYL ETHER	20	<10	10	μg/l
DICHLORODIFLUOROMETHANE	10	<1	1	μg/l
METHYLENE CHLORIDE	20	<5.0	5.0	μg/l
VOLATILE ORGANICS (2)	10	<10	(10)	μg/l

NOTES:

- (1) Parenthetical reporting limit represents the highest reporting limit for USEPA Method 625 for those compounds not listed individually.
- (2) Parenthetical reporting limit represents the highest reporting limit for USEPA Method 624 for those compounds not listed individually. Value excludes Acrolein and Acrylonitrile which are analyzed by approved screen methodology per USEPA Method 624.

Appendix C

Proposed Pump, Piping, And Equipment Information

Secondary Containment Submersible Pump Data

(Goulds)



FEATURES

Impeller: Cast iron, semi-open, non-clog with pump-out vanes for mechanical seal protection. Balanced for smooth operation. Silicon bronze impeller available as an option.

Casing: Cast iron volute type for maximum efficiency. 2" NPT discharge.

Mechanical Seal: Silicon Carbide vs. Silicon Carbide sealing faces. Stainless steel metal parts, BUNA-N elastomers.

Shaft: Corrosion-resistant, stainless steel. Threaded design. Locknut on all models to guard against component damage on accidental reverse rotation.

Fasteners: 300 series stainless steel.

Capable of running dry without damage to components.

Designed for continuous operation when fully submerged.

EXTENDED WARRANTY AVAILABLE FOR RESIDENTIAL APPLICATIONS.

WE Series Model 3885

SUBMERSIBLE EFFLUENT PUMPS



Wastewater

APPLICATIONS

Specifically designed for the following uses:

 Homes, Farms, Trailer Courts, Motels, Schools, Hospitals, Industry, Effluent Systems

SPECIFICATIONS

Pump

- Solids handling capabilities: ¾" maximum.
- Discharge size: 2" NPT.
- Capacities: up to 140 GPM.
- Total heads: up to 128 feet TDH.
- Temperature: 104°F (40°C) continuous, 140°F (60°C) intermittent.
- See order numbers on reverse side for specific HP, voltage, phase and RPM's available.

MOTORS

- Fully submerged in high-grade turbine oil for lubrication and efficient heat transfer.
- Class B insulation on 1/3 11/2 HP models.
- Class F insulation on 2 HP models.

Single phase (60 Hz):

- Capacitor start motors for maximum starting torque.
- Built-in overload with automatic reset.

- SJTOW or STOW severe duty oil and water resistant power cords.
- ½ 1 HP models have NEMA three prong grounding plugs.
- 1½ HP and larger units have bare lead cord ends.

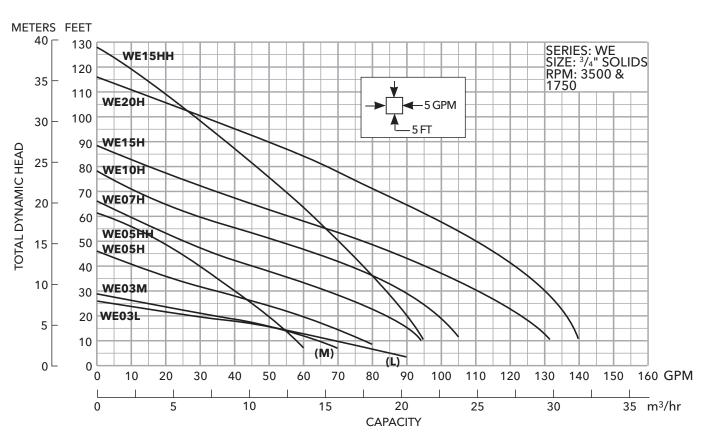
Three phase (60 Hz):

- Class 10 overload protection must be provided in separately ordered starter unit.
- STOW power cords all have bare lead cord ends.
- Designed for Continuous Operation: Pump ratings are within the motor manufacturer's recommended working limits, can be operated continuously without damage when fully submerged.
- Bearings: Upper and lower heavy duty ball bearing construction.
- Power Cable: Severe duty rated, oil and water resistant. Epoxy seal on motor end provides secondary moisture barrier in case of outer jacket damage and to prevent oil wicking. Standard cord is 20'. Optional lengths are available.
- O-ring: Assures positive sealing against contaminants and oil leakage.

AGENCY LISTINGS



Tested to UL 778 and CSA 22.2 108 Standards By Canadian Standards Association File #LR38549



Goulds Water Technology

Wastewater

MODELS

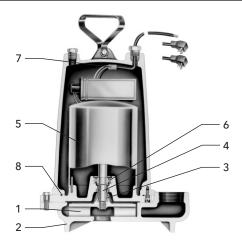
Order	НР	Phase	Volts	DDM	Impeller		Locked Rotor		Full Load		istance	Power	Weight							
Number	пг	rnase	voits	KFIVI	Diameter (in.)	Amps	Amps	Code	Efficiency %	Start	Line-Line	Cable Size	(lbs.)							
WE0311L			115			10.7	30.0	М	54	11.9	1.7									
WE0318L	1		208	1		6.8	19.5	K	51	9.1	4.2									
WE0312L			230	1,750	F 20	4.9	14.1	L	53	14.5	8.0	1.//2	F /							
WE0311M	0.33		115	1750	5.38	10.7	30.0	М	54	11.9	1.7	16/3	56							
WE0318M	1	1	208			6.8	19.5	К	51	9.1	4.2									
WE0312M	1		230			4.9	14.1	L	53	14.5	8.0									
WE0511H		1	115			14.5	46.0	М	54	7.5	1.0	14/3	60							
WE0518H			208			8.1	31.0	K	68	9.7	2.4									
WE0512H	1		230	1		7.3	34.5	М	53	9.6	4.0	16/3	60							
WE0538H	1		200	1	3.56	4.9	22.6	R	68	NA	3.8									
WE0532H	1		230	1	0.00	3.3	18.8	R	70	NA	5.8									
WE0534H	1	3	460	1		1.7	9.4	R	70	NA	23.2	14/4	60							
WE0537H	1		575	1		1.4	7.5	R	62	NA	35.3									
WE0511HH	0.5		115			14.5	46.0	M	54	7.5	1.0	14/3	60							
WE0518HH		1	208	-		8.1	31.0	K	68	9.7	2.4	14/3								
WE0512HH	-	'	230	-		7.3	34.5	M	53	9.6	4.0	16/3	60							
WE0538HH	-		200	-	3.88	4.9	22.6	R	68	NA	3.8									
WE0536HH	-			-	3.00	3.6	18.8	R	70	NA	5.8	-								
	-	3	230 460	-		1.8		R	70	NA	23.2	14/4	60							
WE0534HH WE0537HH			575	-		1.5	9.4 7.5	R	62	NA										
				-							35.3									
WE0718H		1	208	-		11.0	31.0	K	68	9.7	2.4	14/3	70							
WE0712H			230			-	-	-	1	-	-		10.0	27.5	J	65	12.2	2.7		
WE0738H	0.75		200		4.06	6.2	20.6	L	64	NA	5.7									
WE0732H		3	230			5.4	15.7	K	68	NA	8.6	14/4	70							
WE0734H			460			2.7	7.9	K	68	NA	34.2									
WE0737H			575			2.2	9.9	L	78	NA	26.5									
WE1018H		1	208			14.0	59.0	K	68	9.3	1.1	14/3	70							
WE1012H			230	3450		12.5	36.2	J	69	10.3	2.1									
WE1038H	1		200		4.44	8.1	37.6	М	77	NA	2.7									
WE1032H		3	230			7.0	24.1	L	79	NA	4.1	14/4	70							
WE1034H			460			3.5	12.1	L	79	NA	16.2		, 0							
WE1037H			575			2.8	9.9	L	78	NA	26.5									
WE1518H		1	208			17.5	59.0	K	68	9.3	1.1	14/3	80							
WE1512H			230			15.7	50.0	Н	68	11.3	1.6	1475	00							
WE1538H			200		4.56	10.6	40.6	K	79	NA	1.9									
WE1532H		3	230		4.30	9.2	31.7	K	78	NA	2.9	14/4	80							
WE1534H		3	460			4.6	15.9	K	78	NA	11.4	14/4	00							
WE1537H	1.5		575			3.7	13.1	K	75	NA	16.9									
WE1518HH	1.5	1	208			17.5	59.0	K	68	9.3	1.1	14/3	80							
WE1512HH	1	'	230	1		15.7	50.0	Н	68	11.3	1.6	14/3	00							
WE1538HH	1		200	1	F F0	10.6	40.6	K	79	NA	1.9									
WE1532HH]	2	230		5.50	9.2	31.7	K	78	NA	2.9	1 // //	00							
WE1534HH]	3	460	1		4.6	15.9	Κ	78	NA	11.4	14/4	80							
	1		575	1		3.7	13.1	Κ	75	NA	16.9	1								
WE1537HH			0,0																	
WE1537HH WE2012H		1	230			18.0	49.6	F	78	3.2	1.2	14/3	83							
		1					49.6 42.4	K		3.2 NA	1.2	14/3	83							
WE2012H	2		230 200		5.38	12.0	42.4		78											
WE2012H WE2038H	2	3	230		5.38			K		NA	1.7	14/3	83							

PERFORMANCE RATINGS (gallons per minute)

	der lo.	WE- 03L	WE- 03M	WE- 05H	WE- 07H	WE- 10H	WE- 15H	WE- 05HH	WE- 15HH	WE- 20H
	НР	1/3	1/3	1/2	3/4	1	1½	1/2	1½	2
	RPM	1750	1750	3500	3500	3500	3500	3500	3500	3500
	5	86	-	-	-	-	-	-	-	-
	10	70	63	78	94	-	-	58	95	-
	15	52	52	70	90	103	128	53	93	138
	20	27	35	60	83	98	123	49	90	136
-	25	5	15	48	76	94	117	45	87	133
Total Head Feet of Water	30	-	-	35	67	88	110	40	83	130
of V	35	-	-	22	57	82	103	35	80	126
eet	40	-	-	-	45	74	95	30	77	121
J PE	45	-	-	-	35	64	86	25	74	116
He	50	-	-	-	25	53	77	-	70	110
otal	55	-	-	-	-	40	67	-	66	103
12	60	-	-	-	-	30	56	-	63	96
	65	-	-	-	-	20	45	-	58	89
	70	-	-	-	-	-	35	-	55	81
	75	-	-	-	-	-	25	-	51	74
	80	-	-	-	-	-	-	-	47	66
	90	-	-	-	-	-	-	-	37	49
	100	-	-	-	-	-	-	-	28	30

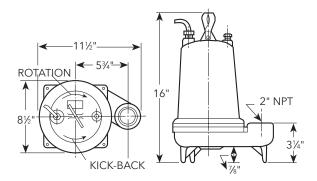
COMPONENTS

Item No.	Description
1	Impeller
2	Casing
3	Mechanical Seal
4	Motor Shaft
5	Motor
6	Ball Bearings
7	Power Cable
8	Casing O-Ring



DIMENSIONS

(All dimensions are in inches. Do not use for construction purposes.)





Xylem, Inc.

2881 East Bayard Street Ext., Suite A

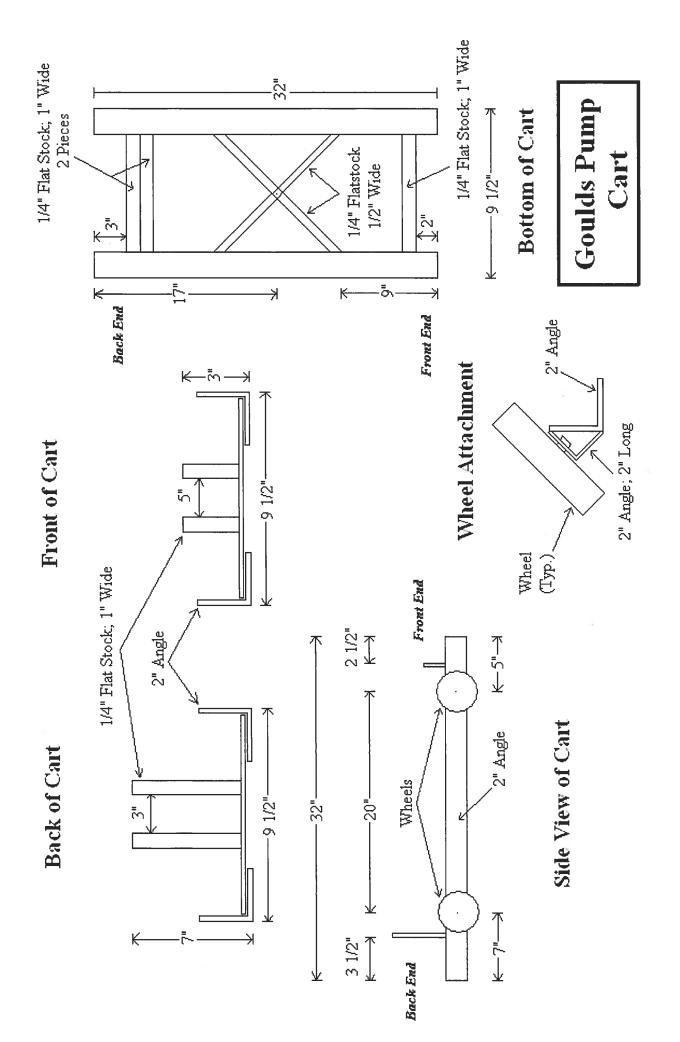
Seneca Falls, NY 13148 Phone: (866) 325-4210 Fax: (888) 322-5877

www.xyleminc.com/brands/gouldswatertechnology

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Pump Cart Shop Drawing

(CWM)



Flex Hose Cut Sheet

(Goodyear)





Plicord® Extremeflex™ BROWN

APPLICATION: A high-tech, flexible and versatile chemical hose capable of handling a wide variety of acids, alcohols, salt solutions and petroleum-based products.

CONSTRUCTION

TUBE: Black Chemrin® (CPE) synthetic rubber

COVER: Corrugated Brown Versigard® (EPDM) synthetic rubber with white spiral stripe

REINFORCEMENT: Spiral plied synthetic fabric with double wire helix

TEM PERATURE: -30°F to 275°F (-34°C to 135°C)

PACKAGING: 100' exact cut length, coiled, polyw rapped

BRANDING: Example: Goodyear[®] Plicord® ExtremeFlex™ Brown w / Chemrin® 150 PSI. Made In

Canada.

COUPLINGS: Use Goodyear® Engineered Products Insta-Lock™ Cam & Groove fittings with the product. See the Coupling Systems information pages at the back of the catalog.

NON-STOCK/SIZES: 400' min if not stocked.

ORDER CODES: 546-723

	ID	NO	M. OD	MAX	(.WP	BEND	RADIUS	VAC	UUM HG	WE	IGHT
in.	mm.	in.	mm.	psi	Мра	in.	mm.	in.	mm.	lb./ft.	kg./m.
1	25.30	1.42	36.00	150	1.03	1.50	38.10	29	737	0.50	0.75
1-1/4	32.00	1.63	41.50	150	1.03	2.00	50.80	29	737	0.57	0.85
1-1/2	38.00	1.92	48.70	150	1.03	2.25	57.20	29	737	0.74	1.10
2	51.20	2.44	61.90	150	1.03	3.00	76.00	29	737	0.97	1.45
3	76.20	3.54	89.80	150	1.03	4.50	114.00	29	737	1.80	2.68
4	102.10	4.57	116.10	150	1.03	6.00	152.00	29	737	2.47	3.68

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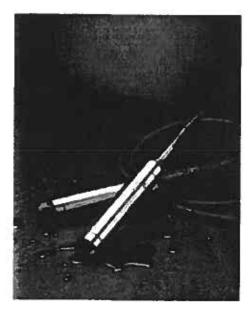


Level Transmitter

(Viatran)



LEVEL TRANSMITTER Model 517



FEATURES

- Submersible
- Less than 7/8" diameter
- Corrosion resistant construction
- Ranges from 30" WC to 1,200 ft WC/500 PSI (34 bar)
- Intrinsically Safe design available
- All stainless steel construction

TYPICAL APPLICATIONS

- Methane gas wells
- Down hole water wells
- Inground and underground tanks
- Water and sewage treatment plants
- Reservoirs / Dams
- Marine / Shipboard
- Chemical waste ponds

HYDROSTATIC HEAD PRESSURE TO **ACCURATELY MEASURE LEVEL**

If you choose to measure level through hydrostatic head pressure, then you can't do better than the Model 517 from Viatran. The Model 517 promises an accuracy to 0.1%.

And it's submersible. Meaning you can throw it in the tank and not worry about some of the things that Process Engineers have

to worry about - like the fog rolling in. The Model 517 will send you a reliable 4 to 20 mA output.

WHAT DOES RUGGED REALLY MEAN?

The Model 517 has been engineered to survive in hostile media. We're confident you can depend on the 517. Internal circuitry provides lightning protection, while a 4 to 20 mA output signal minimizes potential outside interference and signal degradation. All of this is critical if the signal needs to travel over long cable lengths (as in groundwater studies).

RUGGED FEATURES

The unique Viatran cable seal ensures watertight integrity up to 500 PSI (34 bar). Other potential leak paths are avoided by Viatran's all-welded sensor design. This design eliminates the O-ring seal.

OPTIONAL 1/4" NPT PRESSURE PORT

A removable end cap comes standard on the Model 517. However, if weight is needed, heavier end caps are available. The optional 1/4" NPT pressure port is critical for checking unit calibration against a known pressure source.

For more information, contact Viatran.



CE

Viatran 3829 Forest Parkway

Suite 500

Wheatfield, NY 14120

Hotline: 1-800-688-0030

Phone: 1-716-629-3800

Fax: 1-716-693-9162 solutions@viatran.com Email:



PERFORMANCE	Ω		0-3, 5, 10, 15, 30, 50, 100, 300, 500 PSI 0-80, 140, 275, 415, 555, 690, 830 inches water column
	Accuracy Combined		≤±0.1% FSO typical (±0.25% FSO max)
		Hysteresis & Repeatability	
		Full Scale Output (FSO)	
		Resolution	
		Zero Balance	
		Long Term Stability	
		Response time	≤1 mSec
		Temperature Effect on Zero	
		Temperature Effect on Span	≤±1.0% 100°F (37°C)
		Compensated Temperature Range	32°F to 185°F (0°C to 85°C)
		Operating Temperature	
			65°F to 250°F (-53°C to 121°C)
LECTRICAL		Supply Voltage	9 to 30 Vdc
		Power Supply Regulation	≤±0.0001% FSO per Volt
		Output Signal	4 to 20 mA
		Span	
		Circuit Protection	Output may be short-circuited indefinitely. Input polarity may bereversed. Over-voltage protected to 1000 volts. ≤1 mSec duration
		Electrical Connection.	3 wire 22 AWG
		Red	
		Black	
		Bare	
MECHANICAL		Pressure Connection	5/8" - 18 UN female thread with protective end cap installed
		Proof Pressure	3 limes rated range
		Burst Pressure	5 times rated range
		Diameter	0.875 inches
		Weight	Pressure capsule 10 oz.
		Cable Weight	11.3 lbs per 1000 feet (Polyurethane)
MATERIALS OF CONSTRUCTI	ON	Housing	316L stainless steel
		Pressure Connection Sensor	316L stainless steel
		Cable Options	316L stainless steel
		Mounting	Polyurethane, Tefzel
		identification	Laser etched onto body
		Cable Strength	Poly Wire - 30 lbs; Support Line - 100 lbs



THE SHAPE SEE THE

Model 517

CERTIFICATIONS (Consult Factory for Available Options)

FΜ

Intrinsic Safety Class I, II, III. Div. 1, Groups A thru G and AEx ia IIC T4, Indoor and Outdoor NEMA 4X Hazardous Locations

CSA

Intrinsic Safety Class I, Div.1, Ex ia IIC T4 Type 4 Enclosure

OPTIONS

Codes E

DN......Special range
DN......Improved accuracy

Note: Application of some available options may affect standard performance. Consult your Viatran Representative for details.

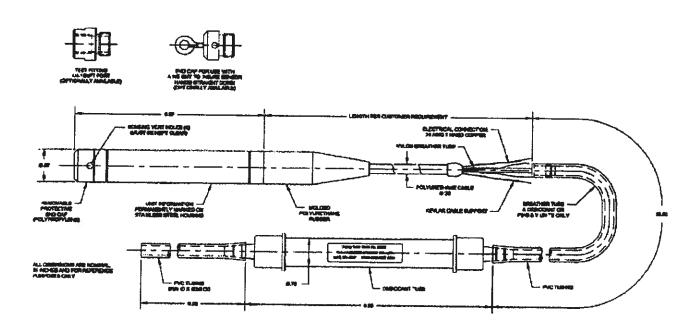
ACCESSORIES

Breather tube filer

Panel mount digital display

Pressure test fitting (1/4" NPT (F) screws into end cap threads)

Desiccant tube kit





Programmable Limit Alarm

(Moore)

Programmable Current/Voltage and RTD/Thermocouple Limit Alarm Trips

May 2010

Description

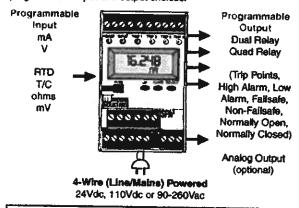
The universal SPA² Programmable Limit Alarm Trips provide on/off control, warn of unwanted process conditions, alarm on rate-of-change and provide emergency shutdown. Very versatile, they accept a signal input from transmitters, temperature sensors and a wide array of other monitoring and control instruments:

- Current and Voltage Signals
- 23 RTD Types
- 9 Thermocouple Types
- Resistance and Potentiometer Devices
- Direct Millivolt Sources

Dual and Quad Alarm Trip Outputs

The 4-wire (line/mains-powered) SPA² provides two or four independent and individually-configurable alarm relay outputs when a monitored process variable falls outside of user-set high and/or low limits. This is typically used to activate a warning light, annunciator, bell, pump, motor or shutdown system.

Figure 1. Available SPA² models deliver versatile and programmable input and output choices.



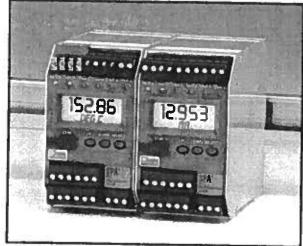
Certifications



Fectory Mutual - FM Approvals cFMus (US/Canada), Non-Incendive Class I, Division 2, Groups A, B, C, D
Suitable for use in General Locations and
Hazardous Classified' Locations when mounted in
suitable protective enclosures
NOTE: Models with the -DPDT option are not FM
approved)

(€

CE Conformant - EMC Directive 89/336/EEC EN 61326; Low Voltage Directive 73/23/EEC EN 61010



The SPA² features a metal, RFI resistant housing with display that snaps onto standard DIN-style rails.

Features

- Universal plant standard. There's no need to stock dozens of different fixed range alarm trips.
- 20-bit Input resolution. Delivers industrybest digital accuracy for both sensor (RTD and thermocouple) and analog (current/voltage) inputs.
- Site- and PC-Programmable. Featuring security password protection, the SPA² offers the choice of using front panel pushbuttons or our Windows⁹-based Intelligent PC Configuration Software for fast and simple set up.
- Long-term stability. Provides up to 5 years between scheduled calibrations.
- Large 5-digit process and status readout. A
 display shows menu prompts during pushbutton
 configuration and, when the SPA² is in operation,
 shows the process variable, the output or toggles
 between the two in selectable engineering units.
- Combined alarm trip and transmitter. The analog output (-AO) option reduces costs and installation time when both alarm and transmitter functions are needed at the same location.
- Isolated and RFVEMI protection. Delivers superior protection against the effects of ground loops, and plant noise, radio frequency and electromagnetic interference.

Programmable Current/Voltage and RTD/Thermocouple Limit Alarm Trips

Site- and PC-Programmable

Operating parameters configure quickly and easily using front panel pushbuttons or our Intelligent PC Configuration Software. Programmable functions include:

- Security password protection on/off and password
- Input type and measurement range (zero and full scale values)
- · Input and output trimming
- · High or low alarm(s) with trip points
- Failsafe or non-failsafe, and normally open or normally closed alarm relays
- Alarm deadband (0-100%) and alarm time delay
- T/C reference junction compensation (on/off)
- Display parameters (scale, engineering units, and set number of digits after the decimal point)
- Differential or averaging of RTD inputs
- Standard and custom linearization curves (up to 128 points)*
- Analog output range**
- On input failure, upscale or downscale drive, fail to last value or fail to selected value**
- Analog signal output damping (0-30 seconds)**

Powers a 2-Wire Transmitter

The SPA² (HLPRG: current/voltage input model) comes standard with 2-wire transmitter excitation that provides 24Vdc to power the loop. This saves the cost of specifying and installing an additional instrument power supply to power a 2-wire transmitter on the input loop.

Figure 2. The SPA² provides transmitter excitation to power a 2-wiretransmitter.

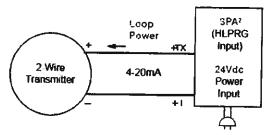
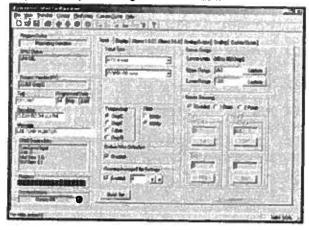


Figure 3. In addition to pushbutton configuration, the SPA² programs quickly from a single software window.



Versatile Alarm Options

Each individually-configurable SPA² alarm trip relay programs via the PC software as a:

High or Low Limit Process Alarm—Monitor a temperature, pressure, level, flow, position or status variable, and use to warn of unwanted process conditions (Figure 4), provide emergency shutdown or provide on/off control (Figure 5).

Rate-of-Change Alarm—Monitor an input for a change in value with respect to time (Figure 6). The alarm trips when the input rate-of-change exceeds a user-selected rate (Delta) over a user selected time period (Delta Time).

Input Fault Alarm—Setting one of the alarm's relays to trip on input or self-diagnostic failure (without affecting the other relay being used to monitor the process) is typically implemented to warn of a failure, such as a broken sensor, without tripping more critical process alarms or shutting down the process.

Out of Range Alarm—Monitor your process variable (PV). If the value strays past user-set limits, the SPA² will go into an alarm state indicating that the PV has gone out of the allowed range.

Self-Diagnostic Alarm—The SPA² checks its own operation and configuration upon start up, and then continuously monitors its status during operation. One of the SPA²'s relays can be configured to trip if it senses that it is not operating properly.

Quick Ranging Calibration

Using the front panel pushbuttons or the PC Configuration Software (instead of potentiometers which can drift), precise zero and span settings can be made in seconds. Just select the zero and span values, and the push of a button locks the values into the alarm trip's memory.

^{*}Programmable via the PC Configuration Software only.

[&]quot;Models with Arraing Output (-AO) option.

Figure 4. High and/or low limit alarms, with a selectable deadband to reduce faise alarms, can be used to warn of unwanted process conditions or to provide emergency shutdown.

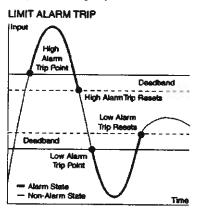


Figure 5. The SPA² can be used as a simple on/off controller such as those required in level applications (pump/valve control) when filling or emptying a container or tank.

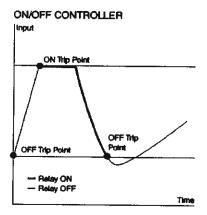
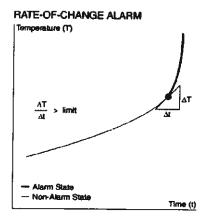


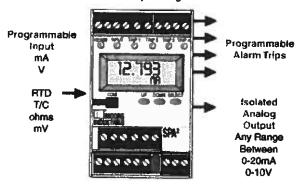
Figure 6. The SPAP can be set to trip when the input rate-of-change exceeds a user-selected rate (Delta) over a user-selected time period (Delta Time)...



Combination Alarm and Isolated Transmitter

When ordered with the Analog Output (-AO) option, the SPA² provides a proportional and isolated analog retransmission of the input signal that can be sent to remote monitoring/control devices like a DCS, PLC, PC, indicator or data recorder (Figure 7). All analog parameters can be selected using the SPA² pushbuttons or the Intelligent PC Configuration Software. Upon input failure, the analog output can be user-set for upscale or downscale drive or fail to last value.

Figure 7. When ordered with the Analog Output (-AO) option, the SPA* is a combination alarm trip and signal transmitter.



Superior Reference Junction Compensation

Uncompensated plastic terminals are very susceptible to ambient temperature changes that may result in readings that are "off" by several degrees. SPA2 models that accept temperature inputs (TPRG input) feature metal terminals and advanced electronic compensation techniques that provide a stable measurement in fluctuating ambient temperature conditions.

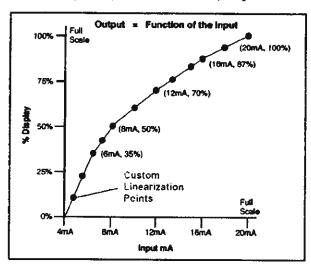
Continuous Self-Diagnostics

Incorporating advanced self-diagnostics, the SPA² checks its own operation and configuration upon start up and then continuously monitors its status during operation. If it senses that it is not operating properly, it displays an error message on its display indicating what condition has occurred. In addition, one or more of the alarm trip outputs can be set as a fault alarm which will trip when an unwanted diagnostic condition occurs.

Programmable Current/Voltage and RTD/Thermocouple Limit Alarm Trips

Custom 128-Point Linearization Curves
The ability to plot a custom linearization curve is
beneficial when non-linear input signals must be converted to linear output representations (Figure 8).
Typical applications include monitoring a non-linear transducer, the level of odd-shaped tanks and flow meter linearization.

Figure 8. Using the Intelligent PC Configuration Software, up to 128 custom linearization points can be selected and saved in the SPA2's memory to compensate for non-linear input signals.



Total Sensor Diagnostics for RTD Inputs Our SPA² Programmable Limit Alarm Trip (TPRG input model) performs continuous sensor diagnostics (Figure 10). This industry-first and patented Moore Industries feature saves you time and money by letting you know when a problem occurs, and its type and location. If the RTD input breaks, the user can decide whether or not to trip one or more alarms to indicate trouble. A plain-English error message on the display, as well as on the PC Configuration Software, indicates exactly which RTD wire has broken. Specific error messages eliminate the work of removing the sensor or checking all lead wires to diagnose a problem. If equipped with the Analog Output (-AO) option, the user has the option of driving the analog output either upscale or downscale on sensor failure.

Trim to Specific Curve Segments
The SPA² can be trimmed with two data points within
the selected zero and span measurement range
(Figure 9). This allows a complete process range to
be monitored while placing measurement emphasis
on a critical segment of the range. This provides
incredible precision over a limited portion of the span
while measuring the remainder of the span with
outstanding accuracy.

Figure 9. The SPAF can be set to measure the segment most critical to the process.

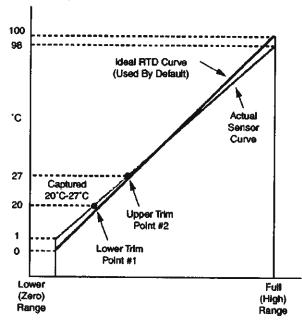
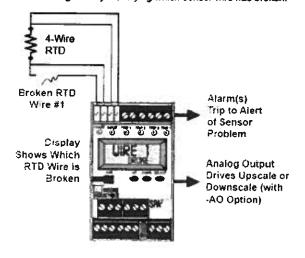


Figure 10. Patented "Total Sensor Diagnostics" saves troubleshooting time by identifying which sensor wire has broken.



Specifications (HLPRG: mA and V Input Model)

Performance Alarm Trip Repeatability: Current Inputs, ±2 microamps (0.01% of 20mA span); Voltage Inputs, ±1mV (0.01% of maximum span) Display Accuracy: ±1 digit; when scaling the display (or in Custom Mode), high input-todisplay span ratios decrease display accuracy Input Accuracy: Current inputs, ±2 microamps (0.01% of 20mA span); Voltage Inputs, ±1mV (0.01% of maximum span) Stability: Refer to Table 1 Deed Band: 11.5V or 50mA, maximum in Linear Mode; equivalent of maximum input range in user-set engineering units in Scaling/Custom Mode Response Time: 256msec maximum (Defined as the time from step change on input to alarm state change when alarm is set to trip mid-point) Alarm Trip Delay: Programmable from 0-120 seconds Line Voltage Effect: ±0.002% of span for a 1% change in line voltage (AC or DC) Isolation: 1000Vms between case, input, output (units with -AO option) and power, continuous. Will withstand a 1200Vac dielectric strength test for one minute (with no breakdown) WITH -RF OPTION: 500Vrms between case, input, output and power **Power Supply:** 24DC range, 18-30Vdc; UAC range, 90-260Vac: 110DC range, 75-150Vdc **Power Consumption:** 3.5W maximum (24DC

Performance supply); 4W maximum (UAC (continued) supply); 6W maximum (110DC supply)

Input Impedance: Current Inputs, 20 ohms; Voltage Inputs, 1 Mohm input Over-Range Protection: Voltage Inputs, ±30Vdc: Current Inputs, ±100mA TX Power Supply: 24Vdc,

Performance WITH ANALOG OUTPUT with Analog Output Accuracy: Current, Output (-AO ±0.01% of maximum span (±2 Option) microamps); Voltage, ±0.01%

of maximum span (±1mV)

±10%@24mA (regulated)

Response Time: 256msec maximum (128msec typical) for the output to change from 10% to 90% of its scale for an input step change of 0 to 100% Ripple (up to 120Hz): Current output, 10mVp-p when measured across a 250 ohm resistor; Voltage output, 50mVp-p maximum **Output Limiting:**

Output | Failure Limits 0-20mA 0, 23.6mA 4-20mA 3.6, 23.6mA X-20mA (90% of X), 23.6mA Voltage output, -0.5-11V Load Effect (current outputs): ±0.01% of span from 0 to 1000 ohms resistance on current output

Current outputs.

Ambient Operating Range: Conditions -40°C to +85°C

(-40°F to +185°F) Relay Range: -25°C to +70°C (-13°F to +158°F) Storage Range: -40°C to +85°C (-40°F to +185°F)

Ambient Temperature Effect: Current, 2 microamps/°C; Voltage, 1mV/°C; Output,

Ambient ±0.009% of maximum Conditions span/°C (continued) Relative Humidity:

0-95%, non-condensing **RFVEMI Protection:** 10V/m@80-1000MHz. 1kHz AM, when tested to IEC61326 with 0.5% of span or less error WITH -RF OPTION: 20V/m@80-1000MHz. 1kHz AM, when tested to IEC61326 with 0.5% of spen or less error **Noise Rejection:** Common Mode 100dB@50/60Hz Normal Mode, Current input, 70dB typical@50mAp-p@ 50/60Hz; Voltage Input, 70dB typical @ 1Vp-p @ 50/60Hz

Adjustments Front panel pushbuttons control settings for zero, span, alarm trip points, high/low alarms, etc.; Internal jumper and menu password protect parameter settings

Indicators LCD: 2x5 14-segment characters, backlit, alphanumeric readout accurate to the nearest dialt.

Range: -99999 to 99999; Decimal point can be user-set LED Type: INPUT LED: **Dual color LED Indicates** input faiture READY LED: Green LED Indicates unit is operating property ALARM 1, 2, 3 and 4 LED: Dual color LED per relay

indicates alarm status

Weight 544 g to 601 g (19.2 oz to 21.2 oz)

Table 1. Long-Term Stability

Stability (% of Maximum	Inpu	rt-to-Ou {Years}	tput		ut-to-Re (Years)				
Span)	1	3	5	1	3	5			
Current Inputs	0.081	0,14	0.18	0.047	0.081	0.105			
Voltage Inputs	0.093	0.16	0.21	0.066	0_114	0.147			

Programmable Current/Voltage and RTD/Thermocouple Limit Alarm Trips

Specifications (TPRG: RTD, T/C, Ohm, mV and Potentiometer Input Model)

<u>-p</u>	tanono (n na.	1110, 170,	min, my and Potenti	omerer inb	ut Model)
Performance		Performance (continued)	(UAC supply): 6W maximum (110DC supply) Input Over-Range Protection: ±5Vdc Input Impedance: T/C inputs, 40 Mohms, nominal Input Over-Range Protection: ±5Vdc Excitation Current: (RTD and Ohms) 250 microamps, ±10% WITH ANALOG OUTPUT Output Accuracy: Current, ±0.01% of maximum span (±2 microamps): Voltage, ±0.01% of maximum span (±1mV) Response Time: 256msec maximum (128msec typical) for the output to change from 10% to 90% of its scale for an input step change of 0 to 100% Ripple (up to 120Hz): Current output, 10mVp-p when measured across a 250ohm resistor; Voltage output, 50mVp-p maximum Output Limiting: Current outputs, Cutput Fallure Limits 0-20mA 0, 23.6mA 4-20mA 3.6, 23.6mA Voltage output, -0.5-11V Load Effect (current outputs): ±0.01% of span from 0 to 1000 ohms resistance on current output Operating Range: -40°C to +85°C (-40°F to +185°F) Retay Range: -25°C to +70°C (-13°F to +185°F) Storage Range: -40°C to +85°C (-40°F to +185°F)	Ambient Conditions (continued) Adjustments	Ambient Temperature Effect: Refer to Table 4 Effect of Ambient Temperature on Reference Junction Compensation (T/C inputs only): ±0.005% per °C change of ambient temperature Relative Humidity: 0-95%, non-condensing RFI/EMI Protection: 10V/m@80-1000MHz, 1kHz AM, when tested to IEC61326 with 0.5% of span or less error WITH -RF OPTION: 20V/m@80-1000MHz, 1kHz AM, when tested to IEC61326 with 0.5% of span or less error Noise Rejection: Common Mode, 100dB@50/60Hz Normal Mode, refer to Table 5 Front panel pushbuttons control settings for zero, span, alarm trip points, high/low alarms, etc.; Internal jumper and menu password protect parameter settings LCD: 2x5 14-segment characters, backlit, alphanumeric readout accurate to the nearest digit. Range: -99999 to 99999; Decimal point can be user-set LED Type: INPUT LED: Dual color LED indicates input failure READY LED: Green LED indicates unit is operating properly ALARM 1, 2, 3 and 4 LED: Dual color LED per relay indicates alarm status
	supply); 4W maximum			Weight	544 g to 601 g (19.2 oz to 21.2 oz)

Programmable Current/Voltage and RTD/Thermocouple Limit Alarm Trips

input	Туре	a	Ohms	Conformance Range	Minimum Span	Input Accuracy/ Repeatability	Maximum Range
RTD			100				-
(2-, 3-,			200	7		Į.	
4-Wire)		1	300	7			
Dual			400	-200 to 850°C	1	9	-240 to 960°C
(2-Wire,			500	(-328 to 1562°F)			(-400 to 1760°F)
one 2-Wire and One			1000	†			
3-Wire)	1	0.003850	Duat 500	†			
Tripte			Dual 1000	-200 to 260°C (-328 to 500°F)			-200 to 260°C
(2-Wire)			Triple 500	-200 to 440°C (-328 to 824°F)		±0.1°C (±0.18°F)	(-328 to 500°F) -200 to 440°C
	Platinum		Triple 1000	-200 to 80°C (-328 to 176°F)			(-328 to 824°F) -200 to 80°C (-328 to 176°F)
	Fiaunum		100		10°C	1	1 320 10 110 17
			200		(18°F)	-	
			400	-100 to 650°C			-150 to 720°C
			500	(-148 to 1202°F)			(-238 to 1328°F)
		0.000000	1000		1:		
	1	J.003302	Dual 500	100 1- 2000	F		
			Dual 1000	(-148 to 500°F)			-100 to 260°C (-148 to 500°F)
()		A03	-100 to 440°C				
			}	(-148 to 824°F)			
	1		11gHZ 1000				(-148 to 176°F)
			100	(-328 to 950°F)			-240 to 580°C (-400 to 1076°F)
	Nickel		120	(-112 to 608°F)			-100 to 360°C (-148 to 680°F)
-	Copper	0.00427	400 500 1000 Dual 500 Dual 1000 Triple 500 Triple 1000 120 120 9.035 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0				-65 to 280°C
			0-4000			{£1.55°F}	(-85 to 536°F)
	Direct Resistance	***			10 ohms	40.4 mbms	0-4095 ohms
Ohms		0.003962 0.00396 0.003916 0.00672 0.00427		The second second		£U.4 ORMS	0-2000 ohms
	Potentiometer				10%	40.1%	0-1300 ohms 0-100%
1	J	n/a	n/a	-180 to 760°C	35°C		-210 to 770°C
1	Ţ		14.0	(-292 to 1400°F)	(63°F)	(±0.45°F)	(-346 to 1418°F)
	к	n/a	n/a	-150 to 1370°C (-238 to 2496°F)	40°C	±0.3°G	-270 to 1390°C
				-170 to 1000°C	(72°F) 35°C	(±0.54°F) ±0.2°C	(-454 to 2534°F)
1	E	n/a	n/a	(-274 to 1832°F)	(63°F)	(±0.36°F)	-270 to 1013°C (-454 to 1855.4°F)
-	T	n/a	n/a	-170 to 400°C	35°C	±0 25°C	-270 to 407°C
1			_	(-274 to 752°F)	(63°F)	(±0 45°F)	(-454 to 764.6°F)
T/C	R	n/a	n/a	0 to 1760°C (32 to 3200°F)	50°C (90°F)	±0.55°C (±0.99°F)	-50 to 1786°C
1	3	o/a		0 to 1750°C	50°C	10 55°C	(-58 to 3246.8°F) -50 to 1786°C
		194	n/a	(32 to 3200°F)	(90°F)	(±0 99°F)	(-58 to 3246.8°F)
į	В	n/a	n∕a	400 to 1820°C (752 to 3308°F)	75°C (135°F)	t0.75°C (±1.35°F)	200 to 1836°C (392 to 3336.8°F)
	N	11/2	n/a	-130 to .1300°C {-202 to 2372°F}	45°C (81°F)	£0.4°G (±0.72°F)	-270 to 1316°C (-454 to 2400.8°F)
	С	n/a	r∀a	0 to 2300°C (32 to 4172°F)	100°C (180°F)	±0 8°C (±1.44°F)	0 to 2338°C (32 to 4240.4°F)
mV	DC	n/a	n/a	n/a	4mV	±30 microvotts	-50 to 1000mV

Programmable Current/Voltage and RTD/Thermocouple Limit Alarm Trips

Ordering Information

Unit	Input	Output	Power	Options	Housing
SPA2 Programmable Limit Alarm Trip	HLPRG Programs to accept: Current: Any range between 0-50mA including: 0-20mA 4-20mA 10-50mA Voltage: Any range between 0-10Vdc including: 0-5Vdc 1-5Vdc 0-10Vdc TPRG Programs to accept (see Table 2 for details): RTD: 2-, 3- and 4-wire; ptetinum, copper, and nickel Thermocouple: J, K, E, T, R, S, N, C, B Chms: 0-4000ohms (Potentiometer, 4000ohms (Potentiometer, 4000ohms maximum) Millivolts: -50 to +1000mV	2PRG Dual Retays (Relays are single-pole/double-throw (SPDT, 1 form C, rated SA@250Vac, 50/60Hz or 24Vdc, non-inductive) 4PRG Quad Relays (Relays are single-pole/double-throw (SPDT), 1 form C, rated SA@250Vac, 50/60Hz or 24Vdc, non-inductive) Each relay individually configures for: High or Low Trip Normally Open or Normally Closed Fallsafe or Non-Fallsafe	24DC ±10% 110DC 75-150DC UAC Accepts any power input range between 90-260Vac	-AO Analog output (Isolated and linearized) scaleable for any range between 0-20mA Into 1000 ohms or 0-10V into 10 kohms (see "Specifications" for additional information) NOTE: Current output can be user-set for internal or external power (source or sink) -DPDT Relays are double-pole/double-throw (DPDT), 2 form C, rated 5A Ø250Vac, 50/60Hz or 24Vdc, non-inductive (2PRG output model only) NOTE: Models with the -DPDT option are not FM approved) -RF Enhanced RFI/EMI protection (see "Specifications" for details) -FMEDA Unit comes with Fallure Modes, Effects and Diagnostic Analysis (FMEDA) data for evaluating the instrument for suitability of use in a safety-related application	DiN Universal DiN-style housing mounts on 32mm (EN50035) G-type and 35mm (EN50022) Top Hat DIN-rails FLD Externally- mounted flange provides a secure mount

When ordering, specify: Unit / input / Output / Power / Options [Housing] Model number example: SPA2/TPRG/2PRG/24DC/- AO-RF [DIN]

Table 3. Long-Term Stability

Stability (% of Maximum		it-to-Oi (Years			ut-to-F (Years	
Span)	1	3	5	1	3	5
RTD, Ohm & Pot Inputs	0.09	0.16	0.21	0.047	0.081	0.104
T/C & mV Inputs	0.08	0.14	0.18	0.008	0.014	0.019

Table 5. Normal Mode Rejection Ratio

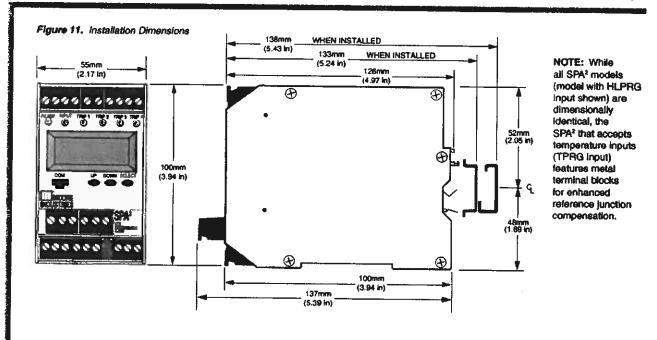
Sensor Ty	/pe	Max. p-p Voltage Injection for 100dB at 50/60Hz				
T/C: J, K, N	, C, E	150mV				
T/C: T, R,	S, B	80mV				
Pt RTD: 100, 200	, 300 ohms	250mV				
Pt RTD: 400, 500,	1000 ohms	1V				
NI: 120 of		500mV				
Cu: 9.03 o	hms	100mV				
Resistance	mV					
1-4 kohms	250-1000	1V				
0.25-1 kohms	62 5-250	250mV				
0.125-0.25 kohms	31.25-62.5	100mV				

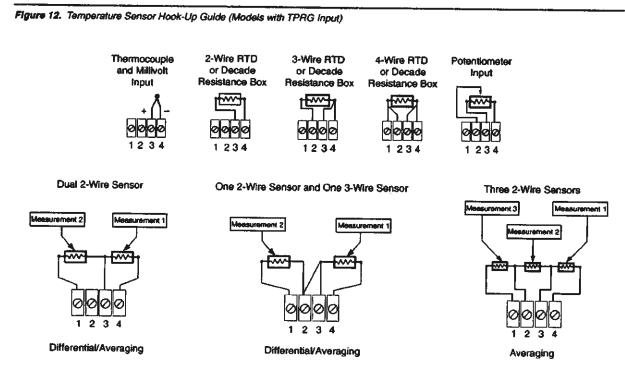
Table 4. Ambient Temperature Effect

	Accuracy per 1°C (1.8°F) Change in Ambien
RTD*	0.0035°C
Millivolt	0.5 microvolts + 0.005% of reading
Ohm	0.002 ohms +0.005% of reading
	Thermocouple
	Accuracy per 1°C (1.8°F) Change in Ambient
J	0.00016°C + 0.005% of reading
К	0.0002°C + 0.005% of reading
E	0.00026°C + 0.005% of reading
T	0.0001°C + 0.005% of reading
R, S	0.00075°C + 0.005% of reading
В	0.0038°C + 0.005% of reading
N	0.003°C + 0.005% of reading
С	0.00043°C + 0.005% of reading
mV	0.5 microvolts + 0.005% of reading

"Accuracy of Ni672 is 0.002°C

Programmable Current/Voltage and RTD/Thermocouple Limit Alarm Trips





Programmable Current/Voltage and RTD/Thermocouple Limit Alarm Trips

Table 6. Terminal Designations (Models with TPRG Input)

Input Type					Top Termin	als (Left t	o Right)	·								
in pocitype	T1	T2	Т3	T4	T5	T6	17	T8	T9	T10						
RTD, Ohm, Potentiometer, T/C & mV Inputs		See Fig	june 12		MPI	MR	+lo Source	-io Source +io Sink	+V0	-Vo -lo Sink						

Output Type		Mid	die Termin	als (Left t	o Right)	
	11	12	13	14	15	16
2PRG (SPDT Relays)	N/A	N/A	N/A	N/A	N/A	N/A
4PRG (SPDT Relays)	NO3	CM3	NCS	NO4	CM4	NC4
2 OPDT Relays	Relay 2 NO1	Relay 2 CMI	Relay 2 NC1	Fieley 2 NO2	Fletay 2 CM2	Relay 2 NC2

Output/Power Type				Во	ttom Term	inala (Left (o Right)			
	81	B2	B3	84	B \$	B6	87	B8	B9	B10
2PRG (SPDT Relays)	NOI	CM1	NC1	NO2	CM2	NC2	Not Used	AC or DC	ACC of DCC	GNO
4PRG (SPDT Relays)	NOt	CMf	NC1	NO2	CM2	NC2	Not Used	AC or DC	ACC or DCC	GND
2 DPDT Relays	Relay 1 NO1	Relay 1 CM1	Relay 1 NC1	Fleley 1 NO2	Ralay 1 CM2	Relay 1 NC2	Not Used	AC or DC	ACC Of DCC	GND

NOTES:

KEY:
AC or DC = Power Input
ACC or DCC = Power Input
CM = Relay Correron
DPDT = Ooutole-Pole/Double-Throw

GND = Ground (case)

io = Current Output MR = Manual Reset NO = Normally Open NC = Normally Closed

Sink = Current Sink Source = Current Source SPOT = Single-Pole/Double-Throw Vo = Voltage Output

Accessories

Each SPA2 order comes with one copy of our Intelligent PC Configuration Software and a configuration cable. Use the chart below to order additional parts.

Part Number 750-75E05-01	Intelligent PC Configuration Software (One copy provided free with each order)
Part Number 803-053-26	Configuration Cable for use in connecting the SPA ² to a PC (one cable provided free with each order)
Part Number 208-836-00	USB Communication Cable

^{1.} Terminal blocks can accommodate 14-22 AWG solid wiring.

the first input power requirement (AC or DC / ACC or DCC) will depend upon your unit's power need.

Programmable Current/Voltage and RTD/Thermocouple Limit Alarm Trips

Table 7. Terminal Designations (Models with HLPRG Input)

Input Type				To	op Termini	nis (Left te	Right)								
	T1	T2	Т3	T4	T5	T6	17	T8	T9	T10					
Current Input	Τx	+1	COM	Not Used	MR	MR	+lo Source	-lo Source +lo Sink	+Vo	-Vo					
Voltage Input	Tx	Not Used	COM	+٧	MR	MR	+lo Source	-lo Source +lo Sink	+V6	-Vo					

Output Type	Middle Terminals (Left to Right)							
	11	12	13	14	15	16		
2PRG (SPDT Relays)	NA	N/A	NA	N/A	NA	N/A		
4PRG (SPDT Relays)	NOS	CMS	NC3	NO4	CM4	NC4		
2 DPDT Relays	Relay 2 NO1	Relay 2 CM1	Relay 2 NC1	Fletey 2 NO2	Reley 2 CM2	Pielay 2 NC2		

Output/Power Type		Bottom Terminals (Left to Right)								
	B1	B2	B3	84	B5	B6	B7	B8	B9	B16
2PRG (SPDT Relays)	NOt	CM1	NC1	NO2	CM2	NC2	Not Used	AC or DC	ACC or DCC	GND
4PRG (SPDT Relays)	NOI	CM1	NGI	NO2	CM2	NC2	Not Used	AC or DC	ACC or DCC	GND
2 DPDT Relays	Relay 1 NO1	Relay 1 CM1	Relay 1 NC1	Relay I NO2	Fleisy 1 CM2	Relay 1 NC2	Not Used	AC or DC	ACC or DCC	GND

NOTES:

1. Terminal blocks can accommodate 14-22 AWG solid wiring, tighten to four inch-pounds (maximum).

2. ±lo/±Vo labeling is present only when the unit is equipped with the Analog Output (-AO) option.

3. Your input power requirement (AC or DC / ACC or DCC) with depend upon your unit's power need.

MEY:
AC/DC = Power Input
AC/DCC = Power Input
CM = Relay Common
COM = Anatog Common
DPOT = Double-Pole/Double-Throw
GND = Ground (case)

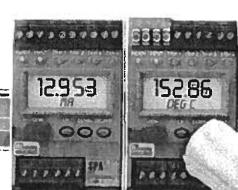
I = Current Input
Io = Current Output
IMR = Manual Reset
INO = Normally Open
INC = Normally Closed
Sink = Current Sink

Source = Current Source SPDT = Single-Pole/Double-Throw TX = Power for 2-wire transmitter V = Voltage Input Vo = Voltage Output

Programmable Current/Voltage and RTD/Thermocouple Limit Alarm Trips

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- Signal Isolator and Converter
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- 2-Wire Transmitter Power Supply (Transmitter Excitation)



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- · Sense dangerous conditions and shut down control equipment before it is damaged.
- · Compare two variables and trip an alarm when the difference between the two exceeds a preset value.
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fech Specs	Additional Information	Compliance & Restrictions	MSDS	Required Accessories	Optional Accessories	Alternate Products	Repair Parts
item	-	Switch					
Type			lly Actuated Dr	Read			
Wire Gauge		72	-,	,			
Overall Length		3.38					
Float Length (ln.)	2					
Float Dia. (In.)		2					
Fitting		14*NPT					
VA Rating		100					
Max. Temp. (C)	200					
Max. Pressure	(PSI)	500					
Operation		NO/NC					
Stem Length (n.)	2.63					
Stem Material		316 SS					
Float Material		316.88					
Mounts		Vertical					
Wire Lead		24					

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ECN #08-490 . Effective Date 04/09 . MF-002, Rev. J

General Information

- 1. Switches should be installed rigidly so the float or floats are free to move as the liquid level changes.
- 2. Switches should be mounted in a tank area free of severe turbulence or protected from such turbulence by appropriate and adequate slosh shields.
 Vertical switch stems should be vertical for best results.
- but satisfactory operation is possible in most liquids with the stem at up to a 30° angle from vertical.
- 4. Side mount switch stems must be mounted with the arrow vertically either up or down depending on switch operation
- Care should be taken that switches are always operated within electrical ratings.
- Orientation for standard Vertical switches can be changed from normally open to normally closed dry or vice versa by removing the float and reversing it in the stem, except with the M3328.

Wire Table for Reed Switch						
Model	GA	Color				
MT3920-1, -2, -3 MT5000-1, -2, -3, -4 MT8000-1, -2	22 22 22	Brown Black White				

Note: Temperature lead wires normally smaller gauge size

Información General

- 1. Los interruptores deben de ser instalados rigidamente de manera que el flotador o los flotadores tengan libertad de movimiento cuando cambie el nivel de líquido.
- 2. Los interruptores deben de ser montados en un área del tanque que esté libre de turbulencia severa o protepidos de tal turbulencia con protectores de chapoteo apropiados.
- 3. Los vástagos de interruptor vertical deben de estar verticales para obtener óptimos resultados, pero es posible lograr una operación satisfactoria en la mayoría de los líquidos si el vástago está a un ángulo de hasta 30º de la ilinea vertical.
- Los vástagos de interruptor de montaje lateral deben ser montados con la flecha en posición vertical, ya sea hacia arriba o hacia abajo, dependiendo de la operación del interruptor.
- 5. Hay que tener cuidado para que los interruptores siempre
- sean operados a los niveles eléctricos correspondientes. 8. Se puede cambiar la orienteción para interruptores verticales estándar de normalmente cerrada a normalmente ablerta seca o viceversa, retirando el flotador y colocándoto en el sentido opuesto en el vástago, excepto con el M3326.

Mainteanner

Maintenance, should opnotes of inspection to see that the float is free to move and not coated with any substance, which would change its weight or volume significantly. If this occurs, the float should be cleaned. This is easily accomplished without disturbing the Installation. In addition. the stem may be wiped down to remove any build-up.

The only repair possible in the field is replacement of either the float or stem. Dents or nicks on the float are usually of no consequence to operation.

mantenimiento debe consistir en una inspección para rificar que el flotador tenga libertad de movimiento y que no esté cubierto de ninguna sustancia que podria cambiar significativamente su peso o volumen. Si esto ocurre, deberá limpiar el fiotador. Esto se logra fácilmente sin alectar la instalación. Además, el vástago puede timplarse hacia abajo para quitar cualquier acumulación.

La única reparación de campo posible es el reemplazo del flotador o del vástago, Las aboltaduras o metaduras en el flotador normalmente no tienen consecuencias pera su operación.

Cautions

- 1. The pressure, temperature and electrical limitations shown for the specified level switches must not be exceeded.
- The pressures and temperatures must take into consideration possible surges in the temperature and
- pressure of the system.

 3. The liquids used must be compatible with the materials of construction. Specifications of materials will be given upon request.
- 4. Life expectancy of the switch varies with applications
- 4. Life expectancy of the switch varies with applications. Contact the factory if life cycle testing is required.
 5. Ambient temperature changes can affect switch set points, since specific gravities of liquids vary with temperature. Consult factory for assistance.
 6. Level switches have been designed to be shock and vibration resistant. For maximum life, both shock and vibration resistant. For maximum life, both shock and vibration should be minimized. Consult factory for
- vibration should be minimized. Consult factory for
- 7. Excessive contaminants in fluid may inhibit float operation, and occasional wipe down may be necessary. Level switches must not be field repaired
- Physical damage to product may render product unserviceable.
- 10. Installation in a vessel made from magnetic materiets may affect operation.

Procescience

- Los limites de presión, temperatura y electricidad mostrados. para los interruptores de nível especificados no deben ser excedition.
- 2. Las presiones y temperaturas deben torner en consideración posibles fluctuaciones en la temperatura y la presión del sistema.
- 3. Los liquidos usados tienen que ser competibles con los materiales de construcción. Las especificaciones de los materiales se brindarán a pedido.
- 4. La vida del interruptor varia según la aplicación. Comuniquese con la fábrica si se requieren pruebas cicilicas de la
- 5. Los cambios en la temperatura ambiente pueden afectar los puntos fijos del interruptor, dado a que el peso específico de los figuidos varía con la temperatura. Consulte con la tébrica si
- 6. Los interruptores de nivel han sido diseñados para ser resistentes a golpes y vibraciones. Para una máxima vida útil, se debe minimizar la cantidad de golpes y vibraciones. Consulte con la fábrica si requiere asistencia.

 7. El acceso de conterminantes en el liquido puede inhibir le
- operación del flotacior, y puede ser necesaria una impieza
- 8. Los interruptores de nivel no deben ser reparados en el lugar de la instalación.
- 9. Los defice fisicos al producto pueden dejarlo inservible.

 10. La instalación en un recipiente hecho de materiales magnéticos. puede afectar la operación.

Operation is stated in the tank dry position.

NC Operation: SS Floats: Witness mark (round circle) down. Plastic Floats: Magneta up.

NO Operation: SS Floats: Witness mark (round circle) up. Plastic Floats: Magnets down.

*Note: M3326, M3326-NO are not reversible. The M3326 is Normally
Closed. The M3328-NO is Normally Open.

Mounted Switches:

HC Operation: Arrow mounted vertically pointed down. NO Operation: Arrow mounted vertically pointed up.

lastatación

El funcionamiento se define en la posición de tanque seco. iaterruptores Verticales:

Cerrado:

inter Flotadores de acero (noxidable (SS); Marca testigo (círculo) hacia abajo. Fictadores de

ptástico: Imanes hacia arriba Normalmente Flotadores de acero inoxidable (SS): Marca

testigo (circulo) hacia arriba. Flotadores de plástico: imanes hacia abajo. ota: Los modelos M3326 y M3326-NO no son reversibl M3326 es Hormalmente Cerrado. El M3326-NO es

normalmente abierto.

Interruptores de Montaje Lateral: Normalmente Flecha montada vertical seflalando hacia abajo. Cerrado:

Normalmente Flecha montada vertical sefialando hacia arriba.

Typical Current and Voltage Ratings

* Note: The ratings at right are for resistive loads only, For inductive loads, maximum switch life will be achieved if appropriate arc uppression is used.

Nota: Las clasificaciones de la derecha son sólo para cargas resistivas. Para cargas inductivas, se logrará una vida itil supresión de arco

15	240 AC 120 AC 100 DC 24 DC	0.12 0.10 0.30
30	240 AC 120 AC 120 DC 24 DC	0.14 0.28 0.07 0.28
60	240 AC 120 AC 120 DC 24 DC	0.40 0.50 0.20 0.50
100	240 AC 120 AC 120 DC 24 DC	0.40 1.00 0.40 1.00

Watta Voltage Current Amps

Antonovale

(See details for part number specific approvats on reverse.) ... número de partes específicas el reverso.)

Aprobaciones es de aprobaciones para

5. CSA Haz Loc

2. UL Haz Loc 6. CE 3. Llic

4. CSA

7. NSF 8 ARS



Wide

Madison Part Number:

Número de Parte Madison :

Switch Location (from bottom of fitting)	Colors	Wett Rating	Switch Type	Ory Position
		<u></u>		

Madison Co.

27 Business Park Dr.
Branford, CT 06405 US
Phone: 203-488-4477
Fax: 203-481-5036
Toll-free: 800-466-5383
Email: info@madisonco.com
Website: http://www.madisonco.com

Item # M5600-PR, Stainless Steel Full Size Switches

\$69.04

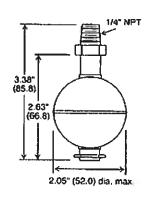
Stainless Steel Full Size Switches

The M5600-PR liquid level switch has a stainless steel stem and a stainless steel float. Stainless steel stems and floats are well suited for corrosive environments as well as food processing, medical, heating, and cooling applications.

The M5600-PR carries CE, NSF International, and American Bureau of Shipping (ABS) approvals. Same day shipping available under our Switch-in-Time program.

Note: SPST = Single Pole, Single Throw





SPECIFICATIONS

Туре	Full Size Switch
Stem Material	316 Stainless Steel
Float Material	316 Stainless Steel
Max. Temperature	200 ℃
Fittings	1/4" NPT
Nominal Current Rating(s)	100 VA SPST Switch
Float SG	0.70
Max. Pressure	500 psig

Dwg. No.	3
Lead Wires	22 ga. Teflon 24"
Approvals	ABS CE NSF International
Maximum Order Quantity for Switch In Time Same Day Shipment	17

Turbine Flow Sensor and Flow Meter Cut Sheet

(Seametrics)



TX80-SERIES Insertion Turbine Flow Sensor



- Industrial wastewater treatment
- · Cooling water monitoring
- · Industrial fluid control

FEATURES

- · Low-friction, long-life jewel bearings
- One moving part
- · Field repairable
- · Choice of materials for chemical compatibility
- Fits 1-1/2" to 8" pipe
- Fixed depth in fitting ensures correct depth in pipe

GENERAL INFORMATION

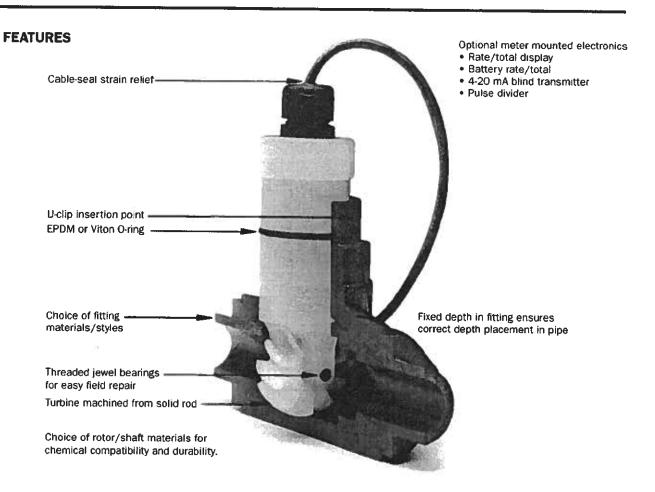
The TX80-Series are insertion turbine meters designed for use in 1-1/2" to 8" pipe. High-quality jewel bearings and precision shafts ensure long life and low friction. Available in 316 stainless steel, brass, PVC and polypropylene, sensor bodies are machined from solid rod for maximum low-flow performance. The TX80-Series use special fittings that ensure ease of installation and correct depth setting in the pipe.

The rotation of the turbine is detected by a non-drag Halleffect sensor. Output is a pulse-type square wave, which can be sent long distances (up to 2,000 feet) without a transmitter. This signal can be connected directly to Seametrics controls and displays, as well as PLC's, counters, and computer cards.

Seametrics TX80 meters are ideal for chemical proportioning applications. If no display is required, a simple divider such as the PD10 provides adjustable pump pacing. For rate and total display, as well as pump pacing, the FT420 flow indicator can be mounted directly on the TX80-Series, or remotely on a wall or panel. The FT415 offers a battery-operated rate/totalizer where power is not available.



TX80-SERIES Insertion Turbine Flow Sensor



SPECIFICATIONS*

Materials	Body	Polypropylene, brass or stainless steel Polypropylene rotor/carbide shaft (PVDF rotor/ceramic shaft optional)						
-	Rotor Assembly							
	Bearings	Ruby jewel		and grade to the second				
	0-Ring	EPDM (Viton optional)						
Rotor Picku	Rotor Pickup GMR (Glant Magnetoresistive Sensor)							
Maximum		Brass	316 SS	PVC/Polypro				
F	Pressure	200 psi (14 bar)	250 psi (17 bar)	175 psi (12 bar) at 75°				
Т	emperature	200° F	(93° C)	130° F (55° C) at 0 psi				
Flow Range)	0.2 to 30 ft./sec.						
Calibrated /	Accuracy	+/- 1.5% of full scale	9					
Signal		Current sinking pulse,	20 mA max. 30 Vdc max (M	icropower option: Pulse output swings between supply voltage and 0 Vdc)				
Power			cropower option: 3.5-16 \					
Cable	-		22 AWG, 3 Con, 18'; 2000' max run					
Regulatory		(Mark (Stainless S	(Mark (Stainless Steel, Brass and Standard Power Only)					

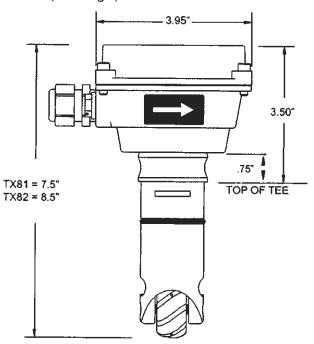
^{*}Specifications subject to change. Please consult our website for the most current data (www.seametrics.com).



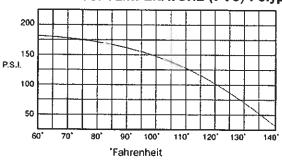
TX80-SERIES Insertion Turbine Flow Sensor

DIMENSIONS

NOTE: Top Housing Optional



PRESSURE VS. TEMPERATURE (PVC/Polypro)

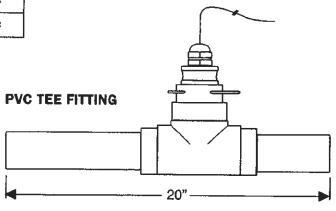


AVAILABLE FITTINGS

	Tee	Saddle	Weld	Braze	Sweat Tee
Вголге	1-1/2"-4"	3"-8"	x	3"-8"	1-1/2"-4"
PVC	1-1/2"-2"	3"-8"	х	х	х
Stainless Steel	1-1/2"-2" 304\$\$	x	3"-8" 316SS	х	x
Carbon Steel	1-1/2"-2"	x	3"-8"	х	х
Ductile Iron	х	3*-8*	х	×	×

FLOW RANGE (in Gallons Per Minute)

	1-1/2"	2"	3"	4"	6"	8"
Min	1.9	3.1	4.6	7.9	18	31
Max	190	314	691	1190	2700	4680





TX80-SERIES Insertion Turbine Flow Sensor

HOW TO ORDER







MATERIAL

Brass = **B**316SS = **S**PVC = **P**Polypro = **Y**

Sec. 01

OPTIONS

Micropower Pickup = -04
(Use with FT415 or DL76)

Rotor/Ceramic Shaft, PVDF (Kynar) = -05

LMI Pump Connector = -08
Seametrics Control Connector = -07

Viton® O-Ring = -60

1.70

FITTINGS

Select from chart above (Fitting Type and Material)



ACCESSORIES

Rate and Total Indicator with pulse & 4-20 mA outputs = FT420
Rate and Total Indicator, battery powered = FT415
Analog transmitter, blind 4-20 mA converter = AO55
Power converter, plug-in, 110-115 Vac, 24 Vdc = PC3

Pulse divider = PD10

Data logger = DL76

Mounting kit, converts wall to meter mount = MK10

Mounting kit, converts meter to wall mount = MK20

CONTACT YOUR SUPPLIER

FT400-Series



RATE/TOTAL INDICATOR INSTRUCTIONS

- FT415
- FT420





The FT400-Series flow computers are microcontroller-based indicator/transmitters that display flow rate and total and provide output signals. The FT415 is battery-powered and provides a scalable pulse output. The FT420 is powered by external DC voltage and has both pulse and 4-20 mA analog outputs. When the FT420 is being used in the 4-20 mA mode, it is a "two-wire" or "loop-powered" device, meaning that the 4-20 mA output signal doubles as its power supply.

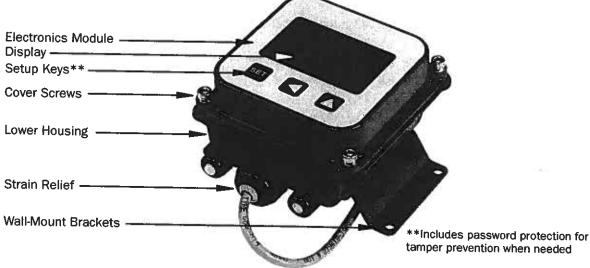
The addition of a dual-relay output board (FT420 only) allows for certain applications requiring contact output isolation (e.g., certain metering pumps and water treatment controls). Dual solid state relays provide exactly the same pulse output as the standard unit, and each can signal one external device. A non-resettable total is also available. The FT420 can be ordered in a plastic enclosure with a 115 Vac power supply for use with mechanical meters, or with a built-in 115

Vac/12-24 Vdc dual power supply for magmeters. Both the FT415 and the FT420 can be factory-mounted on the meter (-M) or remotely wall mounted with the brackets provided (-W). The FT420 is also available as a panel mount (-P) with an open back for easy installation in the user's own electrical enclosure. Most FT400's can be converted from wall-to-meter or meter-to-wall mount configurations after installation if needed.

Housings for the -W and -M models are rugged cast aluminum, potted and gasketed for maximum environmental protection. A membrane keypad allows settings to be changed without removing the cover. (Password protection, a standard feature, can be used to prevent settings from being changed.)

**Includes password protection for tamper prevention when needed

FEATURES



SPECIFICATIONS*		FT415	FT420						
Power		Lithium "C", 3.6 Vdc, replaceable, 3-5 year life	12-30 Vdc, 4mA (4-20 mA when loop-powered)						
Display	Rate	6-digit autorange, 1/2" character height	6-digit autorange, 1/2" character height						
	Total	8-digit, 5/16" character height	8-digit, 5/16" character height						
Outputs	Current Sinking Pulse	Scaled Pulse output (0.1 sec duration 6.1 Hz max) (or High Alarm output or Low Alarm output on FT420 only)							
		Sensor pass-through Pulse output (unscaled)							
	Analog	None	4-20 mA loop; 24-30 Vdc						
Pulse Output Range		0.1 - 9999999.9 units/pulse	0.1 - 9999999.9 units/pulse						
Input		Micropower GMR Sensor (square wave)	5V pulse or contact closure						
Input Rang	e	1.0 - 150 pulses/second	1.0 - 1,500 pulses/second						
K-Factor R	ange	.001 - 99999.999	.001 - 99999.999						
Flow Alarm Output Range		.01 - 999999,99	.01 - 999999.99						
Operating Temperature		-30° to 65° C (-22° to 148° F)	-30° to 65° C (-22° to 148° F)						
Environmental		NEMA 4X, IP66	NEMA 4X, IP66						
Regulatory		None	€ Mark						

HDPE Pipe Data

(Chevron Phillips)



PERFORMANCE PIPE DRISCOPLEX® 4000/4100 Pipe

Water and Wastewater Piping Systems

Corrosion Resistant

Leak Proof Fused Joints

Ideal for Trenchless Applications

Flexible

Hydraulically Efficient ID

Will Not Tuberculate

Reduces Surge Pressure

Outstanding Resistance to Fatigue

Excellent Impact Strength

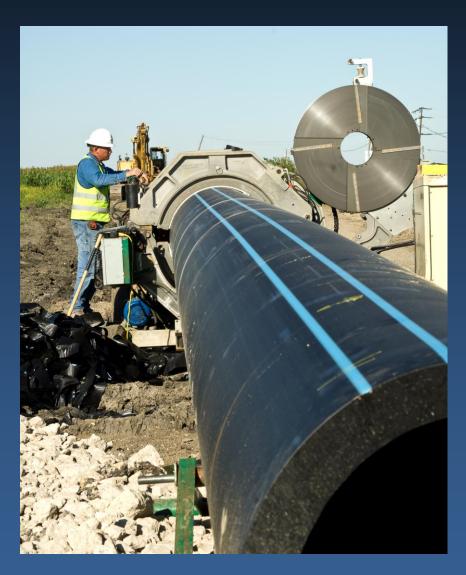
Thrust Blocks Not Needed

Resistant to Sewer Gas

Less Maintenance

Mechanical Fittings Available for Transitions and Repairs

Environmentally Friendly







ASCE Report Card

The American Society for Civil Engineers (ASCE) issues a "report card" on the condition of America's infrastructure about once every five years. In the 2009 report they gave water and wastewater infrastructure a grade of D minus. EPA has identified the two biggest problems facing America's infrastructure as corrosion and leakage. DriscoPlex® 4000 and 4100 High Density Polyethylene (HDPE) pipes offer a solution. HDPE pipes do not undergo galvanic corrosion and are suited for "aggressive soils." They do not rust, rot, corrode, tuberculate, or support biological growth. DriscoPlex® 4000 and 4100 pipes are joined by heat fusion which means the pipes are essentially a continuous pipe without gasket joints to leak. The heat-fused joint is as strong as the pipe itself and fully restrained requiring no thrust blocks.

The Future for Water and Wastewater Piping

Polyethylene pipe's wide acceptance and use for natural gas distribution is the strongest statement that can be made about polyethylene pipe's corrosion resistance and leak-tight nature. Polyethylene pipe has been used for gas distribution pipe since the early 1960's. More than 95% of new gas distribution piping is polyethylene. By 2008, over 577,000 miles of polyethylene natural gas pipe and 39.6 million polyethylene pipe services were installed in the United States. Natural gas service is the most safety critical usage of piping in a municipality. Leakage cannot be tolerated. In addition to the excellent record in gas distribution, polyethylene pipe has been used for water in Europe and North America for 50 years. Recognizing these successes, more and more water and wastewater utilities are turning to polyethylene pipe for both trenchless construction and open-cut applications. For municipal usage, DriscoPlex® pipe is manufactured to ASTM F714, AWWA C901 and AWWA C906 standards. It meets the requirements of NSF/ANSI-61 (NSF/ANSI-14 where noted) and comes in either Iron Pipe Sizes or Ductile Iron Pipe Sizes, i.e. the outside diameter (OD) matches the OD of iron pipe or ductile iron pipe, respectively. In addition to pipe, standard products such as heat-fusion and electrofusion saddles, flanges, mechanical-joint adapters are available for hot tapping and connecting to pumps, hydrants or

valves. Mechanical connections and hot taps requiring no fusion are

available as well.

Performance Pipe Means the Highest Quality

Performance Pipe is a name you can trust in water and sewer piping. Performance Pipe has produced quality polyethylene piping products for fifty years. Our internal QA/QC requirements meet or exceed those required by industry standards. Each production line is continuously monitored throughout the manufacturing cycle to ensure that the product adheres to all internal quality control specifications and the manufacturing standard.

All nine of Performance Pipe's manufacturing facilities and our headquarters are certified in accordance with the latest edition of ISO 9001:2000. Certificates of Conformance are available through our website. Performance Pipe produces all pipe and molded fittings products in the United States. These products are compliant with the Buy American requirement of the 2009 American Recovery and Reinvestment Act.



When you select Performance Pipe DriscoPlex® 4000 and 4100 pipe and fittings, in addition to receiving quality products, you also gain access to our team of experts for technical support, sales and assistance. Our territory sales teams are dedicated to the municipal piping industry and are active



members of the ASTM International, Plastics Pipe Institute, American Water Works Association (AWWA) and many other industry associations. As a company we provide technical expertise and service to these organizations on an ongoing basis.

The unmatched quality and performance of Performance Pipe's polyethylene piping products is further enhanced and strengthened by more than five decades of quality polyolefin plastic resin production from our parent company Chevron Phillips Chemical Company LP.

Polyethylene Resin Continues to Improve

DriscoPlex® pipe and fittings for M&I applications are made from polyethylene materials that are engineered for high density, extra high molecular weight, and broad molecular weight distribution. These characteristics give DriscoPlex® products strength, flexibility, toughness and durability. Since the introduction of polyethylene piping materials in the 1950's, polyethylene resin manufacturers have worked continually to improve their resins. In 2005 "High Performance" polyethylene pipe materials were adopted in U.S. ASTM standards. The most improved of the new materials has a designation code of PE4710. Compared to PE3408 (now PE3608) materials, PE4710 resins have increased density, higher tensile strength and higher resistance to slow crack growth. These increased properties allow the pipe to meet higher performance requirements.



Performance Pipe manufactures pipe and fittings of high performance PE4710. Performance Pipe's PE4710 materials are listed in PPI TR-4 with a Hydrostatic Design Stress of 1000 psi at 73°F. Where

specifications and standards permit, PE4710 materials can be operated at higher pressures than PE3408 materials due to the higher Hydrostatic Design Stress rating at 73°F. PE4710 materials meet or exceed all of the requirements of the former PE3408 resin.

For a more detailed explanation of PE4710 materials and information regarding temperature, design factors and calculation of pressure rating, see PP 816-TN PE3608 and PE4710 Materials Designation Codes and Pipe Pressure Ratings. All Performance Pipe documents may be found at www.performancepipe.com.

Cell Classification for PE4710 Material

ASTM D3350, Standard Specification for Polyethylene Plastics Pipe and Fittings Materials, identifies polyethylene materials for pipe and fittings according to a cell classification system. Performance Pipe's DriscoPlex® 4000 and 4100 series pipe cell classification is listed in Table 1. For specific material properties see PP101, "DriscoPlex® 4000 (DIPS)/4100 (IPS) Water, Wastewater and Industrial".

Table 1: Cell Classifications

Performance Pipe	Material D	esignation Code (MDC)	ASTM D3350 Cell
Product Series	Present	Past	Classification
DRISCOPLEX® 4000/4100 Pipe	PE4710	PE3408	445574C



PE Durability and Disinfectants in Potable Water Applications

HDPE pipes are used extensively in municipal water applications throughout Europe and the United Kingdom – boasting the lowest failure rates of any piping material. HDPE pipes contain additives which protect the pipe from the oxidizing effects of disinfectants. At Performance Pipe, our HDPE water pipes meet AWWA requirements and are evaluated to the toxicological requirements of NSF/ANSI 61. A recent study by Jana Laboratories examined the projected lifespan of polyethylene pipe under typical operating conditions at utilities in Indiana, Florida, North Carolina, and California. Their findings indicate a life expectancy greater than 100 years. Read Jana Laboratories' report, <u>Impact of Potable Water Disinfectants on PE Pipe</u>.

DriscoPlex® Piping Products for Municipal Applications

Performance Pipe offers pipe for municipal applications that are manufactured to both ASTM and AWWA standards simultaneously. Performance Pipe products are generally stocked by distributors and, for many sizes and DR's, are readily Specialty products are available but available. generally not stocked and thus have to be produced at Performance Pipe manufacturing plants. Table 2 lists the various products, applicable standards, and the pipe material designation code. DriscoPlex® pipes series are identified by a four digit number code. For example, DriscoPlex® 4000 pipe.



Table 2. DriscoPlex® Pipes

	DriscoPlex® Municipal Water and Wastewater Pipe											
DriscoPlex® Pipe Series	Features	Size Range	Applicable Standards	Pipe Materials Designation Codes Available (PPI TR-4)								
4000 (DIPS) Municipal potable water, raw water, process water, sewer	Black w/ blue stripes	4" through 42" DIPS	AWWA C906 & ASTM F714 (4" to 42") NSF/ANSI 61	PE4710								
4100 (IPS) Municipal potable water, raw water, process water, sewer	Black pipe is standard	1-1/2" through 54" IPS	AWWA C901 & ASTM D3035 (3" & smaller) ASTM F714 & AWWA C906 (4" to 54") and NSF/ANSI 61	PE4710								

For ¾" through 2" SIDR and CTS and for ¾" through 3" IPS for municipal potable water service lines consider 5100 Ultraline®. See PP410, "DriscoPlex® 5100 Series Ultraline® HDPE Water Service Pipe & Tubing".

DriscoPlex® Pipe is Manufactured to Both ASTM F714 and AWWA C906

DriscoPlex® 4000/4100 pipe meets or exceeds the requirements of ASTM F714 and AWWA C906. ASTM F714 designates a "Pressure Rating (PR)" whereas AWWA C906 designates a "Pressure Class, PC." Currently these are not calculated the same way and therefore are not equal. ASTM F714 recognizes PE4710 material, whereas AWWA C906 is being updated but currently treats PE4710 material as having the same PC as the former PE3408 material. For AWWA C906 ratings, see Appendix 1.



The pressure rating of PE pipe varies with the pipe's Dimension Ratio (DR). The DR is equal to the average pipe outside diameter (OD) divided by the minimum wall thickness. The Plastics Pipe Institute's *Handbook of Polyethylene Pipe* gives the method for calculating the pressure rating. The pressure ratings for DriscoPlex® 4000/4100 pipe allowed by ASTM F714 are given in Table 3.

Water and force main sewer lines have frequent and recurring surges. The designer will consider both the pipe's working or pumping pressure and the total pressure (pumping pressure plus surge pressure) when determining an application's DR. Rating for both are given in Table 3 for easy comparison with design flow conditions.

Table 3 DriscoPlex® 4000 and 4100 Pipe Pressure Ratings per ASTM F714 at 80°F

PE4710 Pipe Pressure Ratings Per ASTM F714 ¹												
Dimension Ratio	Working Pressure Rating (psi)	Allowable Total Pressure During Recurring Surge (psi)	Allowable Total Pressure During Occasional Surge (psi)									
9	250	375	500									
11	200	300	400									
13.5	160	240	320									
14.3	150	225	300									
17	125	185	250									
21	100	150	200									
26	80	120	160									

For Pressure Class and Working Pressure Ratings per AWWA C906, see Appendix 1. Ratings are for water and can vary for other fluids and temperature. Table 3 Working Pressure Ratings may be used with AWWA C901 pipe.

The temperature range for polyethylene pipe is -40°F to 140°F for pressure pipe and -40°F to 180°F for non-pressurized pipe, e.g. gravity flow. When DriscoPlex® pipe operates at a temperature above 80°F the Pressure Rating and Pressure Class of the pipe are decreased. The PR/PC for temperatures above 80°F may be determined by multiplying the PC in Table 3 by the temperature factor from Table 4.

Table 4: Service Temperature Design Factor

Service Temperature Design Factor, F _T ¹														
Service Temperature, °F (°C)	/80 (2/) \ \ -200 (32) -2100 (38) -2110 (43) -2120 (40) -2130 (54) -2140 (60)													
1.0 0.9 0.8 0.71 0.63 0.57 0.50														

¹Use 80°F (27°C) service factor for service temperatures below 80°F (27°C). F_T for temperatures below 100°F are from AWWA M-55. F_T for temperatures above 100°F found by interpolation.

PPI Design & Engineering Calculator for PE Pipe is available on the Performance Pipe website.

DriscoPlex®4000/4100 Pipe Common Sizes

Tables 5 and 6 give dimensions and weights for commonly used DR's in the water and wastewater industry. For other available DR's, see PP152 and PP153, Size and Dimension Sheets. All pipes of a given nominal size are made to the same OD regardless of DR. Therefore, the average inside diameter (ID) varies with the pipe wall thickness. DriscoPlex® 4000/4100 pipe is available in 40 or 50 foot lengths and is also available in coils through 6" DIPS. Packaging and Loading information is available on our website.

Table 5 DriscoPlex® 4000 DIPS Pipe Sizing System

	Common Dimension Ratio's for DriscoPlex® 4000 DIPS Pipe (Custom DR's available. Contact Performance Pipe)												
ASTM F714 PR PR		DR 21 PR = 100 p PC = 80 p	R = 100 psi		DR 14.3 PR = 150 psi PC = 120 psi			DR 11 PR = 200 psi PC = 160 psi			DR 9 PR = 250 psi PC = 200 psi		
Pipe Size, in.	OD, in.	Min. Wall, in.	Avg. ID, in.	Wgt. lbs/ft	Min. Wall, in.	Avg. ID, in.	Wgt. lbs/ft	Min. Wall, in.	Avg. ID, in.	Wgt. lbs/ft	Min. Wall, in.	Avg. ID, in.	Wgt. Ibs/ft
4	4.80	0.229	4.315	1.45	0.336	4.088	2.07	0.436	3.876	2.62	0.533	3.670	3.13
6	6.90	0.329	6.203	2.99	0.483	5.877	4.27	0.627	5.571	5.42	0.767	5.274	6.47
8	9.05	0.431	8.136	5.13	0.633	7.708	7.35	0.823	7.305	9.33	1.006	6.917	11.13
10	11.10	0.529	9.979	7.73	0.776	9.454	11.06	1.009	8.961	14.03	1.233	8.486	16.74
12	13.20	0.629	11.867	10.93	0.923	11.243	15.64	1.200	10.656	19.84	1.467	10.090	23.67
14	15.30	0.729	13.755	14.68	1.070	13.032	21.01	1.391	12.351	26.65	1.700	11.696	31.80
16	17.40	0.829	15.643	18.98	1.217	14.820	27.17	1.582	14.046	34.47	1.933	13.302	41.13
18	19.50	0.929	17.531	23.84	1.364	16.609	34.12	1.773	15.741	43.30	2.167	14.906	51.66
20	21.60	1.029	19.419	29.25	1.510	18.398	41.87	1.964	17.436	53.13	2.400	16.512	63.38
24	25.80	1.229	23.195	41.73	1.804	21.975	59.73	2.345	20.829	75.77	2.867	19.722	90.43
30	32.00	1.524	28.769	64.18	2.238	27.256	91.89	2.909	25.833	116.58			
†36	38.30	1.824	34.433	91.93	2.678	32.622	131.63	3.482	30.918	167.02			
†42	44.50	2.119	40.008	124.09	3.112	37.903	177.70				A		

Average inside diameter is calculated using Nominal OD and Minimum Wall plus 6% for use in estimating fluid flow. Actual ID will vary. When designing components to fit the pipe ID, refer to pipe dimensions and tolerances in the applicable pipe manufacturing specification. †OD available upon special request.

Table 6 DriscoPlex® 4100 IPS Pipe Sizing System

Tubi	Common Dimension Ratio's for DriscoPlex® 4100 IPS Pipe (Custom DR's available. Contact Performance Pipe)															
IPS DR 21 ASTM F714 PR PR = 100 psi		DR 17 PR = 125 psi			Pl	DR 13.5 PR = 160 psi			DR 11 PR = 200 psi			DR 9 PR = 250 psi				
Pipe Size in.	OD, in.	Min. Wall, in.	C = 80 p Avg. ID, in.	Wgt. Ibs/ft	Min. Wall, in.	C = 100 Avg. ID, in.	psi Wgt. Ibs/ft	Min. Wall, in.	C = 130 Avg. ID, in.	psi Wgt. Ibs/ft	Min. Wall, in.	C = 160 p Avg. ID, in.	Vgt. Ibs/ft	Min. Wall, in.	C = 200 Avg. ID, in.	osi Wgt. Lbs/ft
2	2.375	111.			0.140	2.078	0.43	0.176	2.002	0.53	0.216	1.917	0.64	0.264	1.815	0.77
3	3.500				0.206	3.063	0.94	0.259	2.951	1.16	0.318	2.826	1.39	0.389	2.675	1.66
4	4.500	0.214	4.046	1.27	0.265	3.938	1.55	0.333	3.794	1.92	0.409	3.633	2.31	0.500	3.440	2.75
6	6.625	0.315	5.957	2.75	0.390	5.798	3.36	0.491	5.584	4.15	0.602	5.349	5.00	0.736	5.065	5.96
8	8.625	0.411	7.754	4.66	0.507	7.550	5.69	0.639	7.270	7.04	0.784	6.963	8.47	0.958	6.594	10.11
10	10.750	0.512	9.665	7.24	0.632	9.410	8.83	0.796	9.062	10.93	0.977	8.679	13.16	1.194	8.219	15.70
12	12.750	0.607	11.463	10.19	0.750	11.160	12.43	0.944	10.749	15.38	1.159	10.293	18.51	1.417	9.746	22.08
14	14.000	0.667	12.586	12.28	0.824	12.253	14.98	1.037	11.802	18.54	1.273	11.301	22.32	1.556	10.701	26.63
16	16.000	0.762	14.385	16.04	0.941	14.005	19.57	1.185	13.488	24.22	1.455	12.915	29.15	1.778	12.231	34.78
18	18.000	0.857	16.183	20.30	1.059	15.755	24.77	1.333	15.174	30.65	1.636	14.532	36.89	2.000	13.760	44.02
20	20.000	0.952	17.982	25.07	1.176	17.507	30.58	1.481	16.860	37.84	1.818	16.146	45.54	2.222	15.289	54.34
22	22.000	1.048	19.778	30.33	1.294	19.257	37.00	1.630	18.544	45.79	2.000	17.760	55.10	2.444	16.819	65.75
24	24.000	1.143	21.577	36.10	1.412	21.007	44.03	1.778	20.231	54.49	2.182	19.374	65.58	2.667	18.346	78.25
26	26.000	1.238	23.375	42.36	1.529	22.759	51.67	1.926	21.917	63.95	2.364	20.988	76.96	2.889	19.875	91.84
28	28.000	1.333	25.174	49.13	1.647	24.508	59.93	2.074	23.603	74.17	2.545	22.605	89.26	3.111	21.405	106.51
30	30.000	1.429	26.971	56.40	1.765	26.258	68.80	2.222	25.289	85.14	2.727	24.219	102.47	3.333	22.934	122.27
32	32.000	1.524	28.769	64.17	1.882	28.010	78.28	2.370	26.976	96.87	2.909	25.833	116.58	3.333	22.934	122.27
34	34.000	1.619	30.568	72.44	2.000	29.760	88.37	2.519	28.660	109.36	3.091	27.447	131.61			
36	36.000	1.714	32.366	81.21	2.118	31.510	99.07	2.667	30.346	122.60	3.273	29.061	147.55			
42	42.000	2.000	37.760	110.54	2.471	36.761	134.84	3.111	35.405	166.88						
48	48.000	2.286	43.154	144.38	2.824	42.013	176.12									
54	54.000	2.571	48.549	182.73	3.176	47.266	222.90									

For pipe smaller than 2" see PP415, DriscoPlex® 5100 Water Service Pipe and Tubing.

Average inside diameter is calculated using Nominal OD and Minimum Wall plus 6% for use in estimating fluid flow. Actual ID will vary. When designing components to fit the pipe ID, refer to pipe dimensions and tolerances in the applicable pipe manufacturing specification.



PERFORMANCE ADVANTAGES OF DRISCOPLEX® 4000/4100 PIPE

Stripes

Stripes allow easy field identification of pipe. DriscoPlex® 4000 (DIPS) pipe comes standard with three pairs of blue stripe, but lavender, green, and no stripes is optional. The standard DriscoPlex® 4100 (IPS) is black, but blue, lavender and green striping is optional with 4 single stripes at 90 degrees apart.

Flow

DriscoPlex® 4000/4100 pipes are characterized as hydraulically smooth and typically have an absolute surface roughness (ε) of 0.000005 ft. The Hazen-Williams Friction Factor (C) equals 150 to 155 for polyethylene pipes. Even though the inside diameter of polyethylene pipe may be smaller for the same nominal size as metallic or concrete pipes, flow is often equal or greater through polyethylene pipe. For example, an 8" DR17 DriscoPlex® 4000 pipe has a lower pressure drop per given flow rate than an 8" CL350 concrete lined DI pipe (C equals 120). For gravity flow, the n-factor in the Manning equation is typically taken as 0.009 for clear water and 0.010 for sanitary sewer. For design information, see the Handbook of Polyethylene Pipe, Chapter 6.

Surge Pressure

When it comes to surges, polyethylene has two advantages over most piping materials. 1) As Table 3 shows, it has the capacity to handle surge pressures significantly in excess of its pressure rating. 2) It also has the lowest surge pressure of all common water pipes. For example, a 5 ft/sec velocity change in a DR17 Polyethylene pipe will produce a 56 psi surge, in a DR18 PVC pipe the surge is



88 psi, and in a Class 50 DI pipe the surge is 268 psi. Thus, with polyethylene pipe there are lower surge pressures and less wear and tear on valves, hydrants, and other system components and, when surges occur, HDPE pipes may be quite capable of handling them with a lower Pressure Class (PC) than required for other materials.

Fatigue

Repeated surges will cause fatigue stress in pipelines. This is particularly significant in certain thermoplastic pipes, excluding polyethylene. Fortunately, polyethylene has an excellent resistance to fatigue. The projected design life for DriscoPlex® 4000/4100 pipes exceeds 100 years for pipe operating at a velocity of 4 fps with a surge frequency of 4 times per hour continuously. See Bulletin PP-402. Working Pressure Rating and Fatigue Life.

Comparison with Other Piping Products

Polyethylene's superior performance is due to its fused joint, toughness, and flexibility. Comparisons of polyethylene to other piping materials based on PC alone can lead to costly over-designs, since the definition of "Pressure Class" varies from material to material (see AWWA C906, C905, etc). When correctly incorporating HDPE's lower surge magnitudes, higher surge allowances, and greater fatigue strength into the design, the PC required for HDPE may be much lower than the PC required for other pipe materials.



Impact Resistance

Polyethylene pipe is routinely used in mining applications above the Arctic Circle and can withstand water freezing internally. A product that can be handled in these extreme conditions has to have excellent impact resistance. The Izod Impact Strength of high density polyethylene using ASTM D256 Method A is 4 to 5 ft-lbs/in at 73°F, again a value significantly greater than other plastic pipe materials.

Rapid Crack Propagation

Impact damage, fatigue, or joint failure in metal or thermoplastic pipes under certain operating conditions can lead to long, running cracks that will propagate through fused joints and can travel hundreds of feet. This cracking is referred to as Rapid Crack Propagation (RCP). One published report cites an 1100 ft long crack that occurred in a fusion joined PVC pipeline. Polyethylene pipe has excellent resistance to RCP. In fact, laboratory testing has shown that RCP cannot occur in a water filled polyethylene pipe. PP838, *Preventing RCP in Fused Water Pipelines* indicates that the best way to avoid this type of cracking is to specify polyethylene pipe as opposed to other thermoplastic pipes.

INSTALLATION ADVANTAGES OF DRISCOPLEX® 4000/4100 PIPE

Heat Fusion of Polyethylene Pipe

Heat fusion of polyethylene pipe is proven, reliable, and time-tested, with over 50 years of success. The procedure is standardized, published in ASTM F2620, and there are thousands of trained operators around the nation. Compared to fusing other types of thermoplastic pipes, the process for polyethylene pipe is easier to learn, more forgiving, and results in higher productivity rates. Joints have the same tensile strength as the pipe and no thrust blocks or restraints are required at fittings and bends. Polyethylene pipe can be fused and installed in subfreezing weather. See PP750, Heat Fusion Joining Procedures and Qualification Guide.



Exceptional for Trenchless Installations

DriscoPlex® pipe is flexible and tough. As a result, polyethylene pipes are well-suited for horizontal directional drilling, plowing, river and water crossings, pipe bursting and sliplining. Installers like the fact that polyethylene pipe is tough enough to stand up to rigors of field handling with higher impact resistance, greater ductility, more flexibility, and higher resistance to RCP than its closest thermoplastic competitor. There is a wealth of technical publications for trenchless usage of polyethylene pipe including the *Handbook of Polyethylene Pipe*. See Chapter 11 "Pipeline Rehabilitation by Sliplining with PE Pipe," Chapter 12, "Horizontal Directional Drilling," and Chapter 16, "Pipe Bursting."

Small Bend Radius; Big Installation Advantage

Installers often choose DriscoPlex® 4000/4100 pipe because of its flexibility and tight bend radius. The bend radius is the smallest radius to which a pipe can be bent without causing permanent damage. In open-cut and above-grade applications pipe may be strung around corners or over swales often eliminating fittings. Polyethylene water mains can typically be laid around a cul-de-sac without the use of fittings. In trenchless applications, a more flexible pipe results in shorter insertions pits and reduced costs.



For horizontal directional drilling, a tight bend radius greatly reduces laydown space, the area where pipe is placed prior to pullback. In tight suburban right-of-ways, it is often necessary to string pipe around corners or bends while awaiting pullback. Flexibility facilitates this and polyethylene pipe can be curved to a radius 1/10th of that of its closest thermoplastic pipe competitor. Thus, it is more convenient for the installer and less disruptive to the public by eliminating inconvenient street closures. In addition.

this extra flexibility provides a safety factor against damage during pullback as the polyethylene pipe will almost always have a tighter bending radius than the drill rod used to install it. Thus, polyethylene pipe is protected from overbending unlike other fused thermoplastic pipes.

Bend radius should not be confused with the length of the pipe required to make a specific turn. Table 7 gives both the bend radius and the length required to make a 90° bend. For additional information on bending see PP407, "Small Bend Radius Big Installation Advantage" and PP819, "Field Bending of PE Pipe".



Table 7. DriscoPlex® 4000/4100 Minimum Bend Radius

10.010	DriscoPlex® 4000/4100 Minimum Bend Radius												
4100 IPS Size (in)	Mi	Minimum Bend Radius (ft)			Radius Require			uired to M	gth of Pipe red to Make a Bend (ft)				
	DR 9	DR 11 DR 13.5	DR 17 DR 21	DR 9	DR 11 DR 13.5	DR 17 DR 21	(in)	DR 9	DR 11 DR 14.3	DR 21	DR 9	DR 11 DR 14.3	DR 21
2	4.0	4.9	5.3	6.2	7.8	8.4							
3	5.8	7.3	7.9	9.2	11.5	12.4							
4	7.5	9.4	10.1	11.8	14.7	15.9	4	8.0	10.0	10.8	12.6	15.7	17.0
6	11.0	13.8	14.9	17.3	21.7	23.4	6	11.5	14.4	15.5	18.1	22.6	24.4
8	14.4	18.0	19.4	22.6	28.2	30.5	8	15.1	18.9	20.4	23.7	29.6	32.0
10	17.9	22.4	24.2	28.1	35.2	38.0	10	18.5	23.1	25.0	29.1	36.3	39.2
12	21.3	26.6	28.7	33.4	41.7	45.1	12	22.0	27.5	29.7	34.6	43.2	46.7
14	23.3	29.2	31.5	36.7	45.8	49.5	14	25.5	31.9	34.4	40.1	50.1	54.1
16	26.7	33.3	36.0	41.9	52.4	56.5	16	29.0	36.3	39.2	45.6	56.9	61.5
18	30.0	37.5	40.5	47.1	58.9	63.6	18	32.5	40.6	43.9	51.1	63.8	68.9
20	33.3	41.7	45.0	52.4	65.5	70.7	20	36.0	45.0	48.6	56.5	70.7	76.3
22	36.7	45.8	49.5	57.6	72.0	77.8							
24	40.0	50.0	54.0	62.8	78.5	84.8	24	43.0	53.8	58.1	67.5	84.4	91.2
28	46.7	58.3	63.0	73.3	91.6	99.0							
30	50.0	62.5	67.5	78.5	98.2	106.0	30		66.7	72.0		104.7	113.1
32		66.7	72.0		104.7	113.1							
34		70.8	76.5		111.3	120.2							
36		75.0	81.0		117.8	127.2	36		79.8	86.2		125.3	135.4
42		87.5	94.5		137.4	148.4	42		92.7	100.1		145.6	157.3
48			108.0			169.6							
54			121.5			190.9							
	When fittings or flanges are present the hend radius is normally taken as 100 times the nine diameter												

When fittings or flanges are present the bend radius is normally taken as 100 times the pipe diameter.



Safe Pull Strength

Most all trenchless methods using polyethylene pipe are pull-in or pullback techniques. Pull-in distance is often proportional to the pipe's safe pull strength, which is the maximum tensile force that can be applied to the pipe with adequate assurance that the pipe will not be damaged or changed in any way that could affect its long term performance. The maximum safe tensile stress in DriscoPlex® PE4710 pipe for a 10 hour pull is 1300 psi. Table 8 lists the safe pull strength for DriscoPlex® 4000/4100 pipe.

Table 8. Safe Pull Strength for DriscoPlex® 4000/4100

Safe Pull Strength for DriscoPlex® 4000/4100 (PE4710)										
4100 IPS Nom. Size (in)		Safe P	ull Streng	th (lbs)		4000 DIPS Nom. Size	s	afe Pull S	Strength (II	os)
	DR 9	DR 11	DR 13.5	DR 17	DR 21	(in)	DR 9	DR 11	DR 14.3	DR 21
2	2,275	1,904	1,580	1,275	1,045					
3	4,941	4,135	3,431	2,770	2,269			-	-	-
4	8,168	6,835	5,672	4,579	3,751	4	9,294	7,777	6,120	4,267
6	17,704	14,814	12,294	9,924	8,129	6	19,204	16,070	12,647	8,818
8	30,007	25,109	20,838	16,820	13,779	8	33,037	27,644	21,756	15,170
10	46,614	39,005	32,371	26,130	21,404	10	49,699	41,587	32,728	22,821
12	65,572	54,869	45,536	36,757	30,110	12	70,282	58,811	46,283	32,273
14	79,060	66,155	54,903	44,317	36,303	14	94,424	79,012	62,181	43,358
16	103,262	86,407	71,709	57,884	47,416	16	122,123	102,190	80,422	56,077
18	130,691	109,359	90,757	73,259	60,011	18	153,380	128,345	101,005	70,430
20	161,346	135,011	112,046	90,443	74,088	20	188,194	157,477	123,931	86,416
22	195,229	163,363	135,576	109,436	89,646					
24	232,339	194,416	161,346	130,238	106,686	24	268,496	224,672	176,813	123,289
28	316,239	264,621	219,610	177,269	145,212					
30	363,029	303,775	252,104	203,497	166,697	30		345,628	272,003	189,664
32		345,628	286,838	231,535	189,664					
34		390,182	323,813	261,381	214,113					
36		437,435	363,029	293,036	240,044	36		410,898	389,647	271,696
42			494,123	398,855	326,726	42			526,010	366,780
48				520,953	426,745					
54		1		1	540,099					

Horizontal Directional Drilling Resources

In developing plans for a directional drilling project, the designer must determine what DR to use. In addition to working-pressure considerations, DR selection depends on how much force will be required to pull the pipe back into the bore and on how much external force will be applied to the pipe during and afterward from the drilling slurry, soil and groundwater. Several resources are available to help the designer select an appropriate DR. Some of these resources offer additional and important information for planning a crossing. Resources include the following: ASTM F1962, a standard guide for the design



of a directional drilled crossing with polyethylene pipe; the PPI Handbook of Polyethylene Pipe. Chapter 12; ASCE MOP 108, Pipeline Design for Installation by Horizontal Directional Drilling; and the Plastics Pipe Institute's Technical Report 46, Guidelines for Use of Mini-Horizontal Directional Drilling for Placement of Polyethylene Pipe. In addition, the PPI BoreAid program is useful for making a preliminary evaluation of the DR requirements and the anticipated pullback force. A link to PPI BoreAid can be found on the Performance Pipe website on the Engineering Information page.

Burial in Open-Cut Trenching

The PPI Handbook of Polyethylene Pipe, Chapter 6, gives design guidance for open-cut trench installations of polyethylene pipes. HDPE pipe has been placed in landfills with cover depths well in excess of 100 ft. However, most municipal applications are significantly shallower. For the convenience of the designer, AWWA M-55, PE Pipe—Design and Installation, offers a safe design window. Pipe within the window meets the design deflection limits of M-55 and provide at least a 2:1 Safety Factor against buckling. For deeper depths or heavier loading, calculations are required.

Table 9. AWWA M-55 Minimum and Maximum Depths without doing calculations

AWWA M-55 Design Window									
DriscoPlex® 4000/4100 Pipe DR7.3 through DR21									
Minimum Cover Depth with no surface load	2 feet								
Minimum Cover Depth with H20 truck load	3 feet								
Maximum Cover Depth	25 feet								
Requirements									

Minimum E' of native soil of 1000 psi. Maximum backfill weight of 120 pcf. No water above ground surface. Granular embedment soil around pipe with a minimum density of 85% Standard Proctor. Pipe installed per ASTM D2774 and PP-901.

Like all piping materials, HDPE piping must be properly installed. DriscoPlex® 4000/4100 pipe should be installed in accordance with ASTM D 2774 Standard Practice for Underground Installation of Thermoplastic Pressure Piping and Performance Pipe's PP-901, Field Handbook. HDPE is a flexible piping material that works together with its soil embedment to sustain the earth and live loads above it. Suitable embedment is required to provide support around the pipe, and embedment materials must be placed so that the pipe is properly surrounded. Under roadways, compacted coarse sands and gravels are preferred, but other materials may be used under the direction of the design engineer. For more information on installation of 12" and smaller diameter DriscoPlex® pipe see the Plastics Pipe Institute's Polyethylene Piping Systems Field Manual for Municipal Water Applications. For installation by plowing and planting see the special underground installation techniques section of PP-901.

Ground Movement and Seismic Resistance

A large number of water main breaks occur every year due to soil settlement, freeze/thaw cycles, and shrinking or swelling of expansive soils, not to mention the occasional widespread damage that accompanies earthquakes. Polyethylene's flexibility and its fusion joints make it considerably less susceptible to damage from ground movement. California gas utilities recognize polyethylene's excellent record in enduring seismic events without damage.

Poisson Effect

When polyethylene pipe connects to a gasket jointed pipeline, the polyethylene pipe must be anchored or the gasket joints upstream (or downstream) from the transition must be restrained to prevent pullout of the gasket joints. See PP813, Poisson Effect.



Above Grade and Aerial Installation

Performance Pipe black polyethylene pipe contains carbon black allowing indefinite above grade storage and use. For details on above grade applications see PP814, *Thermal Effects* and PP815, *Above Grade Pipe Supports*.

Vacuum Resistance (External Pressure)

Many pipelines operate under full or partial vacuum or experience negative internal pressures when subject to pressure surges. External pressure exceeding the internal pressure (external differential pressure) creates the same effect. Pipelines may be subject to external pressure during installation, submergence, grouting of sliplined pipe, or directional drilling. All pipes have a limit to the amount of external differential pressure (or vacuum) they can withstand. Exceeding that limit will cause the pipe to collapse. Table 10 gives the allowable external differential pressure based on Equation 3-39 in Chapter 6 of the *Handbook of Polyethylene Pipe* with a safety factor of two against collapse and with 3% ovality in the pipe. Higher resistance to collapse can be achieved by embedding the pipe in soil, flowable fill, grout, or concrete. For additional temperatures, see PP-901, *Field Handbook*.

Table 10. DriscoPlex® 4000/4100 Collapse Resistance (Vacuum Resistance)

DriscoPlex® 4000/4100 Collapse Resistance (Vacuum Resistance) DriscoPlex® 4000/4100 External Pressure Resistance PE4710											
Service Temperature	Pipe DR	External Differential Pressure or Vacuum Resistance 3% ovality with 2:1 safety factor ¹ (psi)									
		50 yr	10 yr	1 yr	1000 hr	100 hr	10 hr	0.5 hr	Short- Term		
Modulus Value (psi)		29000	34000	40000	46000	55000	65000	82000	130000		
	9	54.0	63.3	74.5	85.6	102.4	121.0	152.6	242.0		
	11	27.6	32.4	38.1	43.8	52.4	61.9	78.1	123.9		
73°F	13.5	14.1	16.6	19.5	22.4	26.8	31.7	40.0	63.4		
	14.3	11.7	13.8	16.2	18.6	22.3	26.3	33.2	52.7		
	17	6.7	7.9	9.3	10.7	12.8	15.1	19.1	30.2		
	21	3.5	4.1	4.8	5.5	6.6	7.7	9.8	15.5		
	9	31.3	36.7	43.2	49.7	59.4	70.2	88.5	140.3		
	11	16.0	18.8	22.1	25.4	30.4	35.9	45.3	71.9		
120°F	13.5	8.2	9.6	11.3	13.0	15.6	18.4	23.2	36.8		
120°F	14.3	6.8	8.0	9.4	10.8	12.9	15.3	19.3	30.5		
	17	3.9	4.6	5.4	6.2	7.4	8.8	11.1	17.5		
	21	2.0	2.3	2.8	3.2	3.8	4.5	5.7	9.0		

¹Gray shading indicates value equals or exceeds full vacuum of 14.7 psi.

Fittings

Performance Pipe manufactures HDPE molded <u>Fittings</u> including tees and elbows in sizes through 8" diameter. Flange adapters for flange connections are available through 24" diameter. MJ Adapters for both DriscoPlex® 4000 and 4100 pipe are available through 12" diameter. Larger fittings are available through third party fabricators.



Transition to Non-Polyethylene Pipes

Polyethylene pipe can be conveniently connected to metallic valves, pumps and even pipe. Normally the connection is made using a polyethylene Van Stone style Flange Adapter with a metallic backup ring which mates to a metallic flange or using a polyethylene Mechanical Joint (MJ) Adapter which mates to a DI mechanical joint bell. The MJ Adapter works with both IPS and DIPS polyethylene pipe. Acceptable methods also include metallic transition couplings that slide on, seal, and grip the polyethylene pipe or metallic transition couplings that slide on and seal but require additional external restraint rings. These types of couplings may require the use of an insert stiffener in



the polyethylene pipe. DriscoPlex® 4000 pipe may be inserted directly into an MJ Bell. This requires placing an insert stiffener inside the end of the DriscoPlex® pipe and restraining the connection with an external ring or clamp on the DriscoPlex® pipe. When selecting mechanical couplings or components for use with DriscoPlex® pipe, make sure the mechanical coupling manufacturer recommends the particular part for HDPE pipe. For additional information on HDPE to non-HDPE pipe transitions, see the Plastics Pipe Institute's TN-36, General Guidelines for Connecting Potable Water HDPE Pressure Pipes to DI and PVC Piping Systems and Polyethylene Piping Systems Field Manual for Municipal Water Applications.

Tapping

A variety of heat fusion and mechanical fittings make hot or cold tapping a straightforward process. Heat fusion jointed products include saddle fusion tapping tees, electrofusion tapping tees, and branch-saddles. A number of manufacturers produce metallic full body tapping saddles and sleeves for polyethylene pipe. Performance Pipe recommends that the manufacturer be contacted to make sure their saddles work with polyethylene pipes. Service saddles are available as well. These may come with double or extra wide straps, with spring washers, or with both.

Repair

Polyethylene pipe has an excellent field record. However, circumstances may arise where repair is necessary. The most likely form of damage is impact or an underground strike which is usually localized. A variety of repair clamps (both mechanical and electrofusion) and tapping saddles are available. If a section of pipe has to be removed, a new pup piece can be inserted using mechanical couplings, polyethylene flange adapters, or electrofusion couplings.

Leak Testing

Polyethylene pipe may be hydrostatically tested to determine system integrity for leaks. When testing is required, observe all safety measures. See Performance Pipe PP 802, *Leak Testing of Polyethylene Pipe*. Typically, HDPE pipe is leak tested to 1.5 times its Pressure Rating (PR). See Tables 5 and 6.

Water Quality

Water utilities aim to maintain a high standard of water quality and to protect public drinking water from any internal and external contaminates. All piping systems have some potential for contamination from external agents through permeation of gaskets, jointed connections, or permeation through the pipe wall. Literature suggests that permeation of organic chemicals and hydrocarbons through polyethylene pipe is possible, while actual cases of soil contaminated hydrocarbon permeation are extremely rare.



Hydrocarbons do not degrade polyethylene but can diffuse through the wall of the pipe in areas of gross contamination. The exterior contact may affect sidewall fusions and or butt fusions; thus, after polyethylene pipes have been exposed to grossly contaminated soils, mechanical connections may be preferred.

There are several ways to address gross hydrocarbon contamination of soil surrounding the pipe including removal and replacement of the contaminated soil with good clean soil of Class I or Class II materials, sleeving the pipe, and rerouting the pipe around the contaminated area.

Safety

Polyethylene piping has been safely used in thousands of applications. However, there are general precautions that should be observed when using any product. In this respect, polyethylene piping is no different. Performance Pipe's recommends the following reading for a more detailed list of cautions and safety features.

- 1. The Plastic Pipe Institute Handbook of Polyethylene Pipe, Chapter 2. *Inspections, Tests and Safety Features*.
- 2. The Performance Pipe Field Handbook.
- 3. Pipe Loading/Unloading-Truck Driver Safety Video

Technical Information

A large body of technical information related to the design and installation of polyethylene pipe is available at the Plastics Pipe Institute's website, www.plasticpipe.org and on Performance Pipe's website, www.performancepipe.com. Additional information on polyethylene pipe including case history information is available at the PE Alliance site, www.pepipe.org.









APPENDIX A. PRESSURE CLASS SELECTION PER AWWA C906

Selecting the right Pressure Class for High Density Polyethylene pipe in accordance with AWWA C906 is easy. Just two steps! AWWA C906 takes into account the continuous pumping and transient (surge) pressures that occur in municipal water pipes.

Step 1. Compare the pipeline working pressure with the pipe's Pressure Class.

AWWA C906 defines working pressure as "the maximum anticipated, sustained **operating pressure applied to the pipe exclusive of transient pressures".** The maximum working pressure for a pipe must be less than or equal to the pipe's Pressure Class. Table A-1 gives Pressure Class for standard Dimension Ratio's (DR) HDPE pipe made from PE3608 material.

Table A-1: Maximum Allowable Pressures for HDPE Pipe (PE3608) at 80°F¹ (Per AWWA C906)

		(1.01.7111171.0000)									
		Pressure Class/ Maximum Working Pressure (psi)	Maximum Total Pressure ² Allowed During Recurring Surge (psi)	Maximum Total Pressure ² Allowed During Occasional Surge (psi)	Maximum Test Pressure Allowed per AWWA Manual M55 (psi)						
	7.3	254	380	510	380						
	9	200	300	400	300						
DR	11	160	240	320	240						
Pipe	13.5	128	185	250	185						
	17	100	150	200	150						
	21	80	120	160	120						

¹Pressures above 80°F require derating. See Table 4.

Step 2. Compare the peak pipeline pressure during surge with the pipe's allowable Maximum Total Pressure.

Peak pressure during a surge is equal to the sum of the pumping pressure and the transient surge pressure. Transient surge pressure depends on the instantaneous change in flow velocity. Maximum transient pressure due to an instantaneous change in flow velocity is given in Table A-2. Peak pressure may be obtained by adding the surge pressure at the design velocity from Table A-2 to the pumping pressure. Peak pressure is compared with the Maximum Total Pressure Allowed During Surge in Table A-1. The Maximum Total Pressure Allowed equals 1.5 times the pipe's Pressure Class for recurring surge and 2.0 times the pipe's Pressure Class for occasional surge.

²Total pressure equals the combined pumping (working) pressure plus surge pressure. Recurring surges are frequently occurring surges inherent to the design and operation of the system. Occasional surges are caused by emergency operations such as fire flows.



Note: The surge pressure occurring in HDPE pipe is significantly lower than surge pressures occurring in cast or ductile iron pipe and is lower than that in PVC pipe of the same DR. For example, a 4 fps instantaneous velocity change in HDPE DR17 pipe results in a 45.0 psi surge whereas for DI pipe the surge is 200 psi and for PVC DR18 pipe the surge is 69.6 psi. When HDPE pipe is connected to DI pipe the surge pressure is dampened by the HDPE pipe.

Table A-2. Surge Pressure at 80°F for Sudden Velocity Change, psi (Per AWWA M-55)

	(1.0.7111171.11.00)											
		Surge Pressure, psi										
		1 fps	2 fps	3 fps	4 fps	5 fps	6 fps	7 fps	8 fps			
	7.3	18.4	36.8	55.2	73.6	92.0	110.4	128.8	147.2			
	9	16.2	32.4	48.5	64.7	80.9	97.1	113.2	129.4			
DR :	11	14.4	28.7	43.1	57.5	71.9	86.2	100.6	115.0			
Pipe	13.5	12.8	25.6	38.4	51.2	63.9	76.7	89.5	102.3			
	17	11.3	22.5	33.8	45.0	56.3	67.5	78.8	90.0			
	21	10.0	20.1	30.1	40.1	50.2	60.2	70.2	80.3			

Working Pressure and Surge Pressure Example:

An engineer is designing a water system that operates at 85 psi and has some runs in it where the flow velocity is 4 fps. In addition, his/her state requires a 150 psi test for the pipeline. What DR pipe does the engineer use?

Step 1. Compare the pumping pressure, 85 psi, with the available Pressure Classes in Table A-1. DR17 has a PC of 100 psi>85 psi. The test pressure of DR17 is also 150 psi, which meets the specified test pressure.

Step 2. The anticipated peak pressure in the pipeline is found by adding the pumping pressure of 85 psi to the surge pressure of 45.0 psi (given in Table A-2 for a 4 fps velocity). The sum equals 130.2 psi and is less than the Maximum Total Pressure Allowed for Recurring Surge for DR17 pipe of 150 psi. DR17 pipe is O.K. A similar comparison can be made for peak pressure during fire flow where velocity may reach 8 fps. In this case add 90.0 psi (from Table A-2) to 85 psi to obtain a peak pressure during occasional surge of 175 psi. Compare with the Maximum Total Pressure Allowed for Occasional Surge for DR17 of 200 psi. DR17 pipe is O.K.



CONTACT INFORMATION:

Performance Pipe a Division of Chevron Phillips Chemical Company LP 5085 West Park Blvd, Suite 500, Plano, TX 75093

Phone: 800-527-0662 Fax: 972-599-7329

Visit Performance Pipe on the web for the latest literature updates.

www.performancepipe.com







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Ball Valve and Hose Adapter

(Grainger)





Ball Valve, Two Piece, 2 In, 316 SS Body

Two Piece Ball Valve, FNPT Connection, Max. Pressure 1000 psi WOG, Full Port, Material of Construction 316 Stainless Steel, Seats PTFE, Ball Material 316 Stainless Steel, Stem Material 316 Stainless Steel, Stem Blowout Proof, Handle Stainless Steel, Lockable, With Vinyl Grip, Standards -

Grainger Item # 1WMY7 \$202.00 Price (ea.)

GRAINGER APPROVED Brand **VENDOR**

Mfr. Model # 1WMY7

Ship Qty. Sell Qty. (Will-Call) 1 Ship Weight (lbs.) 5.5

Availability Ready to Ship

4364 Catalog Page No.

Price shown may not reflect your price. Log in or register.

Additional Info

316 Stainless Steel Ball Valves with Handle Options

Stainless steel handle with vinyl grip. Bottom-loaded stem resists blowout. 2-pc. valves with PTFE seats and FNPT connections. Vacuum service to 29" Hg. For use with water, oil, and gas in most corrosive industrial environments.

■ Rated: 1000 psi; 150 psi WSP Temp. range: -25° to 450°F

Tech Specs

Item: Ball Valve Type: Two Piece Connection: FNPT

Max. Pressure: 1000 psi WOG

Pipe Size: 2" Port: Full

Material of Construction: 316 Stainless Steel

Seats: PTFF

Ball Material: 316 Stainless Steel Stem Material: 316 Stainless Steel

Stem: Blowout Proof

Handle: Stainless Steel, Lockable, With Vinyl Grip

Temp. Range (F): -25 to 450 Degrees Overall Length (In.): 4-29/32

Notes & Restrictions

There are currently no notes or restrictions for

this item.

MSDS

This item does not require a Material Safety Data Sheet (MSDS).

Required Accessories

There are currently no required accessories for this item.

Optional Accessories

There are currently no optional accessories for this item.

Alternate Products

Ball Valve, Two Piece, 2 In, 316 SS Body



Item #: 1WNA7

Brand: GRAINGER APPROVED

VENDOR

Usually Ships: Ready to Ship

Price (ea): \$207.75

Repair Parts

A Repair Part may be available for this item. Visit our Repair Parts Center or contact your local branch for more information.





Adapter, Male, 2 In

Cam And Groove Coupling, Size 2 In, Male Adapter x FNPT Connection, Max Working Pressure 250 PSI, Material of Construction Aluminum

Grainger Item # 3LX26
Price (ea.) \$13.43

Brand GRAINGER APPROVED VENDOR

Mfr. Model # 3LX26
Ship Qty. 1
Sell Qty. (Will-Call) 1
Ship Weight (lbs.) 0.35

Availability Ready to Ship

Catalog Page No. 4066

Price shown may not reflect your price. Log in or register.

Additional Info

Aluminum and Stainless Steel

Max. pressure: 250 psi (up to 2"); 125 psi (3"); 100 psi (4") Temp. range:
 -40° to 212°F Interchangeable with all product produced to MIL-C-27487F
 Buna N gasket

Cam and Groove Couplings

Couplings have Buna N seals and stainless steel pins. Pull rings and locking pins are plated carbon steel.

Meet ASTMC 38000 and MIL-C-27487F specifications.

Tech Specs

Item: Adapter

Type: A Size: 2"

Connection: Male Adapter x FNPT

Max. Working Pressure (PSI): 250

Material of Construction: Aluminum

Notes & Restrictions

There are currently no notes or restrictions for this item.

MSDS

This item does not require a Material Safety Data Sheet (MSDS).

Required Accessories

There are currently no required accessories for this item.

Optional Accessories

Coupler, Female, 2 In



Item #: 3LX32

Brand: GRAINGER APPROVED

VENDOR

Usually Ships: Ready to Ship

Price (ea): \$27.20

Cap with Handle, 2 In, Polypropylene



Item #: 4YLL3

Brand: GRAINGER APPROVED

VENDOR

Usually Ships: Ready to Ship

Price (ea): \$41.00

Alternate Products

Adapter, Male, 2 In, 316 SS



Item #: 3LX27

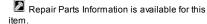
Brand: GRAINGER APPROVED

VENDOR

Usually Ships: Ready to Ship

Price (ea): \$63.40

Repair Parts



PART 361 SITING CERTIFICATE APPLICATION

Submitted in separate electronic file

PART 617 DRAFT ENVIRONMENTAL IMPACT STATEMENT (DEIS)

Submitted in separate electronic file